El Paso County Stormwater Master Plan

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Prepared for:

El Paso Water 1154 Hawkins Boulevard El Paso, Texas 79961



and

El Paso County 500 E. San Antonio El Paso, TX 79901



Prepared by:



9400 Amberglen Blvd. Austin, Texas 78729

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Acronyms and Abbreviations

°F Degrees Fahrenheit

% Percent

AECOM Technical Services, Inc.

CBC Concrete box culvert

CIP Capital Improvement Program
CLOMR Conditional Letter of Map Revision

CMP Corrugated metal pipe
DDM Drainage Design Manual

EDAP Economically Distressed Areas Program

EPNG El Paso Natural Gas EPW El Paso Water

ETJ Extraterritorial Jurisdiction Areas

FEMA Federal Emergency Management Agency

FIRM Flood Insurance Rate Map FIS Flood Insurance Study

HEC-HMS Hydrologic Engineering Center-Hydrologic Modeling System
HEC-RAS Hydrologic Engineering Center-River Analysis System

IBWC International Boundary and Water Commission

IH-10 Interstate Highway 10LOMR Letter of Map RevisionMSR Model Subdivision Rule

No. Number

NOAA National Oceanic and Atmospheric Administration

NRCS Natural Resources Conservation Service

PMP Probable maximum precipitation PSC Parkhill, Smith, & Cooper, Inc.

PVC Polyvinyl chloride

RCP Reinforced concrete pipe

ROW Right-of-way

SCS Soil Conservation Service SMP Stormwater Master Plan

SSURGO Soil Survey Geographic Database

TCEQ Texas Commission on Environmental Quality

TR Technical Release

TWDB Texas Water Development Board TxDOT Texas Department of Transportation

URS Corporation (Acquired by AECOM in 2014)

USACE U.S. Army Corp of Engineers
USDA U.S. Department of Agriculture
WWTP Wastewater Treatment Plant

EXECUTIVE SUMMARY

The El Paso County Stormwater Master Plan (SMP) (hereafter referred to as the County SMP) is a continuation of the stormwater master planning efforts that were initiated with the City of El Paso SMP (hereafter referred to as the City SMP) which was originally completed in 2009. The City SMP addressed stormwater needs throughout the City. As the City master plan was being completed, El Paso County recognized that a similar effort was needed to address stormwater needs throughout the rest of the County.

The SMP was a joint effort and was originally funded by El Paso County, the Texas Water Development Board (TWDB), and El Paso Water (EPW). The SMP focuses on developed areas of El Paso County that had experienced flooding problems ranging from localized storms to the major floods of 2006. The master planning protocols that were developed for the City SMP were used as the basis for preparing the County SMP.

The original SMP was completed in August 2010. Public input was an important component of the SMP. Input was received from three public meetings, interviews with residents in the flood prone areas, and city and county officials. In addition to the public meetings, a series of technical working meetings were held with representatives from El Paso County, EPW, the City of Socorro, the Village of Vinton, and the TWDB.

This SMP represents an update to that original SMP, and was a joint effort funded by El Paso County and EPW. It includes updates to proposed projects included in the original SMP to account for changes in cost estimates and concept designs due to a) increases in average construction costs, b) new development that has occurred in the County since the original SMP was published, and c) new precipitation frequency estimates published in 2018 by the National Oceanic and Atmospheric Administration (NOAA) called Atlas-14. It also includes study of a new area of the County, the Montana Sector, which had not been included in the original SMP.

The County SMP has identified a total of 69 proposed projects totaling \$258,880,000 to address flooding issues throughout the county. Obviously, not all of these projects can be funded at one time so an effort was made to prioritize the projects. Representatives from El Paso County and EPW divided the projects into three tiers – Tier I (highest), Tier II, and Tier III. Within each tier the projects were ranked in descending order by benefit-cost ratio (BCR), or the estimated average annual cost of the project divided by the sum of the estimated average annual benefits. These prioritizations were not intended to be an absolute ranking of projects, but intended to provide the County and other officials with input for funding considerations for future stormwater projects. A table summarizing the prioritized projects is shown below.

Tier	Priority	Number of Projects	Total Cost
I	High	13	\$169,340,000
II	Moderate	14	\$55,580,000
III	Less	42	\$33,960,000
Total		69	\$258,880,000

It is important to recognize that these projects are needed to address existing drainage problems based on existing development. It is essential that future developments control stormwater flows so that they do not increase flooding.

A key element of the County SMP was identifying issues that have contributed to stormwater problems throughout the County. One of the overriding problems is that drainage issues often cross jurisdictional boundaries. It is not uncommon for a drainage flow path to begin in an unincorporated part of the County and pass from one city or village into another. Therefore, two to four different entities may be affected by a single flow path. Each of these entities may have its own drainage criteria, development criteria, construction permit requirements, and enforcement standards. If consistent drainage and development policies are not enforced throughout the County, flooding problems will increase. One of the recommendations from this SMP is that countywide stormwater policies be developed to ensure consistent drainage standards, development standards, and construction permits are enforced.

1.0 INTRODUCTION

El Paso County is situated in the Chihuahuan Desert in western Texas. The rainfall averages 10 inches annually, and residents enjoy approximately 300 sunny days in a typical year. The County is also subject to occasional hard rains during the summer monsoon season.

Beginning on July 31, 2006 and continuing through early August, a series of torrential rains hit the El Paso area causing flooding in many areas of El Paso and the surrounding communities. This series of rains is referred to as Storm 2006. Following this event, there was a recognition by many involved with the Storm 2006 response that additional data and analysis as well as a longer-term plan of action were required to have the means to address these complex drainage issues in a reasoned and cost-effective manner. Major efforts to address flood issues have since been underway including the completion of the City of El Paso Drainage Design Manual (DDM) (City of El Paso, 2008), and the City of El Paso Stormwater Master Plan (SMP) (hereafter referred to as the City SMP) (URS Corporation [URS] and Moreno Cardenas Inc. [MCi], March 2009). The DDM provides guidance and criteria to protect new development from negatively impacting the flood risk of downstream properties. The City SMP was created to evaluate the existing stormwater drainage system, identify problem areas, and develop a logical approach to upgrade the City's stormwater system.

Following the completion of the City SMP, a similar plan was proposed for selected areas prone to flooding in El Paso County. This plan was funded by the Texas Water Development Board (TWDB), El Paso County, and El Paso Water Utilities (EPW), with contract administered by EPW, and was completed in August 2010. In 2018 El Paso County proposed updating the SMP to include the Montana Sector, a previously unstudied area in the north-east corner of the County, as well as a restudy of the rest of the County to ensure that the SMP uses the best and most recent available data.

The selected watersheds in El Paso County are predominantly rural, but are experiencing an increase in development. As development in the County progresses, it will become increasingly important to have a comprehensive stormwater plan to not only address existing flooding issues, but to prevent future flooding issues that could arise from future unregulated development.

2.0 SCOPE OF MASTER PLAN

2.1 Stormwater Master Plan Overview

The study areas included in this master plan were selected based on data provided in the *Study of Rural Homesites Deemed at Risk of Flooding by 100-Year Flood* (El Paso County, 2007). This document identified locations with structures located in the Federal Emergency Management Agency (FEMA) regulatory floodplains. The focus of this SMP is to address specific flood prone areas identified in the above referenced report, as well as the Montana Sector of the County. These study areas include specific arroyos and flow paths shown on Figure 2-1. For the purposes of this report, they are referred to as:

- Vinton;
- Canutillo;
- Sparks Arroyo and Sub Basin A;
- Socorro;
- Hacienda Real;
- Fabens;
- Tornillo; and
- Montana Sector.

In addition to being identified based on data provided in the *Study of Rural Homesites Deemed* at *Risk of Flooding by 100-Year Flood* (El Paso County, 2007), the Sparks Arroyo and Sub Basin A Study Area was identified based on information provided in a feasibility study performed by the U.S. Army Corps of Engineers (USACE) for the County of El Paso, completed in February 2013.

Areas deemed at risk due to flooding by the Rio Grande were not evaluated in this SMP. Flooding issues of the Rio Grande fall under the jurisdiction of the International Boundary and Water Commission (IBWC).

The El Paso County SMP (hereafter referred to as the County SMP) was developed to:

- Estimate the stormwater runoff quantities;
- Evaluate major features of the existing stormwater drainage system;
- Identify components of the existing stormwater drainage system that are undersized;
- Estimate sediment loads;
- Recommend major stormwater drainage system improvements;
- Develop a general prioritization of recommended improvements; and
- Recommend countywide stormwater policies.

2.2 Technical Standards and Assumptions Impacting the Plan

The County SMP utilized the same standards and assumptions as the City SMP in order to maintain consistency in project definition and design. It has been prepared to the standards outlined in the City of El Paso DDM. The criteria outlined in the DDM describe standards that

are commonly used in the Southwest for evaluating risk and drainage infrastructure design and construction. Drainage structures are typically designed to handle a specific design storm, which is selected based on the desired level of safety and economic risk. The design storm utilized in the DDM is the 24-hour, 100-year storm, also called the 1 percent (%) storm. This is the storm that has a 1% chance of being equaled or exceeded in any given year. While some observers have interpreted this as a once in a lifetime event - and therefore an excessively conservative standard for evaluations and the basis of structural improvements - it is far from either. Rather, the 100-year storm is a statistical description of the probability of the event occurring in any one year based on historical rainfall measurements.

The use of the 100-year design storm is standard in flood evaluations and flood protection. It is the standard used by flood insurance providers, funding entities, and regulators in making many determinations. The County is well served by including the use of this standard in their planning and regulations. To not reflect this standard could be costly to the County on many levels.

Many of the areas studied in this document are currently rural or undeveloped. The analysis and resulting projects outlined in the County SMP are all based on the existing development conditions and do not account for future development. It is assumed that future development will be regulated by the County and local communities so that flood risk will not be increased. This is a very important concept and consistent with standard drainage design practices. However, it is incumbent on the County and communities involved to properly manage future development and enforce development regulations to ensure that these conditions are met.

2.3 Public Meetings and Technical Working Meetings

Three public meetings were held from 2009-2010 in the original master planning process to communicate the process, status, and results, and to solicit valuable input from the public in order to help focus ongoing analysis effort. The first public meeting was held in September 2009 to present the proposed study watersheds to be included in the County SMP and to gather input regarding existing flooding issues in these areas. The second public meeting was held in January 2010 to present the preliminary results of the hydrologic and hydraulic analysis and present potential projects to address the flooding issues. The third public meeting was held in May 2010 to present the draft County SMP including the selected project alternatives.

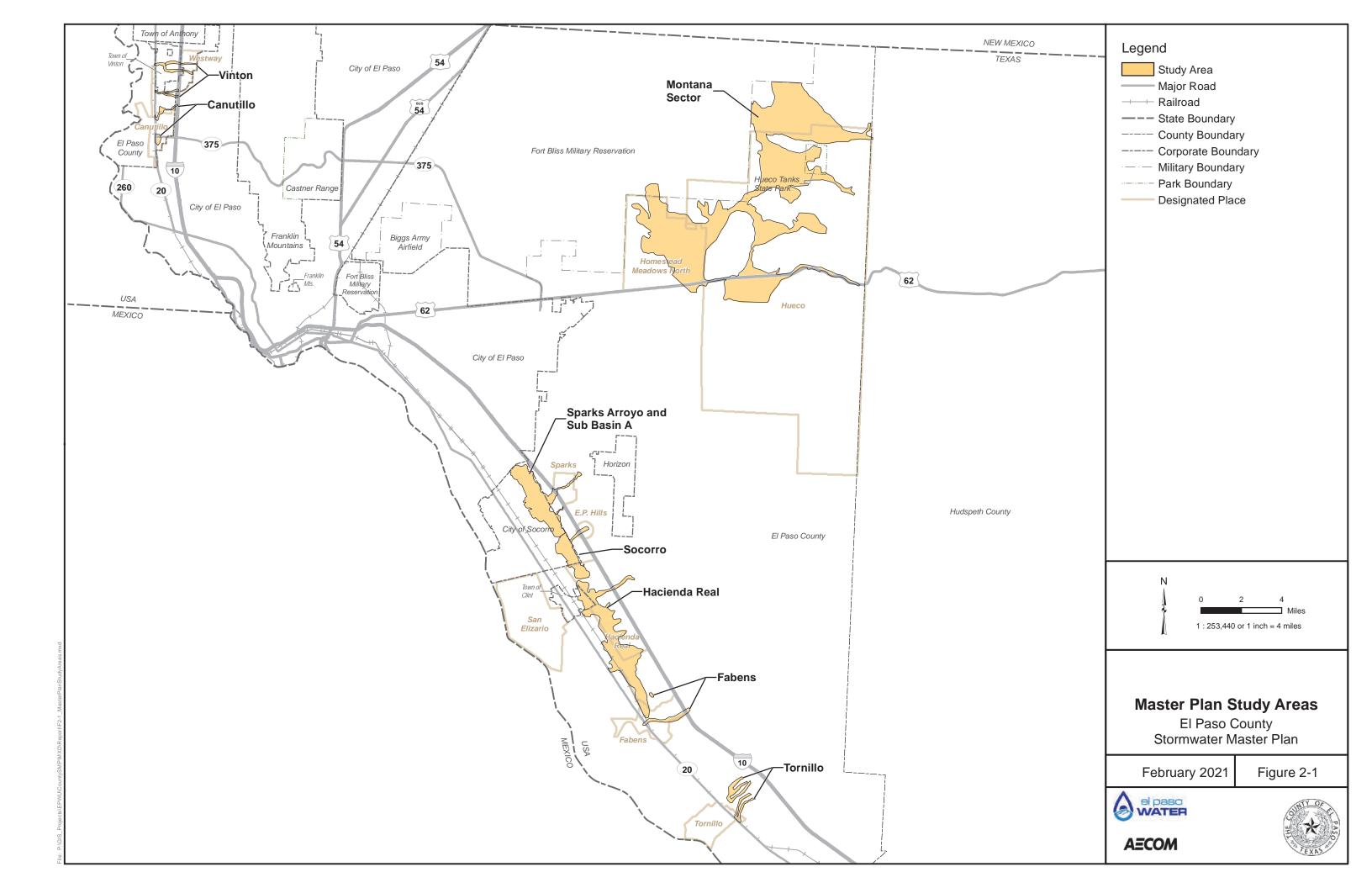
Three public meetings were held from 2019-2021 as part of the current update to the SMP, to serve the same general purposes as the original three public meetings. The first public meeting was held in November 2019 to present the proposed study watersheds for the Montana Sector to be included in the County SMP, to gather input regarding existing flooding issues in this area, and to present the approach for updating concept designs and cost estimates for projects included in the original SMP. The second public meeting was held in December 2019 to present the preliminary results of the hydrologic and hydraulic analysis and present potential projects to address the flooding issues in the Montana Sector, and to present the preliminary results of the benefit-cost analysis (BCA). The third and final public meeting will be held in January 2021 to present the draft County SMP including the selected project alternatives and proposed prioritization of projects.

Input from the public meetings helped guide the development of the Draft SMP and Draft updated SMP.

In addition to the public meetings, a series of working meetings were held with technical representatives from El Paso County, EPW, TWDB, City of Socorro, Village of Vinton, and El

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Paso County Water Improvement District No. 1. During these working meetings, alternatives were discussed and the final projects selected. These working meetings provided an excellent opportunity for the affected stakeholders to collaboratively develop a prioritized list of projects to address drainage issues throughout the County.



3.0 OVERVIEW OF DRAINAGE SYSTEMS

El Paso County has an arid, warm climate with hot, low-humidity summers and mild, dry winters. Average daily temperatures range from a high of 55 to a low of 33 degrees Fahrenheit (°F) in January and a high of 97°F to a low of 72°F in July. The mean annual precipitation is approximately ten inches with most of it occurring during July through September. While high intensity, short duration storms occur throughout the year, most of the high-volume, long duration storms in El Paso County that cause flooding in major drainage features consist of afternoon thunderstorms caused by the monsoonal flow from the Gulf of California during these summer months, and are typically limited in affected area.

The Franklin Mountains run from north to south, dividing eastern and western El Paso County, and range approximately 16 miles long and 5 miles wide with a general relief of over 3,000 feet above the surrounding area. The Vinton and Canutillo Study Areas are located in western El Paso County, downstream of the Franklin Mountains. The Hueco Mountains also run from north to south along the border between El Paso and Hudspeth Counties, and range approximately 16 miles long and 12 miles wide with a general relief of over 2,600 feet above the adjacent areas. The Montana Sector Study Area is located in north-east El Paso County, downstream of the Hueco Mountains. The remaining study areas included in the County SMP (Sparks Arroyo and Sub Basin A, Socorro, Hacienda Real, Fabens, and Tornillo) are located in southeastern El Paso County between an elevated mesa area and the flat Rio Grande Valley. It is at the downstream end of these elevation changes where flooding issues have arisen due to the high volumes of flow combined with erosive soils.

Throughout the County SMP, the eight study areas are discussed in order starting in the western part of the County, proceeding to the eastern part of the County:

- Vinton:
- Canutillo;
- Sparks Arroyo and Sub Basin A;
- Socorro;
- Hacienda Real;
- Fabens; and
- Tornillo; and
- Montana Sector.

An overview of the limits of the above study areas is shown on Figure 2-1.

3.1 Vinton Study Area

3.1.1 Site Topography

The Vinton Study Area is located on the northwest side of El Paso County, and runs through the Village of Vinton, as shown on Figure 3-1. The drainage features in this area include many natural arroyos and man-made earthen channels.

Many of the contributing watersheds are composed of three different drainage patterns; steep mountainous terrain, alluvial fan, and flat valley area. The flow begins in the steep terrain along

the west side of the Franklin Mountains. As the flow approaches the foothills, the slope of the land begins to flatten resulting in alluvial fans, which consist of less defined channels. As the flow continues downstream, it crosses Interstate Highway 10 (IH-10) through a series of culverts, to either man-made earthen channels or existing natural channels. Before reaching the Rio Grande, flow must be conveyed through a series of culverts under Doniphan Drive.

3.1.2 Site Surficial Geology

The areas within the Franklin Mountains, the foothills, and a portion of the residential areas consist of soils that are classified as hydrologic soil group D per U.S. Department of Agriculture standard classification. These soils are primarily clays at or near the surface causing low infiltration with high runoff potential. The residential areas close to the Rio Grande consist of soils that are classified as hydrologic soil group B. These soils have moderately fine to moderately coarse textures with moderate permeability.

3.1.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that a majority of the Vinton Study Area has not been developed. There are areas of high density residential development on the lower valley, between the Rio Grande and IH-10. In addition, there are areas of high density residential development east of IH-10, to the north and south of Westway Boulevard.

3.2 Canutillo Study Area

3.2.1 Site Topography

The Canutillo Study Area is located on the northwest side of El Paso County, south of the Village of Vinton, as shown on Figure 3-2. The drainage features in this area include many natural arroyos and man-made earthen channels.

Many of the contributing watersheds for the northern portion of the study area are composed of three different drainage patterns; steep mountainous terrain, alluvial fan, and flat valley area. The flow begins in the steep terrain along the west side of the Franklin Mountains. As the flow approaches the foothills, the slope of the land begins to flatten resulting in alluvial fans, which consist of less defined channels. As the flow continues downstream, it crosses IH-10 through a series of culverts to either man-made earthen channels or existing natural channels. Before reaching the Rio Grande, flow must be conveyed through a series of culverts under Doniphan Drive.

The contributing watershed for the southern portion of the study area is primarily composed of flat valley area. The flow entering the study area accumulates downstream of IH-10 and is conveyed through the watershed via residential streets. The flow enters a topographic depression at the downstream end of the watershed with no outfall to the Rio Grande.

3.2.2 Site Surficial Geology

The Franklin Mountains, the foothills, and a portion of the residential areas consist of soils that are classified as hydrologic soil group D. These soils are primarily clays at or near the surface causing low infiltration with high runoff potential. The residential areas close to the Rio Grande

consist of soils that are classified as hydrologic soil group B. These soils have moderately fine to moderately coarse textures with moderate permeability.

3.2.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that a majority of the Canutillo Study Area has not been developed. There are areas of high density residential and commercial development on the lower valley, between IH-10 and the Rio Grande. Currently, there is no significant development east of IH-10.

3.3 Sparks Arroyo and Sub Basin A Study Area

3.3.1 Site Topography

The Sparks Arroyo and Sub Basin A Study Area, shown on Figure 3-3 is located in southeast El Paso County. The drainage features in the area include several natural arroyos and the Mesa Spur Drain.

The contributing watershed is composed of three different drainage patterns: the mesa at the upstream end, the Sparks Arroyo and Sub Basin A Study Area valley at the downstream end, and the hilly arroyos that connect the mesa and the valley. The upstream mesa has relatively flat slopes of approximately 0.15%. Downstream of the mesa, the terrain becomes steeper (approximately 3%) with several natural arroyos conveying flows to the agricultural valley that is outlined in Figure 3-3 as the Sparks Arroyo and Sub Basin A Study Area. The flows from the arroyos are conveyed beneath IH-10 through a series of culverts before becoming less defined and spreading out to form an alluvial fan as they enter the Sparks Arroyo and Sub Basin A Study Area.

3.3.2 Site Surficial Geology

The mesa, located in the farthest upstream portion of the watershed, is comprised of soils classified as hydrologic soil group C. These soils are typically sandy clay loam. In the hilly arroyo areas separating the mesa and valley, the soil is classified as hydrologic soil group A. These soils have high permeability and are typically sand, loamy sand, or sandy loam. The flat agricultural valley located downstream of the hilly arroyos consists of soils that are classified as hydrologic soil group B. These soils have moderately fine to moderately coarse textures with moderate permeability.

3.3.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that a large portion of the Sparks and Sub Basin A Study Area has been developed. There are areas of high density residential development on the upper mesa, upstream of IH-10, and downstream of IH-10 in the central portions of the watershed. In addition, there are areas of high density residential development and commercial development along the western watershed boundary. There is a significant amount of commercial development adjacent to IH-10 and a small amount of residential development just upstream and downstream of the Mesa Spur Drain within the watershed.

3.4 Socorro Study Area

3.4.1 Site Topography

The Socorro Study Area, shown on Figure 3-4, is located in southeast El Paso County and is primarily agricultural in land use. The drainage features in this area include several natural arroyos and the Mesa Spur Drain.

The contributing watershed is composed of three different drainage patterns: the mesa at the upstream end, the Socorro Study Area valley at the downstream end, and the hilly arroyos that connect the mesa and the valley. The upstream mesa has relatively flat slopes of approximately 0.15%. Downstream of the mesa, the terrain becomes steeper (approximately 3%) with several natural arroyos conveying flows to the agricultural valley that is outlined in Figure 3-4 as the Socorro Study Area. The flows from the arroyos are conveyed beneath IH-10 through a series of culverts before becoming less defined and spreading out to form an alluvial fan as they enter the lower elevations of the Socorro Study Area. The Socorro Study Area is bound on the downstream edge by the Mesa Spur Drain.

3.4.2 Site Surficial Geology

The mesa, located in the farthest upstream portion of the watershed, is comprised of soils classified as hydrologic soil group C. These soils are typically sandy clay loam. In the hilly arroyo areas separating the mesa and valley, the soil is classified as hydrologic soil group A. These soils have high permeability and are typically sand, loamy sand, or sandy loam. The flat agricultural valley located downstream of the hilly arroyos consists of soils that are classified as hydrologic soil group B. These soils have moderately fine to moderately coarse textures with moderate permeability.

3.4.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that a majority of the Socorro Study Area has not been developed. There are areas of high density residential development on the upper mesa and upstream of IH-10 in the western portions of the watershed. In addition to these areas, there is a small amount of commercial development adjacent to IH-10 and a small amount of residential development just upstream and downstream of the Mesa Spur Drain within the watershed.

3.5 Hacienda Real Study Area

3.5.1 Site Topography

The Hacienda Real Study Area, shown on Figure 3-5, is located in southeast El Paso County and is primarily agricultural in land use. The drainage features in this area include several natural arroyos, as well as the Mesa Drain, and Salatral Lateral.

The contributing watershed is composed of three different drainage patterns: the mesa at the upstream end, the Hacienda Real Study Area valley at the downstream end, and the hilly arroyos that connect the mesa and the valley. The upstream mesa has relatively flat slopes of approximately 0.1%. Downstream of the mesa, the terrain becomes steeper (approximately 3%) with several natural arroyos conveying flows to the agricultural valley that is outlined in

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Figure 3-5 as the Hacienda Real Study Area. The flows from the arroyos are conveyed beneath IH-10 through a series of culverts before becoming less defined and spreading out to form an alluvial fan as they enter the lower elevations of the Hacienda Real Study Area. The Hacienda Real Study Area is bound on the downstream edge by the Mesa Drain and the elevated Salatral Lateral. Site inspection revealed that the Salatral Lateral presents a continuous boundary with no identified crossings or openings that would allow upstream flows to cross.

3.5.2 Site Surficial Geology

The mesa, located in the farthest upstream portion of the watershed, is comprised of soils classified as hydrologic soil group C. These soils are typically sandy clay loam. In the hilly arroyo areas separating the mesa and valley, the soil is classified as hydrologic soil group A. These soils have high permeability and are typically sand, loamy sand, or sandy loam. The flat agricultural valley located downstream of the hilly arroyos consists of soils that are classified as hydrologic soil group B. These soils have moderately fine to moderately coarse textures with moderate permeability.

3.5.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that a majority of the Hacienda Real Study Area has not been developed. There is an area of high density residential development on the upper mesa in the western portion of the watershed and some areas of low density development on the upper mesa in the central portion of the watershed. In addition to these areas, there is a small amount of residential development just upstream and downstream of the Northloop Drive within the watershed.

3.6 Fabens Study Area

3.6.1 Site Topography

The Fabens Study Area is located in southeast El Paso County, and runs through the Fabens community, as shown on Figure 3-6. The area is mostly undeveloped, although the Fabens community is composed of agricultural and residential lands. The drainage features include natural channels, the San Felipe Arroyo, the Salatral Lateral, the River Drain, and the Fabens Dam.

The contributing watersheds are composed of many different drainage patterns. The upstream ends of the watersheds begin in the mesa, a relatively flat area, with a slope of approximately 0.1%. The downstream end, known as the lower valley, is also a relatively flat area where the community of Fabens is located along with many of the agricultural lands. Between these two flat areas lies the escarpment area, which is composed of many natural well-defined channels with steeper slopes. Several earthen dams have been constructed within the watershed in an attempt to control flow as it travels downstream. The flow is conveyed through a series of culverts under IH-10 and continues to flow downstream through either natural channels or manmade earthen channels. There are only a few openings along the intricate system of canals and irrigation ditches within the lower valley that allow stormwater to flow and exit the system.

3.6.2 Site Surficial Geology

The upstream watershed is composed of soils classified as hydrologic soil group C. These soils are typically sandy clay loams. As the watersheds enter into the steeper more defined channel area, the soil is classified as hydrologic soil group A. These soils have high permeability and are typically sand, loamy sand, or sandy loam. In the downstream area, which is made up of agricultural and residential lands, the soil is classified as hydrologic soil group B. These soils have moderate permeability and have moderately fine to moderately coarse textures.

3.6.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that the majority of the Fabens Study Area has not been developed. There is an area of high density residential development within the town of Fabens near the downstream portion of the San Felipe Arroyo. There is no other significant development within this study area.

3.7 Tornillo Study Area

3.7.1 Site Topography

The Tornillo Study Area, shown on Figure 3-7, is located in southeast El Paso County and runs through the town of Tornillo. The drainage features in this area are natural channels.

The contributing watershed is composed of hilly arroyos with a relatively constant slope of approximately 2%. Flows crossing IH-10 are conveyed through a series of culverts as they continue downstream through natural channels. As the flow reaches the residential areas, the channels become less defined and the flow begins to disperse, traveling along the path of least resistance.

3.7.2 Site Surficial Geology

The upstream watershed is composed of soils classified as hydrologic soil group C. These soils are typically sandy clay loams. The majority of the watersheds are located in an area where the soil is classified as hydrologic soil group A. These soils have high permeability and are typically sand, loamy sand, or sandy loam.

3.7.3 Residential/Commercial Development

Based on field reconnaissance gathered from site visits and the 2008 Orthophotography (El Paso County, 2008), it appears that a majority of the Tornillo Study Area has not been developed. There is a small area of low density residential development in the lower portions of the watershed, along the southern boundary. In addition to this area, there is a very small amount of commercial development in the central portion of the watershed. In addition to the currently developed areas, a new port of entry is expected to be built in the near future. The new port of entry will result in a roadway that connects IH-10 to the US/Mexico border. The roadway is expected to cross the northernmost channel, along with the two channels located directly south. The channels in this area, which are currently unnamed, will be known from north to south in this study as High School Channel, South High School Channel, and Flow Path T.

3.8 Montana Sector Study Area

3.8.1 Site Topography

The Montana Sector Study Area, shown on Figure 3-8, is located in northeast El Paso County and includes the unincorporated residential neighborhoods of Butterfield and Homestead Meadows. The drainage features in this area are natural channels.

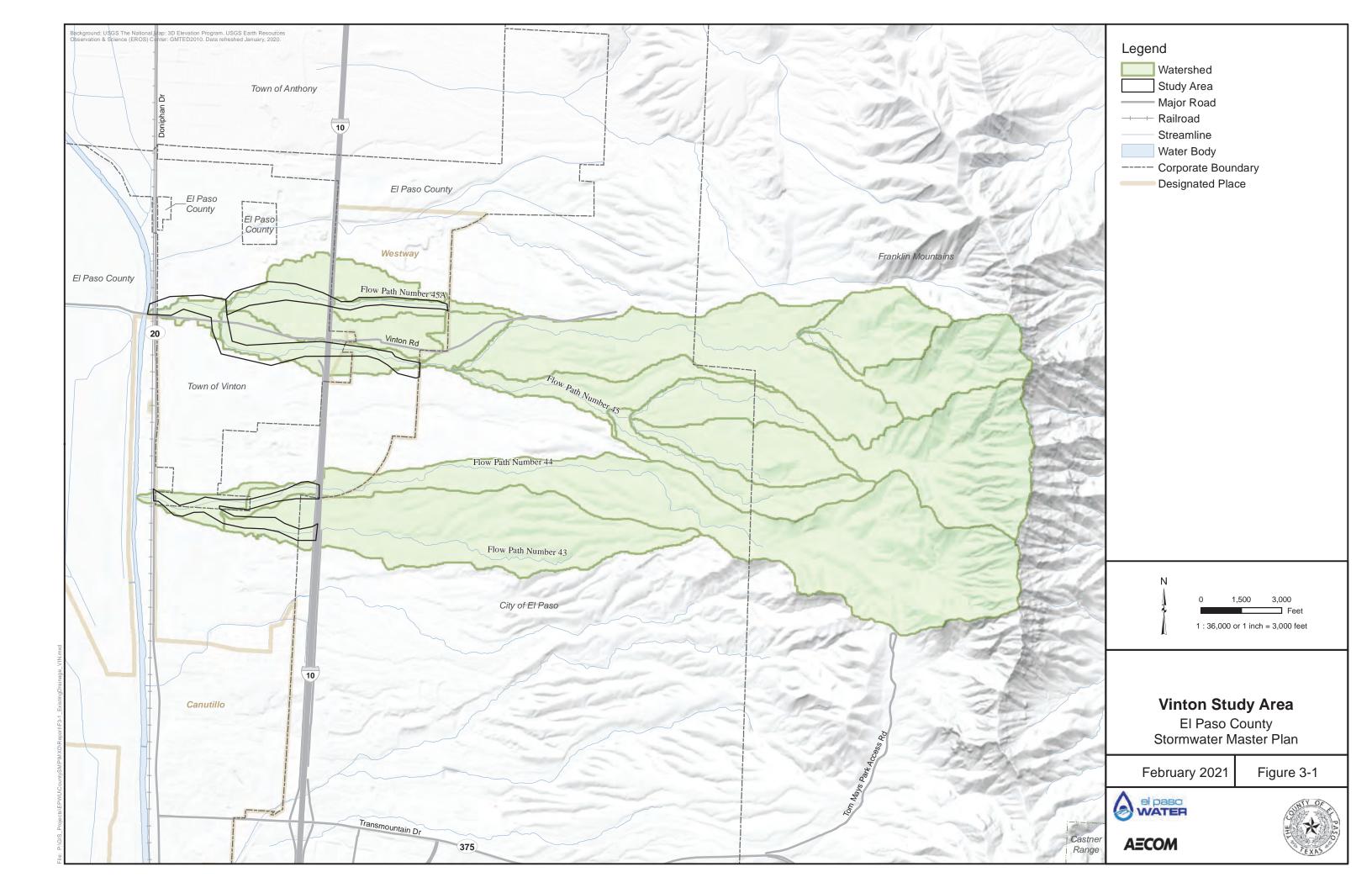
The contributing watershed is composed of hilly arroyos on the western slopes of the Hueco Mountains. As the flow reaches the residential areas, the channels become less defined and the flow begins to disperse, traveling along the path of least resistance, until the channels disappear altogether in large natural depressions.

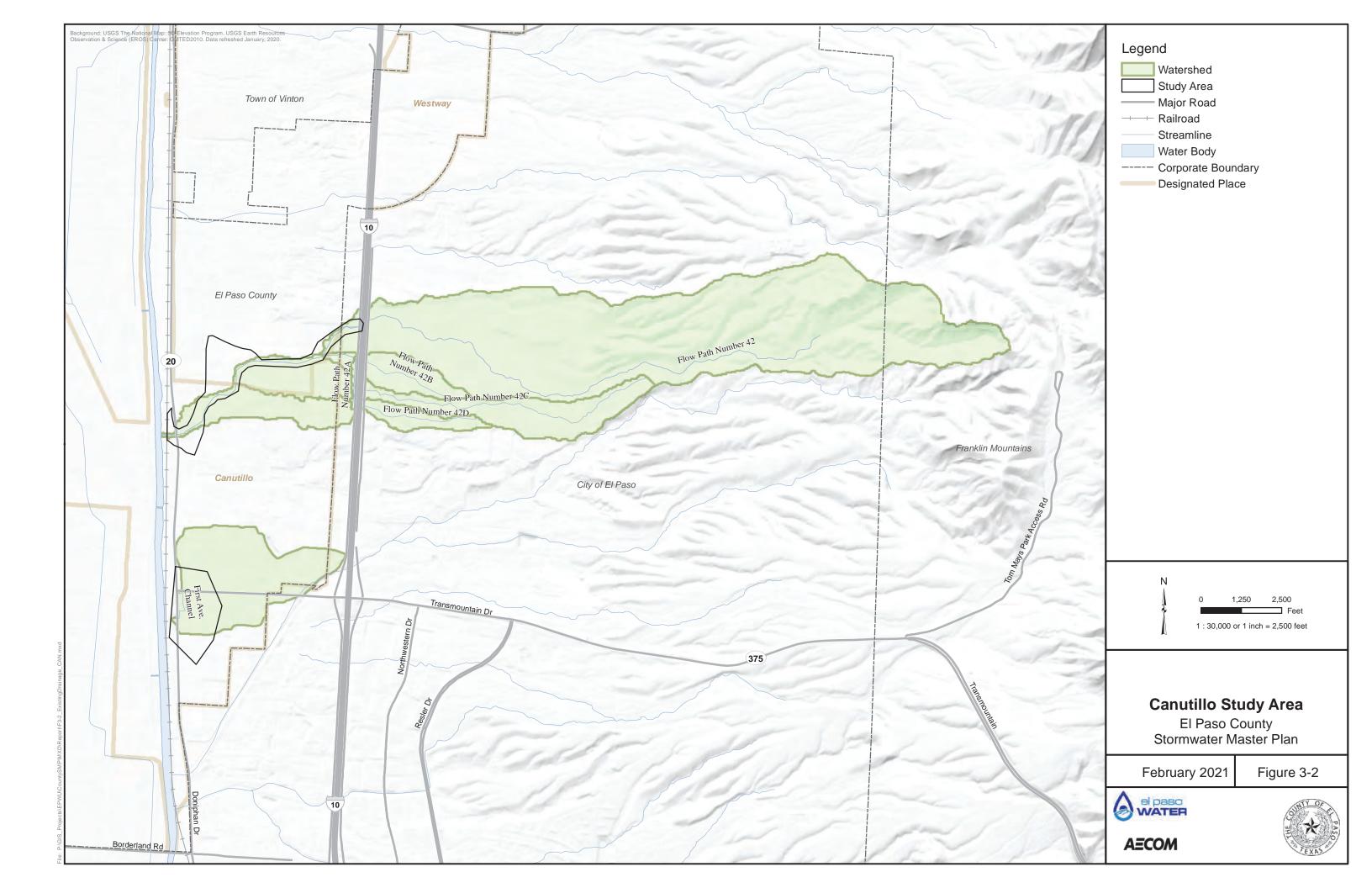
3.8.2 Site Surficial Geology

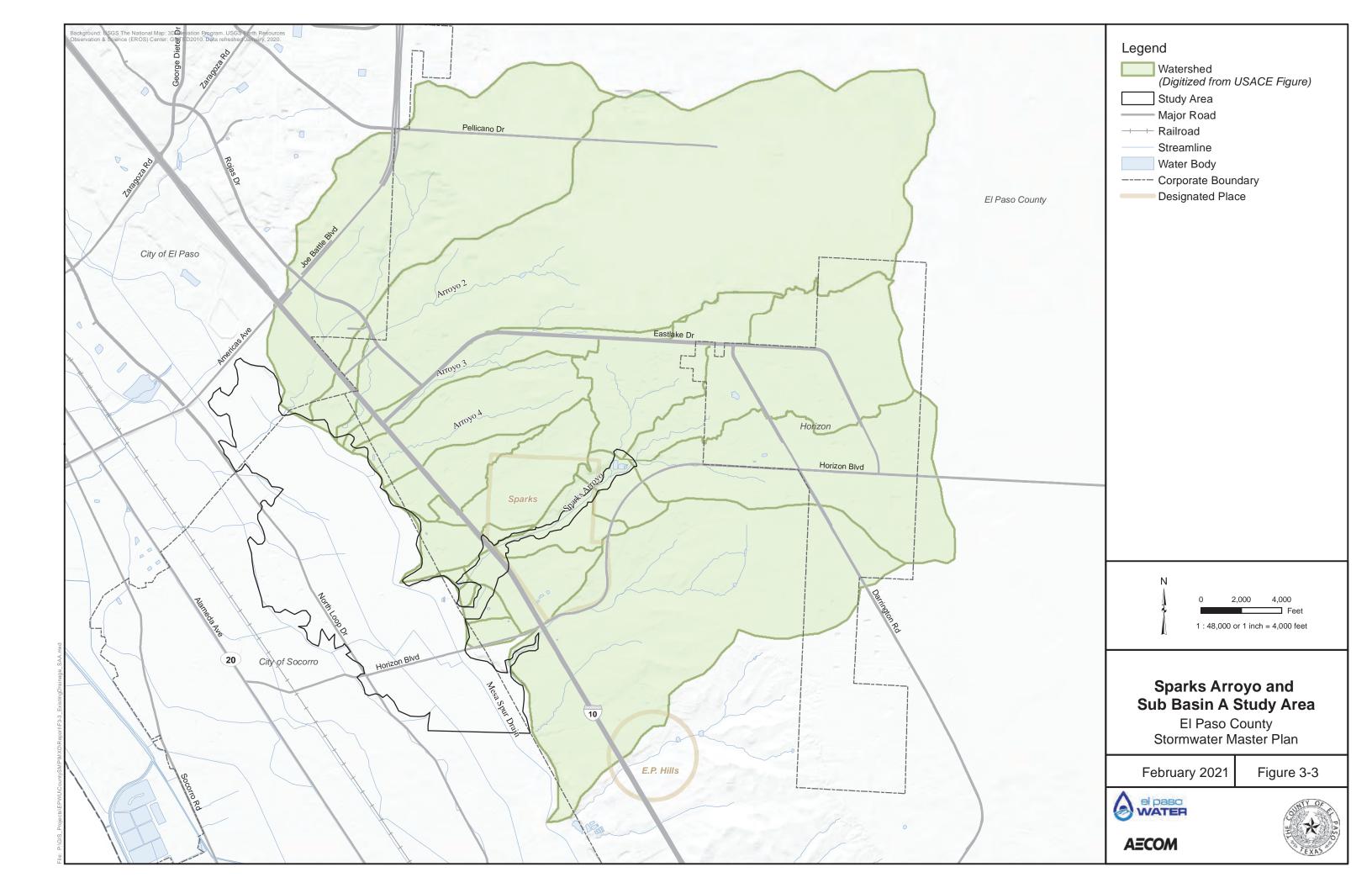
The upstream watershed is composed of soils classified as hydrologic soil group D. These are typically rock outcroppings. The lower ends of the watersheds are located in flatter areas where the soil is classified as hydrologic soil group A, which have high permeability and are typically sand, loamy sand, or sandy loam, or hydrologic soil group C, which are typically sandy clay loams.

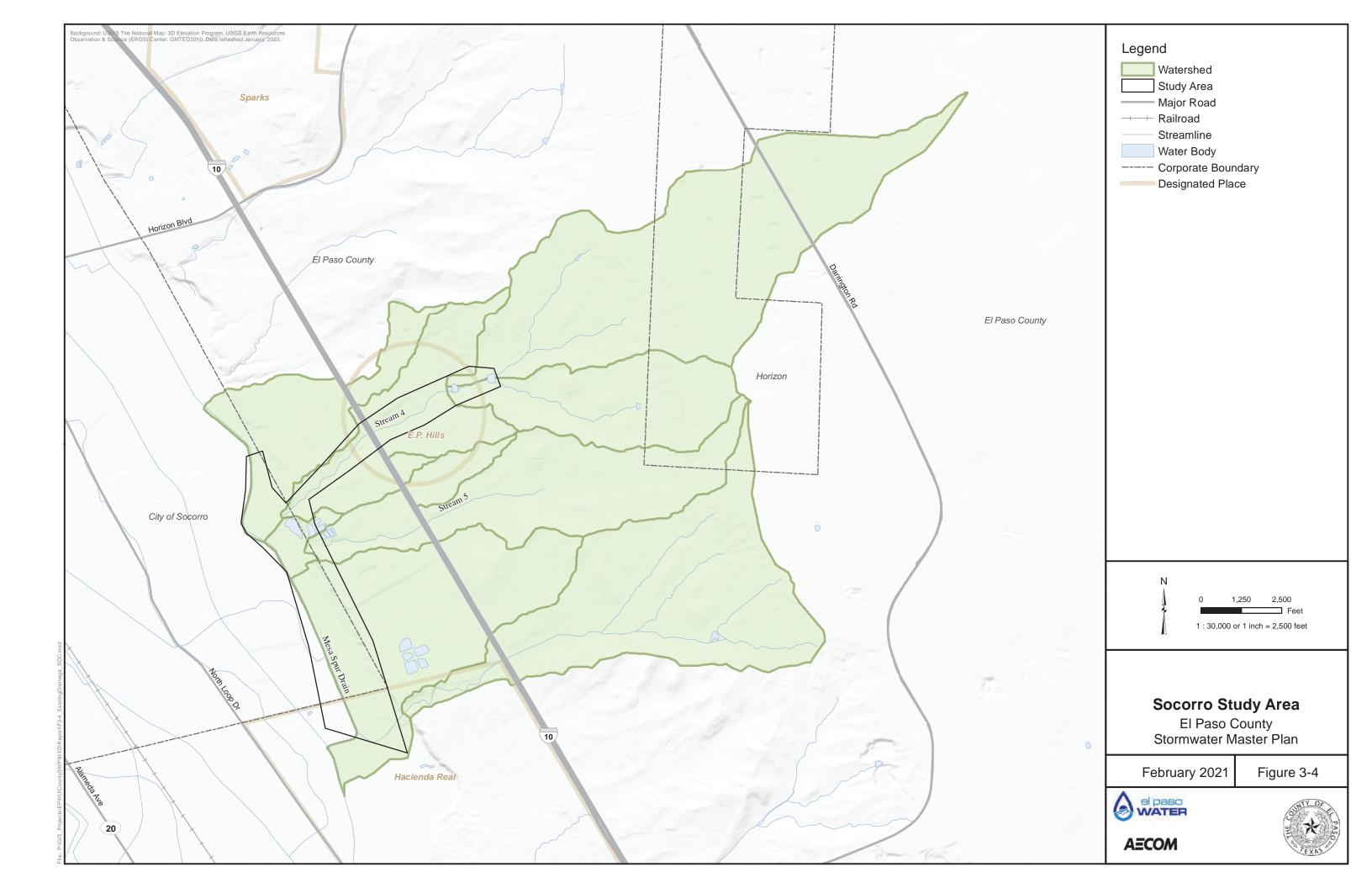
3.8.3 Residential/Commercial Development

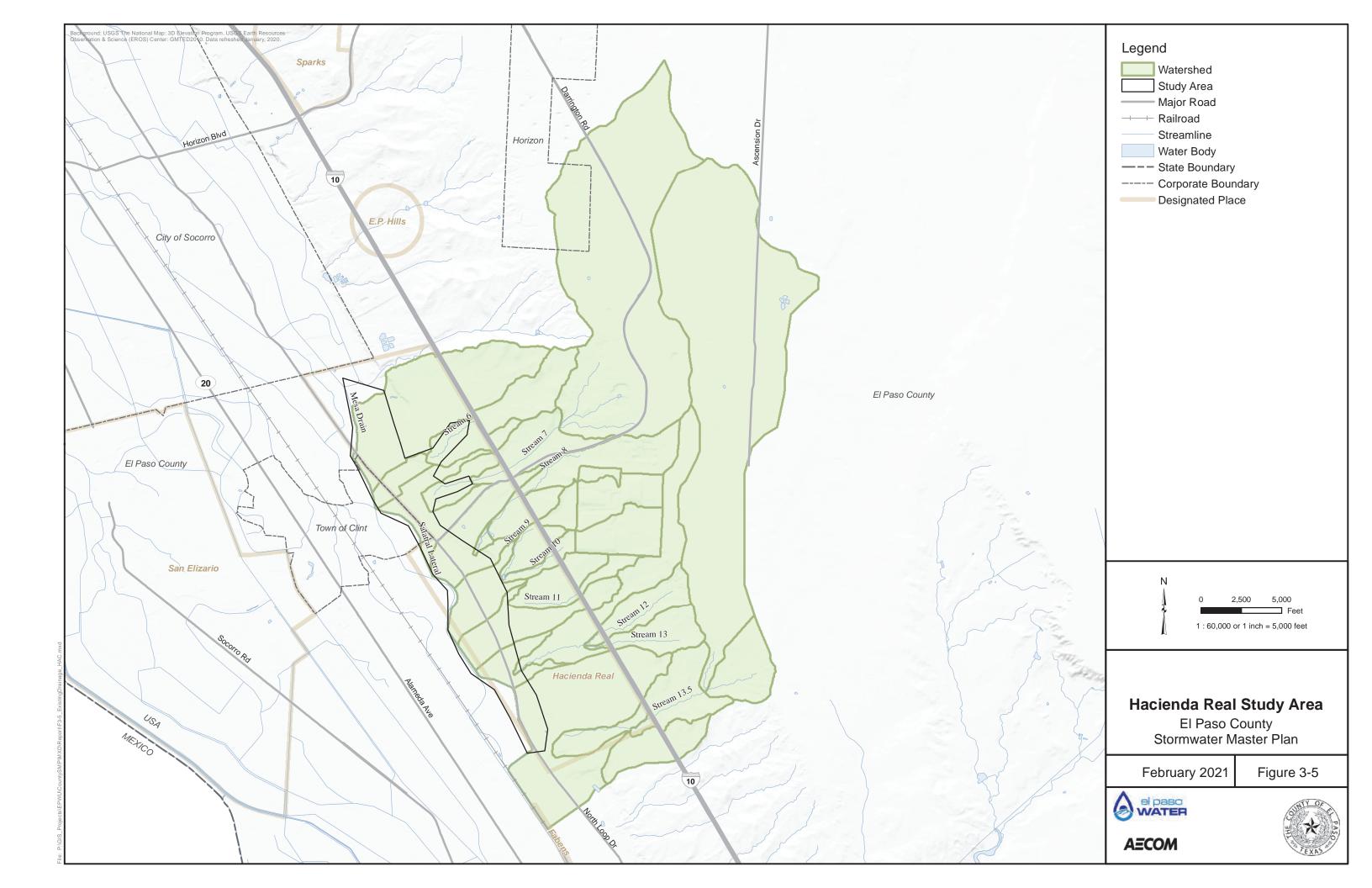
Based on field reconnaissance gathered from site visits and aerial photography, it appears that a majority of the Montana Sector Study Area has not been developed. There is a small area of low-density residential development immediately to the west and north of Hueco Tanks State Park, and another north of Marvin Avenue, which forms the southern boundary of the Montana Sector, and east of Fager Street. There is also a small amount of commercial development along Montana Avenue (US Highway 62) that runs across the southern portion of the study area.

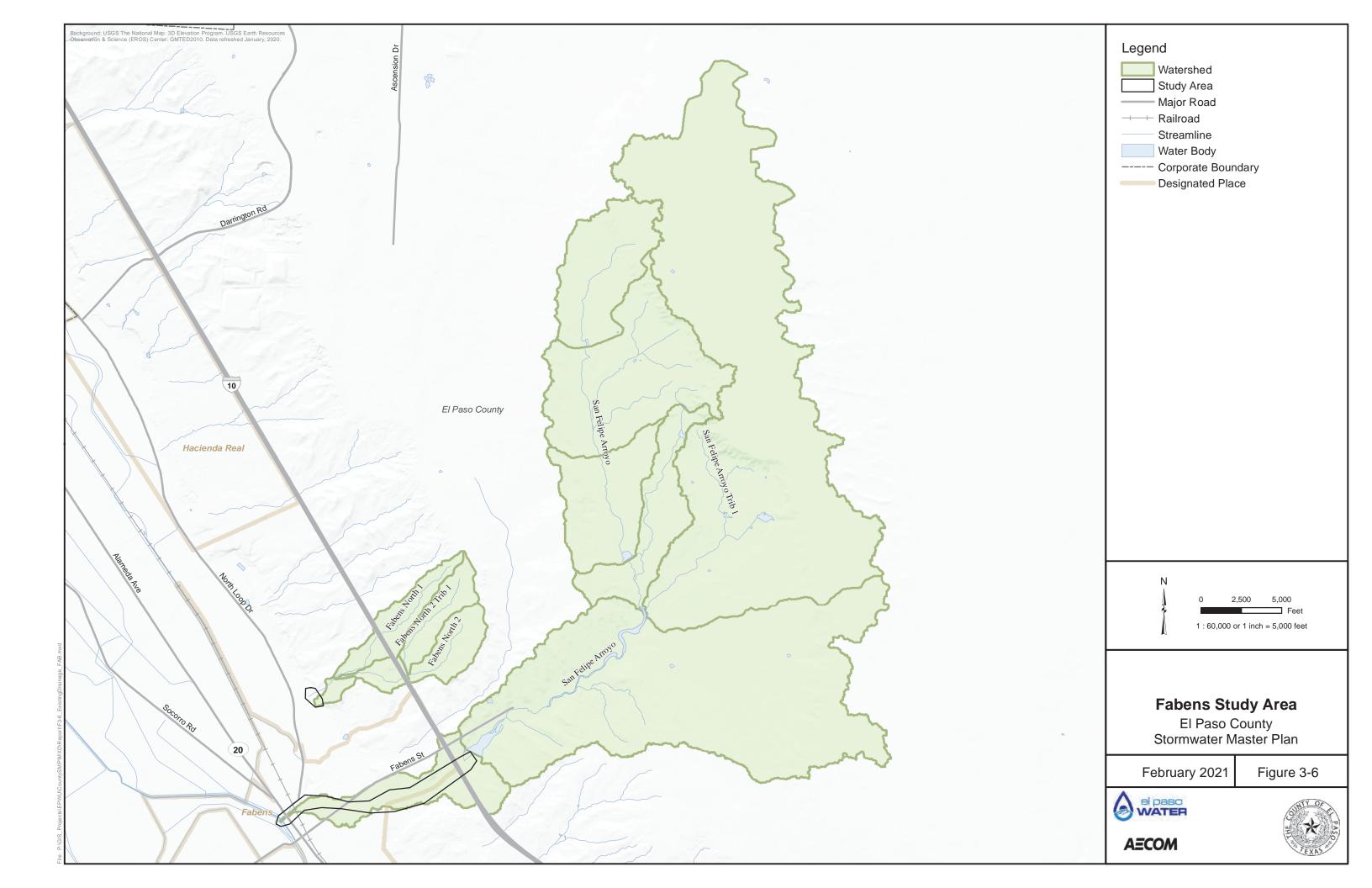


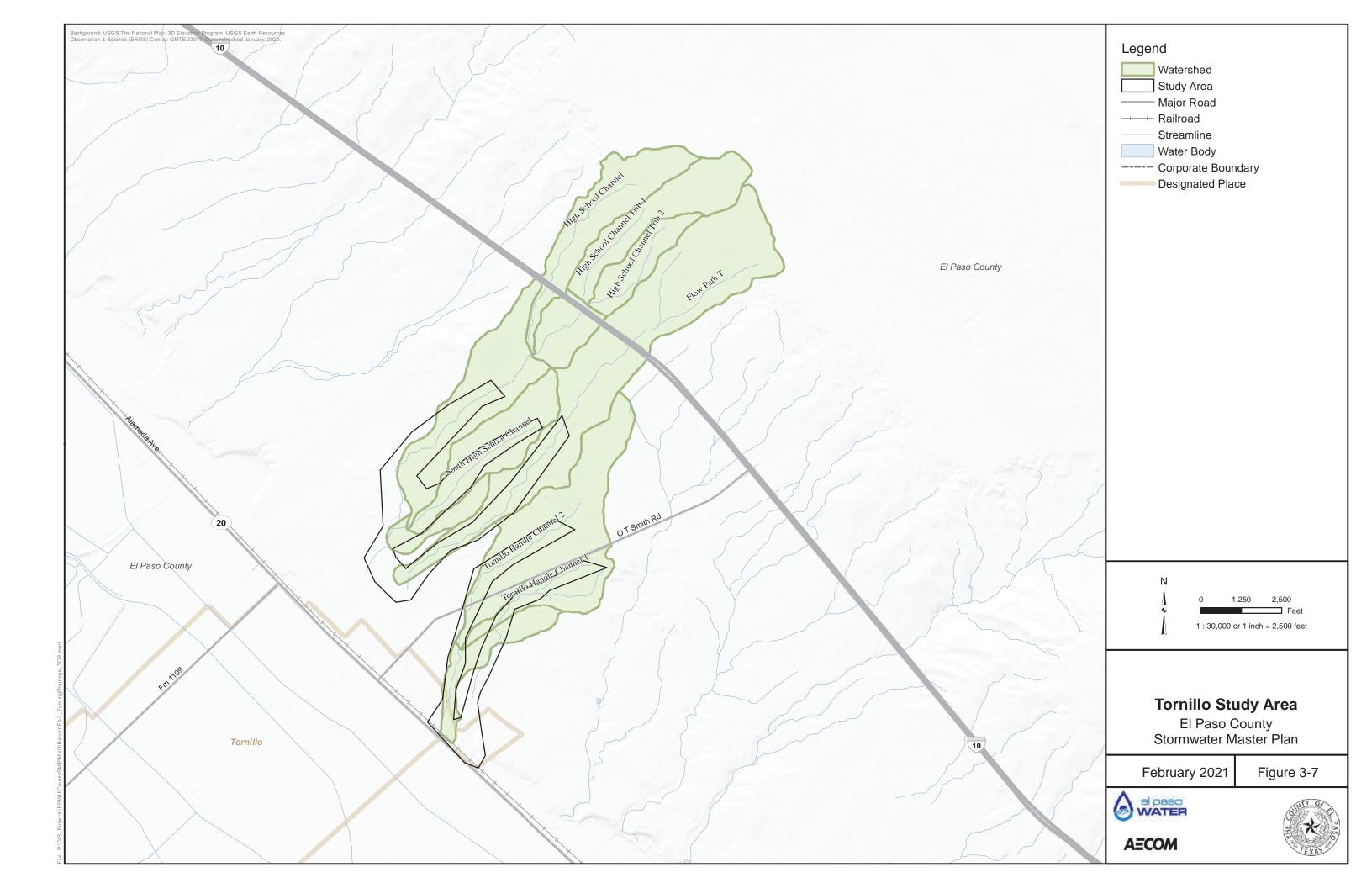


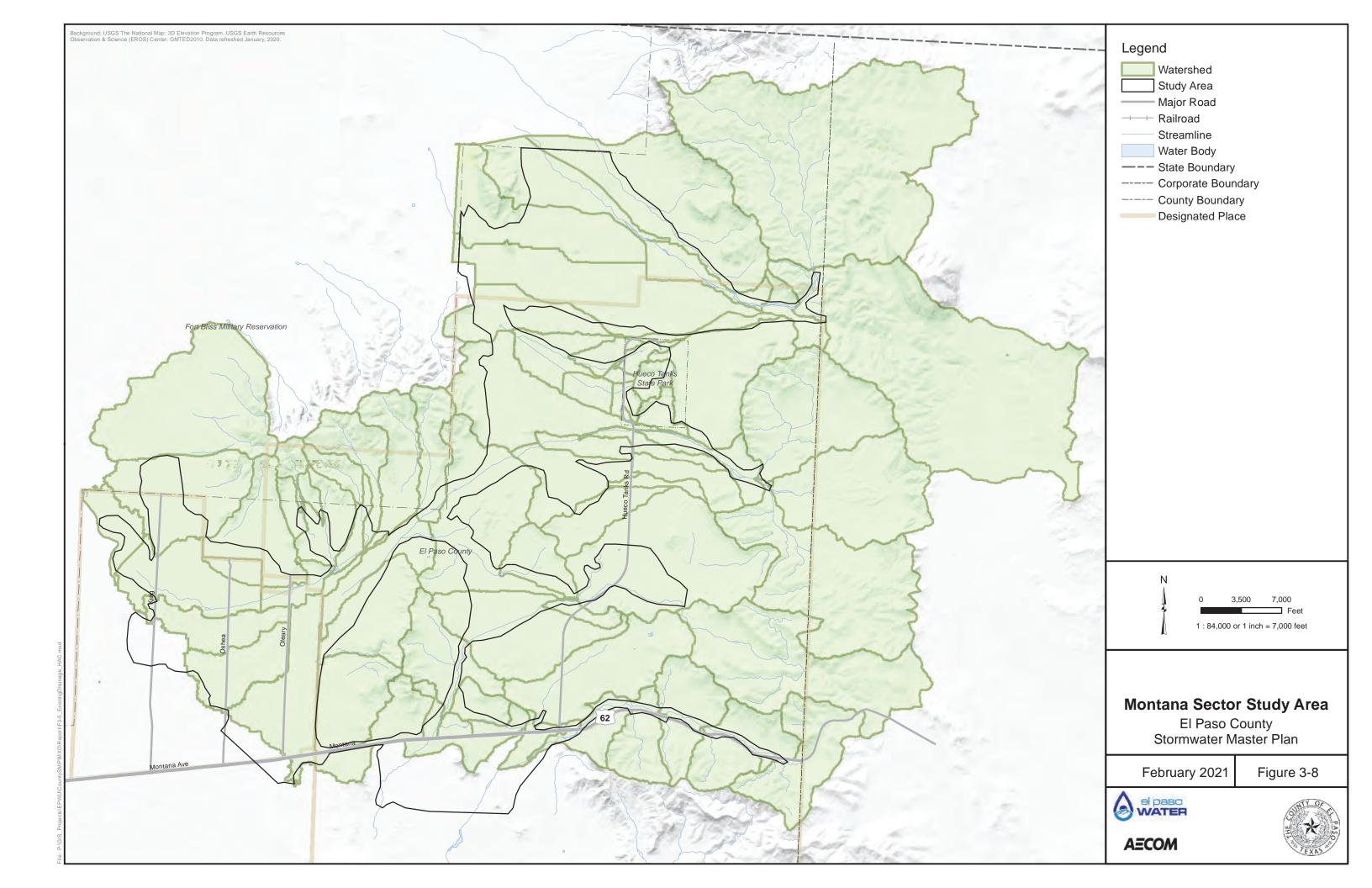












4.0 MASTER PLAN METHODOLOGY

Several areas of El Paso County experience flooding problems on an annual basis. Other areas experience flooding only during significant rainfall events. The study areas included in this master plan were selected based on the data provided in the *Study of Rural Homesites Deemed at Risk of Flooding by 100-Year Flood* (El Paso County, 2007). This document provides mapping of regulatory FEMA floodplains and identifies structures that currently lie within these floodplains. Areas with a significant number of structures shown to be at risk of flooding by the 100-year flood were selected as the initial study areas for this plan. Based on initial meetings with the County as well as site visits, a more specific list of problem areas was created.

Watershed delineations were generated for these problem areas based on available topographic information. The watershed boundaries were used in the hydrologic analysis, which led to the analysis of the 100-year storm. Discharge hydrographs were developed for the existing development conditions found within the County at the time of this analysis.

Based on the hydrologic analysis, the existing drainage system was evaluated for conveyance capacities. These capacities were based on data gathered from a variety of sources. Hydrologic and hydraulic evaluations were performed in accordance with the City of El Paso DDM.

In general, the approach to evaluating the identified El Paso County Study Areas' existing drainage system included the following steps:

- Review the existing data available to be used in this study, including existing studies and plans;
- Divide the major watersheds developed from earlier studies into sub-watersheds at identified problem areas, as well as any major crossings or other significant drainage features;
- Determine the watershed hydrologic properties;
- Supplement available data with field reconnaissance;
- Determine the geometric properties of the drainage features from available data;
- Develop the hydrologic modeling in order to estimate discharge hydrographs and runoff volumes;
- Evaluate the existing system conveyance capacities;
- Identify system inadequacies;
- Develop conceptual alternatives to improve system performance and minimize potential flooding and flood damages;
- Evaluate the conceptual alternatives; and
- Select the preferred alternative.

The Sparks Arroyo and Sub Basin A Study Area was analyzed as part of a USACE feasibility study. For this study area, information from the USACE analysis was used where available. The following steps were involved in the evaluation of the Sparks Arroyo and Sub Basin A Study Area:

- Review data provided by the USACE relating to the analysis of the study area;
- Review data provided by the USACE related to the recommended improvements;
- Perform approximate hydrologic and hydraulic analysis to generate additional data required to develop and evaluate improvements per the methods used in this County SMP; and
- Develop and evaluate improvements per the methods used in this County SMP.

The County SMP did not include validation of regulatory FEMA floodplains or formal delineation of new floodplains in currently unmapped areas of the County. This study is a planning document and does not guarantee that identified solutions without further detailed definition will lead to removal of flood prone areas from designated floodplains or flood zones.

4.1 Review of Historical Flooding and Prior/Ongoing Studies

Multiple data sources were used to determine where historical flooding problems occurred and to identify potential solutions. Valuable input and information was received from:

- El Paso County Staff;
- EPW Staff;
- Public during Public Meeting Number (No.) 1;
- Local Residents during field visits;
- Mayor of Socorro;
- City Manager from Socorro;
- Representatives from Vinton;
- Public during Public Meeting No. 2; and
- USACE.

This information was complied at the onset of the project and was continually evaluated and updated throughout the master planning process. In addition, the following specific information was received:

Report	Date	Author	Description
Interviews with El Paso County	2009	URS	Interviews were conducted with engineering and maintenance personnel to help in identifying problem areas, the causes of the problems, and possible solutions.
Interview with Matt Dyer from Parker, Smith, & Cooper, Inc. (PSC) to discuss Clint Landfill drainage scenario	2009	PSC	PSC provided an exhibit with watershed delineations, as well as retention pond locations and storage volumes.
Interview with Halff Associates to discuss ongoing Clint Landfill analysis	2009	Halff Associates	Halff Associates discussed the status of an ongoing analysis of the Clint Landfill area. The study completion date was behind the schedule for the production of this County SMP.

Report	Date	Author	Description
Study of Rural Homesites Deemed at Risk of Flooding by 100-Year Flood	2007	El Paso County	This report details areas of El Paso County with structures shown to be at risk by the 100-year FEMA Regulatory Floodplain.
Sparks Arroyo Flood Control Project	2013	USACE	This feasibility study and other associated documents produced and provided by the USACE identify problem areas within the Sparks Arroyo and Sub Basin A Study Area, provide information on the hydrologic analysis performed, provide potential improvements as solutions to the identified problems, and provide estimated costs for each of the improvements.

4.1.1 Vinton Study Area

As part of the City SMP, Flow Path Number 45 and Flow Path Number 45A were studied and improvements were recommended. The information and recommendations put forth within the City SMP were incorporated into the County SMP.

4.1.2 Canutillo Study Area

The IBWC conducted a study called, *Development of Alternatives for Canutillo Flood Control Improvements*, *Rio Grande Canalization Project* in February 2007. The purpose of the analysis was to provide flood control improvement alternatives along the Rio Grande for the town of Canutillo. URS evaluated the alternatives and determined that many of the alternatives involved improving the levee along the Rio Grande. Alternatives to improve the levee were not considered within the purview of the County and not included in this study.

FEMA conducted an update of the Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS) for El Paso County in 2006. Since that time, a Letter of Map Revision (LOMR) has been approved for the portion of Flow Path Number 42 that runs through Canutillo Heights and a Conditional Letter of Map Revision (CLOMR) has been approved for the portion from Los Mochis to IH-10. The hydrologic and hydraulic analyses that were completed as part of these revisions utilized the Hydrologic Engineering Center-Hydrologic Modeling System (HEC-HMS) and the Hydrologic Engineering Center-River Analysis System (HEC-RAS), respectively. The hydrologic and hydraulic analyses were obtained, as they are applicable to portions of the Canutillo Study Area. The revised hydrologic analysis results were incorporated into the hydraulic model and the channel was analyzed accordingly.

4.1.3 Sparks Arroyo and Sub Basin A Study Area

The USACE conducted a feasibility study for the Sparks Arroyo and Sub Basin A Study Area in 2013. The study consisted of a discussion of problem areas, a hydrologic analysis for the watersheds contributing to these problem areas, development of potential improvements, and conceptual design and costing of the improvements. AECOM coordinated with the USACE to obtain as much information as possible from this study and utilized the information to develop potential improvements using a method consistent with what was done for the rest of the County

SMP. The developed improvements are similar to, but in some cases with substantial differences to, the USACE improvements. These projects were included in the County SMP and evaluated with the other projects.

In 2019 the City of Socorro constructed a new retention basin downstream of the Sparks Arroyo, approximately 1,700 feet north-west of the intersection of Horizon Blvd and Thunder Rd. This basin provided floodwater and debris protection from the Sparks Arroyo for residential and agricultural land to the south. Dimensions of this basin were estimated from a site visit in November 2019 and the benefits were included in the analysis of the Sparks Arroyo and Sub Basin A Study Area.

4.1.4 Socorro Study Area

AECOM is unaware of any ongoing or prior drainage studies relating to the Socorro Study Area.

4.1.5 Hacienda Real Study Area

Parkhill, Smith & Cooper Inc. (PSC) analyzed several of the ponds located on the City of El Paso Landfill property near Clint. For these ponds, PSC was able to provide valuable information regarding watershed delineations and run-off detention design. The watershed delineations and storage volumes provided by PSC were incorporated into the hydrologic analysis for the Hacienda Real Study Area.

The City of El Paso recently purchased land for the purpose of expanding the Landfill near Clint. This land covers the flow path that drains a watershed of approximately 5.3 square miles, including an area well suited for a potential drainage basin to protect areas downstream of this watershed. The City of El Paso was consulted in 2019 regarding the potential for stormwater infrastructure in this area, and their input was included in the analysis for the Hacienda Real Study Area.

4.1.6 Fabens Study Area

FEMA conducted an update of the FIRMs and FIS for El Paso County in 2006. As part of this update, a hydrologic and hydraulic analysis was conducted on the San Felipe Arroyo. It was determined that the FEMA hydrologic analysis did not include the dams within the upper reaches of the San Felipe Arroyo Watershed and that it would not be applicable to this SMP. The hydraulic analysis, conducted using HEC-RAS, was determined to be applicable, and was modified to reflect the revised hydrologic analysis findings.

4.1.7 Tornillo Study Area

AECOM is unaware of any ongoing or prior drainage studies relating to the Tornillo Study Area.

4.1.8 Montana Sector Study Area

FEMA is currently conducting an analysis of floodplains in the Montana Sector. Preliminary hydraulics models were received from FEMA and information from these models were consulted and incorporated into this SMP.

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4.2 Hydrology

The purpose of the hydrologic analysis was to estimate runoff hydrographs and volumes that were used to evaluate capacities of the existing facilities as well as size proposed facilities. In general, the hydrologic analysis performed as part of this SMP utilized the Unit Hydrograph Method as outlined in the DDM. Detailed information regarding the hydrologic analysis and the results of the analysis can be found in Appendix A.

Hydrologic analysis for the Sparks Arroyo and Sub Basin A Study Area was performed by the USACE as part of a feasibility study. Data from the USACE hydrologic analysis were used to develop projects in this study area.

In 2018 NOAA published Volume 11 of the Precipitation-Frequency Atlas of the United States (Atlas-14), which included new depth-duration-frequency curves for the State of Texas. These curves showed an increase in 100-year 24-hr depth of approximately 7%-37% in the El Paso area. In December 2019 AECOM performed an analysis for the City of El Paso using independent gauge data, which confirmed the validity of Atlas-14 data for the study areas included in this SMP. Thus, Atlas-14 was used in all hydrologic analyses herein.

4.3 Hydraulics

The purposes of the hydraulic analysis were to evaluate capacities of existing structures, to size proposed structures, and to estimate the benefits of proposed structures and structure improvements. The level of detail available for characterizing hydraulic capacity of existing structures varied across the County, from areas where a FEMA detailed study had been previously performed (with associated surveyed cross-sections and structures) to areas where structural dimensions and elevations were estimated by field measurements. The hydraulic designs of proposed structures were dependent upon the level of detail of the available information, but are consistent with the planning level of this County SMP.

Special 2D hydraulic models were developed using HEC-RAS software Version 5.0.7. These 2D models were built using best available topographic data and measurements taken from a site visit performed by AECOM in November 2019. Topographic data was generally based on LiDAR taken in 2014, but this did not cover all portions of the Montana Sector. Where not available, LiDAR was supplemented with a topographic surface developed by TxDOT in 2015 using photogrammetry.

Detailed information regarding the hydraulic analyses inputs, methods, and results can be found in Appendix B.

4.4 Working Meetings

Throughout the master planning process, technical input was received from El Paso County, EPW, and key stakeholders during a series of four working meetings. The working meetings included the following stakeholders:

- El Paso County;
- EPWU;
- The City of Socorro;
- The Village of Vinton;

- The El Paso County Water Improvement District No. 1; and
- TWDB.

The initial working meeting included a discussion of the selected study areas and the technical approach for the stormwater master planning process. County personnel helped to identify critical flooding features located in each study area, and accompanied URS staff on field visits to each study area. The second working meeting was held after initial modeling results were completed and focused on discussion of identified problems, potential projects, and the path forward.

The third and fourth working meetings included stakeholders listed above and focused on detailed discussions of proposed project alternatives, including selection of alternatives and initial prioritization of projects.

As part of the current update to the SMP, a fifth working meeting was held to revisit the original SMP and discuss updates that were needed, including a discussion of several of the potential projects included in the original SMP individually. A sixth working meeting was held to select proposed project for the Montana Sector.

A seventh working meeting was conducted with The El Paso County Water Improvement District No. 1 (EPCWID) to collect feedback on proposed projects and proposed project improvements, and to discuss refined of project cost estimated. An eight working meeting was conducted to individually discuss projects from the original SMP not discussed in the fifth working meeting.

A ninth working meeting was conducted with El Paso County staff to discuss the proposed update to the prioritization methods.

4.5 Problem Area Definitions

Problem areas were defined within each study area based on information provided by the County, information gathered at the public meetings, field reconnaissance, and the hydrologic and hydraulic analysis performed as part of this SMP, and information from previous studies. Areas currently experiencing flooding and areas at risk for potential flooding were identified as problem areas. In some cases, multiple flooding issues were combined into a single problem area. The problem areas identified were discussed during the second working meeting and agreed upon by the parties present.

4.6 Development of Project Alternatives

For each problem area defined, multiple alternatives were identified to address the issues associated with the problem area. However, for problem areas with a clear solution only one alternative was carried forward. These alternatives were developed with input from the County. Each project alternative consisted of proposed improvements designed to meet the 100-year storm criteria whenever possible. Improvements considered include:

- Adding or improving detention/retention;
- Adding sediment and or debris control;
- Improving channel and crossing capacity; and
- Building new channels and storm drains.

Each developed alternative consisted of a series of individual improvements. Sizing of the improvements was based on the hydrologic and hydraulic analyses performed as part of this County SMP. Cost estimates for each alternative were developed. Cost estimates included the costs associated with the structure improvements as well as excavation and grading, demolition, possible utility relocations, right-of-way (ROW) acquisitions, and repaving as applicable. The costs developed for each improvement were then summed to develop a total project cost. The total project cost was then used for evaluation of each alternative. All costs are based on estimates effective November 2019. The methodologies used for concept design and cost estimation of alternatives are described in Appendix C.

Some potential projects within the Vinton Study Area were developed by URS as part of the City SMP, and at the request of the County and EPW were incorporated into the County SMP.

Additionally, a number of potential projects in the Sparks Arroyo and Sub Basin A Study Area were identified as part of a feasibility study performed by the USACE. The project locations and general concepts incorporated into this SMP are consistent with the USACE feasibility study, but the conceptual designs and cost estimates do not reflect USACE designs. The conceptual designs and cost estimates for these projects were developed using methods consistent with design criteria used for the rest of the County SMP.

4.7 Alternatives Evaluation

Table C-6 in Appendix C provides a listing of each alternative and its associated estimated construction cost. Tables C-2 through C-5 list the principal improvement components of each alternative.

4.8 Alternatives Selection

Working Meeting No. 3 was held to review and discuss the various alternatives for each project. The meeting included representatives from El Paso County, the City of Socorro, the Village of Vinton, and EPW. URS presented the various options and provided technical input to the meeting participants. Representatives from TWDB attended the meeting as observers. During the meeting the attendees:

- Discussed the basic issue to be addressed by each project;
- Discussed each alternative for a project; specifically, type of improvement, cost, location, and level of flood protection;
- Discussed the technical and qualitative factors for each alternative; and
- Selected the most favorable alternative for each project.

4.9 Prioritization

During working meetings three, four, and nine, the stakeholders identified in Section 4.8 developed general prioritization criteria and then evaluated the recommended projects based on those criteria. The end result was a prioritized list of projects that will help identify the relative priority for funding the various projects.

5.0 IDENTIFIED PROBLEM AREAS

Initial phases of the stormwater master planning process included:

- Hydrologic and hydraulic analyses for each of the study areas;
- Field reconnaissance of the study areas;
- · Review of previous studies;
- Discussions with local residents; and
- Discussions with representatives from El Paso County, EPWU, TWDB, City of Socorro, Village of Vinton, and EPCWID No.1.

These activities resulted in identifying specific problem areas within each of the study areas. The problem areas are identified with three numbers representing the study area and numbered sequentially. For example, the specific problem areas discussed in this study for Vinton are identified as VIN1, VIN2, VIN3, etc. The following sections provide a general description of the problems identified in each study area followed by more detailed description of each identified problem area.

5.1 Vinton Study Area

A number of flooding and sedimentation issues were identified in the Vinton Study Area based on information gathered from representatives from El Paso County, Village of Vinton, field reconnaissance gathered from site visits, and previous studies. Flooding of residences and property located along the arroyos is the primary concern in this area.

Many of the upstream watersheds for the Vinton Study Area are very large, causing a significant amount of uncontrolled water and sediment to be carried to downstream residential areas via natural arroyos. As the large flows reach the residential areas, the arroyos become constricted, resulting in the flooding of homes and properties.

As identified in the City SMP, there are a number of identified issues associated with Flow Path Number 45 and its tributary Flow Path Number 45A. In addition to many portions of the channels not having sufficient capacity, 12 of the 15 total crossings within the developed areas are undersized. Another major concern in the study area is sediment transport. Sediment loads originating in the mountains upstream of the study area have the potential to clog channels and crossing structures, reducing their already limited capacity. It is likely that this would result in the flooding of residents living along the channel. Westway residents, who live along Flow Path Number 45, expressed their concerns about flooding during Public Meeting Number 1 held in September 2009. These residents were flooded during the storms of 2006.

Flow Path Number 44 has also been identified as having capacity issues through the residential area. The channel, which converges with Flow Path Number 43 upstream, is constricted between properties as it passes through the residential area. This, in conjunction with fill being placed in the channel by property owners, results in the overtopping of the channel and the flooding of downstream residents.

The following sections describe the specific problems associated with each problem area shown on Figure 5-1.

5.1.1 VIN1

Uncontrolled flows from the upstream watershed and the absence of a defined channel cause flooding problems to residences at the upstream portion of Flow Path Number 45A, between Remington Drive and IH-10. Runoff and sediment from undeveloped areas in the watershed enter the upper tributaries of the watershed that converge to form the Flow Path Number 45. Approximately 2,800 feet upstream of the convergence of the tributaries, a portion of the flow branches from a main tributary and continues traveling west toward the intersection of Remington Drive and Southwood Road. When flow reaches this intersection, there is no defined channel, as development has encroached into the channel. At this location, flows spread out along Southwood Road (Flow Path Number 45A), flooding a number of residences and depositing sediment.

5.1.2 VIN2

Uncontrolled flows and insufficient channel capacity along Flow Path Number 45A pose a flood risk to residences adjacent to the channel between Kiely Road and Iron Drive. Flows from the upstream watershed travel along Southwood Road as discussed in Section 5.1.1. After reaching Kingsway Drive, flows enter an earthen channel. Between Iron Drive and Kiely Road, the channel runs through private property. The County does not own or possess a drainage easement through this area making it difficult to improve and maintain the channel. In addition, this portion of the channel has significantly reduced capacity due to encroachment into the channel by residents living adjacent to the channel. The lack of maintenance and reduction in channel capacity causes the channel to overtop and pose a flood risk to residents downstream and adjacent to the channel.

5.1.3 VIN3

Uncontrolled flows originating in the upper end of the watershed and encroachment into the channel by residents of Vinton are resulting in the flooding of residences along Flow Path Number 45, between Tom Mays Drive and De Alva Drive. Runoff from undeveloped areas in the watershed enters the upper tributaries that converge to form the Flow Path Number 45. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. As flows reach Tom Mays Drive where a culvert is planned for a future extension of Tom Mays Drive, the channel becomes constricted, resulting from encroachment into the channel by residents living adjacent to the channel. The channel has insufficient capacity at this location, resulting in the flooding of residences adjacent to the channel. In addition, sediment poses maintenance issues at De Alva Drive and potential maintenance issues at the planned culvert at Tom Mays Drive.

5.1.4 VIN4

Uncontrolled flows originating in the upper end of the watershed and encroachment into the channel by residents of Vinton are resulting in the flooding of residences along Flow Path Number 45, between Quejette Road and Rancho Estancias Drive. Runoff from undeveloped areas in the watershed enters the upper tributaries that converge to form the Flow Path Number 45. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. As flows reach Quejette Road, the channel becomes constricted, resulting from encroachment into the channel by residents living adjacent to the channel. The channel has insufficient capacity at this location, resulting in the flooding of residences adjacent to the

channel. In addition, residents have constructed encroaching improvements that increase flooding to adjacent properties. The County does not own or possess a drainage easement through this area making it difficult to improve and maintain the channel.

5.1.5 VIN5

Uncontrolled flows originating in the upper end of the watershed and encroachment into the channel by residents of Vinton are resulting in the flooding of residences along Flow Path Number 44, between Selva Drive and Midway Street. The south half of this channel is located within the City of Vinton, and the north half is El Paso County. Runoff from undeveloped areas in the watershed enters the upper tributaries that converge to form the Flow Path Number 44. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. As flows reach Selva Drive, the channel becomes constricted, resulting from encroachment into the channel by residents living adjacent to the channel. The channel has insufficient capacity at this location, resulting in the flooding of residences adjacent to the channel. Erosion and undermining has been observed on these properties. The County does not own or possess a drainage easement through this area making it difficult to improve and maintain the channel.

5.1.6 VIN6

The crossing (one 16-foot by 5-foot concrete box culvert [CBC]) at the intersection of Flow Path Number 44 and Doniphan Drive was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.1.7 VIN7

The bridge at the intersection of Flow Path Number 45 and The Railroad was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the bridge does not have sufficient capacity to convey the 100-year flood through the crossing. There are current plans to replace the existing bridge with a control structure that is being sized to match the capacity of the Doniphan Rd bridge (VIN8), which also has insufficient capacity.

5.1.8 VIN8

The crossing (two 6-foot by 6-foot CBCs) at the intersection of Flow Path Number 45 and Doniphan Drive was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.1.9 VIN9

The crossing (four 36-inch corrugated metal pipes (CMPs) at the intersection of Flow Path Number 45 and A.P. Ramirez Street was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.1.10 VIN10

The crossing (two 8-foot by 3-foot CBCs) at the intersection of Flow Path Number 45 and Kiely Road was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing. Residents have constructed a private sluice gate approximately 1,000 feet upstream of this crossing that causes induced flooding to adjacent land owners and over an uncontrolled section of Kiely Rd approximately 450 feet north of the crossing.

5.1.11 VIN11

The low water crossing at the intersection of Flow Path Number 45 and Quejette Road was reported to be an issue. Without a structure allowing flow to pass under the road surface, flow will continue to pass over the road during storm events. Residents have reported that some of this flow travels along Quejette Road and ponds to the south.

5.1.12 VIN12

The crossing (thirteen 9-foot by 5-foot CBCs) at the intersection of Flow Path Number 45 and IH-10 northbound off-ramp was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.1.13 VIN13

The crossing (two 30-inch reinforced concrete pipes [RCPs]) at the intersection of Flow Path Number 45A and Kiely Drive was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.1.14 VIN14

The crossing (three 30-inch RCPs) at the intersection of Flow Path Number 45A and Iron Drive was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.2 Canutillo Study Area

A number of flooding and sedimentation issues were identified in the Canutillo Study Area based on information gathered from representatives from El Paso County, residents of the affected areas, as well as field reconnaissance gathered from site visits. These identified issues were the focus of further hydrologic and hydraulic analysis.

The primary concern within the northern portion of the Canutillo Study Area is that many of the upstream watersheds are very large, causing a significant amount of uncontrolled water and sediment to be carried to downstream semi-rural areas via natural arroyos. As the large flows reach the residential areas, the arroyos become less defined, resulting in the flooding of homes and properties.

A particular arroyo of concern is within the northern portion of the Canutillo Study Area is Flow Path Number 42. A number of arroyos, originating in upstream watersheds, converge with Flow Path Number 42 upstream of the Canutillo Heights Community. A concrete lined channel provides sufficient capacity through the Canutillo Heights Community, but does not extend past El Chanate Drive. At this location, there is no longer a stable channel configuration, resulting in downstream flooding. The County only has drainage easement through the developed portion of Canutillo Heights and does not have the authority to maintain or improve channel segments upstream or downstream of this development.

The southern portion of the Canutillo Study Area has a much smaller contributing watershed compared to the northern area. The primary concern within this area is the ponding of runoff, resulting in flooding of residences and businesses.

A particular area of flooding concern within the southern portion of the Canutillo Study Area is at the intersection of Talbot Avenue and Doniphan Drive, near the Dollar General and the local flea market. This location is a localized topographic depression and does not discharge to the Rio Grande. This watershed area contains no curb and gutter nor is there a clear flow path through the community. This lack of drainage infrastructure requires that the County drain the area by pumping during high runoff events.

The following sections describe the specific problems associated with each problem area shown on Figure 5-2.

5.2.1 CAN1

Uncontrolled flows originating in the upper end of the watershed and the encroachment into the channel by residents of Canutillo are resulting in the flooding of residences along Flow Path Number 42, downstream of the Canutillo Heights Community. Runoff from undeveloped areas in the watershed enters the upper tributaries that converge to form the Flow Path Number 42. Additional runoff is accumulated as flows travel through the steepest part of the watershed. The channel has sufficient capacity to convey flows through the Canutillo Heights Community due to concrete channel improvements, but the improvements do not extend beyond the community. As flows leave the community, the channel becomes earthen and unstable. The channel also becomes constricted, resulting from encroachment into the channel by residents living adjacent to the channel. The channel has insufficient capacity at this location, resulting in the flooding of residences adjacent to the channel. The County does not own or possess a drainage easement through this area making it difficult to improve and maintain the channel.

5.2.2 CAN2

The lack of drainage infrastructure within the lower portion of the study area is resulting in the flooding of residences and businesses. County staff noted flooding issues around the intersection of Talbot Avenue and Doniphan Drive, near the Dollar General and the local flea market. This location is a localized topographic depression and there in no nearby location for the water to traverse the railroad to discharge to the Rio Grande at this time. This watershed area contains no curb and gutter nor is there a clear flow path for the flow to travel through the community. This lack of drainage infrastructure results in the County having to pump water away from the area during high runoff events.

5.2.3 CAN3

The crossing (two 6 foot x 3 foot CBCs) at the intersection of First Avenue Channel and Doniphan Drive was reported to have capacity issues. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing. Although the culvert is large enough, it slopes to the wrong direction.

5.3 Sparks Arroyo and Sub Basin A Study Area

Problem areas in the Sparks Arroyo and Sub Basin A Study Area were identified as part of a USACE feasibility study. The following paragraphs are based on this information as well as information provided by representatives from El Paso County, representatives from the City of Socorro, and residents of the affected areas.

Frequent flooding of residences and properties located at the downstream end of the natural arroyos is a primary concern in the Sparks Arroyo and Sub Basin A Study Area. Large flows originating on the upstream mesa are conveyed downstream via natural arroyos before reaching the flat agricultural valley. When flows reach the downstream end of the arroyos they have significant velocities and sediment. At this point, the arroyos become poorly defined and flows spread out causing shallow flooding and sediment deposition. The specific arroyos identified as potential problems in the Sparks Arroyo and Sub Basin A Study Area are Arroyo 1, Arroyo 2, Arroyo 3, Arroyo 4, Arroyo 5, Arroyo 6, and the Sparks Arroyo. According to the USACE feasibility study, the wastewater treatment plant (WWTP) located at the upstream end of the Sparks Arroyo is also at risk of flooding due to the uncontrolled flows from the upstream watershed.

There are a number of additional flooding problems associated with the Sparks Arroyo. The arroyo has capacity and stability issues along its entire length. These issues pose a significant risk to residences adjacent to the arroyo. Much of the flooding will be reduced by oversized detention that will be part of future development currently being planned north of the WWTP and a planned extension of Rojas Drive. However, even after this development a significant portion of the watershed will remain uncontrolled.

In addition, the current configuration of the arroyo downstream of IH-10 poses a significant flood risk to downstream residences in the Valley Ridge Subdivision.

The following sections describe the specific problems associated with each problem area shown on Figure 5-3.

5.3.1 SSA1

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to agricultural land at the mouth of Arroyos 1, 2, and 3, just downstream of IH-10. Residences located downstream of these arroyos, on the south side of the Mesa Spur Drain, are also at risk due to the volume of flow from the arroyos. Runoff from the development in Horizon City and other undeveloped areas on the mesa enters the upper tributaries of the watershed that converge to form the arroyos. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,500 feet downstream of IH-10, the arroyos become undefined, with no clear outfall to the Mesa Spur Drain. At this location, flows spread out depositing sediment and posing a flood risk to agricultural land in the area. Due to the large

volume of the flow from the arroyos, there is the potential to exceed the capacity of the Mesa Spur Drain and flood residences located south of the channel.

5.3.2 SSA2

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to agricultural land at the mouth of Arroyo 4, just downstream of IH-10. Runoff from undeveloped areas in the watershed is conveyed through the watershed via Arroyo 4. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 100 feet upstream of Old Hueco Tanks Road, the arroyo becomes undefined, with no clear outfall to the Mesa Spur Drain. At this location, flows spread out depositing sediment and posing a flood risk to agricultural land in the area.

5.3.3 SSA3

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to agricultural land, residences, and the El Paso Community College Mission del Paso Campus parking lot at the mouth of Arroyos 5 and 6, just downstream of IH-10. Runoff from undeveloped areas in the watershed is conveyed through the watershed via the arroyos. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,500 feet downstream of IH-10, the arroyos become undefined, with no clear outfall to the Mesa Spur Drain. At this location, flows spread out depositing sediment and posing a flood risk to agricultural land in the area. The El Paso Community College Mission del Paso Campus parking lot is located adjacent to the downstream end of Arroyo 5 and is at risk of flooding and being undermined. In addition, there are a number of residences located adjacent to the downstream end of Arroyo 6 that are at risk of flooding.

5.3.4 SSA4

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to the WWTP at the upstream end of the Sparks Arroyo and to residences located adjacent to the arroyo. Runoff from the development in Horizon City and other undeveloped areas on the mesa enters the upper tributaries of the watershed that converge to form the Sparks Arroyo. According to the USACE feasibility study, flows from these tributaries pose a flood risk to the WWTP at the upstream end of the Sparks Arroyo. The tributaries converge approximately 300 feet downstream of the WWTP. At this location, flows from the tributaries exceed the capacity of the Sparks Arroyo and pose a flood risk to residences downstream.

5.3.5 SSA5

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences located adjacent to the Sparks Arroyo. Runoff from the development in Horizon City and other undeveloped areas on the mesa enters the upper tributaries of the watershed that converge to form the Sparks Arroyo. At the point of convergence, flows from the tributaries exceed the capacity of the Sparks Arroyo and pose a flood risk to residences adjacent to the arroyo. Additionally, the arroyo is very erodible and large flows have resulted in the widening of the arroyo. Without modification, the widening may begin to impact homes adjacent to the arroyo.

5.3.6 SSA6

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences located adjacent to the Sparks Arroyo. Runoff from the development in Horizon City and other undeveloped areas on the mesa enters the upper tributaries of the watershed that converge to form the Sparks Arroyo. At the point of convergence, flows from the tributaries exceed the capacity of the Sparks Arroyo and pose a flood risk to residences adjacent to the arroyo. Additionally, runoff from the Sparks Community exacerbates the capacity issues of the Sparks Arroyo, posing a risk to residences adjacent to the Arroyo, as well as posing a flood risk to residences downstream of the community.

5.4 Socorro Study Area

A number of flooding and sedimentation issues were identified in the Socorro Study Area based on information gathered from representatives from El Paso County, representatives from the City of Socorro, residents of the affected areas, field reconnaissance gathered from site visits, and the hydrologic and hydraulic analysis.

Frequent flooding of residences and properties located at the downstream end of the natural arroyos is a primary concern in the Socorro Study Area. Large flows originating on the upstream mesa are conveyed downstream via natural arroyos before reaching the flat agricultural valley. When flows reach the downstream end of the arroyos they have significant velocities and sediment. At this point, the arroyos become poorly defined and flows spread out causing shallow flooding and sediment deposition. The specific arroyos identified as potential problems in the Socorro Study Area are Stream 4, Stream 5, and an unnamed stream labeled Stream 5.5 for the purposes of this County SMP.

A basin in El Paso Hills had been alleviating some of the issues described above for downstream areas, but is currently not functioning properly as the embankment has failed.

Several crossings along the Mesa Spur Drain were identified to have insufficient capacity. The Mesa Spur Drain is an agricultural drain that runs from northeast to southwest along the edge of the Socorro Study Area. It has an approximate average depth of 9 feet and a top width of 30 to 40 feet. There were no capacity issues reported for the portion of the channel within this study area. The flow capacity of the Mesa Spur Drain was estimated and compared to crossing capacities to help indentify potentially undersized crossings. The crossings along the Mesa Spur Drain located at Carr Road, Coker Road, Anderson Road, and the intersection of the Mesa Drain were identified as problem crossings.

The following sections describe the specific problems associated with each problem area shown on Figure 5-4.

5.4.1 SOC1

The basin in El Paso Hills currently has a failed embankment and is not functioning properly. According to El Paso County staff, a portion of the embankment failed in a 2004 storm event. Currently this failure has not been repaired. The basin had been providing some benefit prior to its failure by controlling flows in Stream 4, but is providing minimal benefit in its current state.

5.4.2 SOC2

Uncontrolled flows originating in the upper end of the watershed are causing flooding at the mouth of Stream 4, just upstream of Coker Road. Runoff from development in Horizon City enters the upper tributaries of the watershed that converge to form Stream 4. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Additional runoff from El Paso Hills enters Stream 4 before it passes under IH-10. Approximately 1,050 feet upstream of Coker Road and the Mesa Spur Drain, the arroyo becomes undefined, with no clear outfall to the Mesa Spur Drain. At this location, flows spread out along Kennstrom Court flooding a number of residences and depositing sediment.

5.4.3 SOC3

Uncontrolled flows originating in the upper end of the watershed are causing flooding at the mouth of Stream 5, upstream of Coker Road. Runoff from undeveloped areas along the mesa is conveyed through the watershed via Stream 5. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,000 feet upstream of the intersection of Coker Road and Worsham Road, the arroyo becomes undefined, with no clear outfall to the Mesa Spur Drain. At this location, flows spread out flooding a number of residences and depositing sediment.

5.4.4 SOC4

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences upstream of the intersection of Stream 5.5 and the Mesa Spur Drain. Runoff from undeveloped areas along the mesa is conveyed through the watershed via Stream 5.5. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Several feet of sediment have been observed on Gateway E. Drive after major storm events. Approximately 1,000 feet upstream of the intersection of Stream 5.5 and Mankato Road, development and agricultural lands are present on both sides of the arroyo. The arroyo passes over a low water crossing at Mankato Road, depositing sediment before converging with the Mesa Spur Drain. The flows in the arroyo are uncontrolled and pose a flood risk to residences and agricultural lands adjacent to Stream 5.5.

5.4.5 SOC5

Although the crossing (one 48-inch CMP) at the intersection of the Mesa Spur Drain and Carr Road was not reported to have capacity problems, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Spur Drain was flowing bank-fill, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.4.6 SOC6

Although the crossing (one 48-inch CMP) at the intersection of the Mesa Spur Drain and Coker Road was not reported to have capacity problems, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Spur Drain was flowing bank-fill, this crossing would restrict the capacity of the channel and potentially cause flooding of the residential and agricultural lands adjacent to the channel.

5.4.7 SOC7

Although the crossing (one 48-inch CMP) at the intersection of the Mesa Spur Drain and Anderson Road was not reported to have capacity problems, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Spur Drain was flowing bank-fill, this crossing would restrict the capacity of the channel and potentially cause flooding of the residential and agricultural lands adjacent to the channel.

5.4.8 SOC8

Although the crossing (one 60-inch CMP) at the intersection of the Mesa Spur Drain and Mesa Drain was not reported to have capacity problems, based on inspection and hydraulic analysis it appears that the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Spur Drain was flowing bank-fill, this crossing would restrict the capacity of the channel and potentially cause flooding of the residential and agricultural lands adjacent to the channel.

5.5 Hacienda Real Study Area

A number of flooding and sedimentation issues were identified in the Hacienda Real Study Area based on information gathered from representatives from El Paso County, residents of the affected areas, field reconnaissance gathered from site visits, and the hydrologic and hydraulic analysis.

Frequent flooding of residences and properties located at the downstream end of the natural arroyos, at the break in slope as the arroyos enter the flatter agricultural valley, is a primary concern in the Hacienda Real Study Area. Large flows originating on the upstream Mesa are conveyed downstream via natural arroyos before reaching the flat agricultural valley. When flows reach the downstream end of the arroyos, they have significant velocities and sediment. At this point, the arroyos become poorly defined and flows spread out causing shallow flooding and sediment deposition. The specific arroyos identified as potential problems in the Hacienda Real Study Area are Stream 6, Stream 7, Stream 8, Stream 9, Stream 10, Stream 11, Stream 12, Stream 13, and an unnamed stream labeled Stream 13.5 for the purposes of this County SMP.

Several crossings along Mesa Drain, and one along Stream 7 were also identified to have issues with collapse, washout, or insufficient capacity. The Mesa Drain is an agricultural drain that runs from northeast to southwest along the edge of the Hacienda Real Study Area. It has an approximate average depth of 10 feet and a top width of 30 to 40 feet. There were no capacity issues reported for the portion of the channel within this study area. The flow capacity of the Mesa Drain was estimated and compared to crossing capacities to help identify potentially undersized crossings. Six crossings along Mesa Drain were identified to have issues ranging from insufficient capacity to collapse. The crossings along Mesa Drive located at Northloop Drive, FM 1110, the Salatral Lateral, Fenter Road, Celum Road, and at a dirt road upstream of Celum Road were identified as being problem crossings. Additionally, the crossing at the intersection of Stream 7 and Bridgeway Drive was identified as a problem crossing.

The following sections describe the specific problems associated with each problem area shown on Figure 5-5.

5.5.1 HAC1

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences within the colonia located to the west of the intersection of IH-10 and FM 1110. Runoff from undeveloped areas along the mesa is conveyed through the watershed via Stream 6. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Just downstream of IH-10, the arroyo outfalls into two small basins that are located upstream of Ferntower Drive and Pennington Drive. Once the basins reach capacity, they overflow into the streets of the colonia, where the storm water is conveyed to the lower end of the colonia. This street flow poses a risk to residences within the colonia.

5.5.2 HAC2

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences east of the intersection of Roberts Ranch Road and Wild Horse Road, at the downstream end of Stream 7. Runoff from the development in Horizon City and undeveloped areas along the mesa enters the upper tributaries of the watershed that converge to form Stream 7, where the combined flows result in uncontrolled flooding over the crossing at Fortuna Street. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,900 feet upstream of the intersection of Northloop Drive and Roberts Ranch Road, the arroyo becomes undefined, with no clear outfall to the Mesa Drain. At this location, flows spread out depositing sediment and posing a flood risk to residences in the area.

5.5.3 HAC3

Uncontrolled flows originating in the upper end of the watershed are causing flooding at the mouth of Stream 8, upstream of Northloop Drive. Runoff from undeveloped areas along the mesa is conveyed through the watershed via Stream 8. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,500 feet east of the intersection of Virrey Road and Reina Road, the arroyo becomes undefined, with no clear outfall to the Mesa Drain. At this location, flows spread out flooding a number of residences and depositing sediment.

5.5.4 HAC4

Uncontrolled flows originating in the portion of the watershed below the Clint Landfill are causing flooding at the convergence of Streams 9 and 10, upstream of Northloop Drive. Runoff from undeveloped areas in the watershed is conveyed downstream via Streams 9 and 10. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 2,000 feet upstream of Northloop Drive, the arroyos converge and become undefined, with no clear outfall to the Mesa Drain. At this location, flows spread out flooding a number of residences and depositing sediment.

5.5.5 HAC5

Uncontrolled flows originating in the portion of the watershed below the Clint Landfill pose a flood risk to residences at the mouth of Stream 11, upstream of Northloop Drive. Runoff from undeveloped areas in the watershed are conveyed downstream via Stream 11. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 2,500 feet upstream of Northloop Drive, the arroyo becomes undefined, with no

clear outfall to the Mesa Drain. At this location, flows spread out depositing sediment and posing a flood risk to residences in the area.

5.5.6 HAC6

Uncontrolled flows originating in the upstream portion of the watershed pose a flood risk to residences at the mouth of the convergence of Streams 12 and 13, upstream of Northloop Drive. Runoff from undeveloped areas in the watershed are conveyed downstream via Streams 12 and 13. The streams converge and additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 2,150 feet upstream of Northloop Drive, the arroyo becomes undefined, with no clear outfall to the Mesa Drain. At this location, flows spread out depositing sediment and posing a flood risk to residences in the area.

5.5.7 HAC7

Uncontrolled flows originating in the upstream portion of the watershed pose a flood risk to residences at the mouth of Stream 13.5, upstream of Northloop Drive, and to extensive agricultural land downstream. Runoff from undeveloped areas along the mesa passes through land where an expansion of the City of El Paso landfill near Clint is currently being planned, and enters the upper tributaries of the watershed that converge to form Stream 13.5. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,800 feet upstream of Northloop Drive, the arroyo becomes undefined, with no clear outfall to the Mesa Drain. At this location, flows spread out depositing sediment and posing a flood risk to residences in the area.

5.5.8 HAC8

The crossing (five 48-inch CMPs) at the intersection of Stream 13.5 and Bridgeway Drive was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.5.9 HAC9

Although the crossing (one 60-inch RCP) at the intersection of the Mesa Drain and Northloop Drive was not reported to have capacity problems, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Drain was flowing bank-full, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.5.10 HAC10

The crossing (one 42-inch CMP) at the intersection of the Mesa Drain and FM 1110 (Clint Cut-Off Road) was reported to be collapsed or silted, and it was confirmed that it was not functioning properly during a 2009 site visit. Additionally, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Drain was flowing bank-full, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.5.11 HAC11

Although the crossing (one 36-inch RCP) at the intersection of the Mesa Drain and the Salatral Lateral was not reported to have capacity problems, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Drain was flowing bank-full, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.5.12 HAC12

Although the crossing (one 72-inch CMP) at the intersection of the Mesa Drain and Fenter Road was not reported to have capacity problems, based on inspection and hydraulic analysis, the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Drain was flowing bank-full, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.5.13 HAC13

Although the crossing (one 36-inch CMP) at the intersection of the Mesa Drain and the dirt road just upstream of Celum Road was not reported to have capacity problems, based on inspection and hydraulic analysis it appears that the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Drain was flowing bank-full, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.5.14 HAC14

Although the crossing (one 54-inch CMP) at the intersection of the Mesa Drain and Celum Road was not reported to have capacity problems, based on inspection and hydraulic analysis it appears that the culvert does not have capacity greater than or equal to that of the channel. If the Mesa Drain was flowing bank-full, this crossing would restrict the capacity of the channel and potentially cause flooding of the agricultural lands adjacent to the channel.

5.6 Fabens Study Area

Based on information gathered from representatives from El Paso County, the primary issue identified in the Fabens Study Area is the lack of drainage easements. In addition, a county-owned, Texas Commission on Environmental Quality (TCEQ) regulated dam within the study area currently does not meet TCEQ requirements. A 30% design has been developed by the County to rehabilitate this dam.

The County currently does not have a drainage easement through the developed portion of the study area, making it difficult to improve or maintain a portion of the San Felipe Arroyo.

A privately constructed ponding area located to the north of the Fabens Community breached during a recent storm event. The channels that contribute flow to this ponding area are currently unnamed and will be identified in this study, from north to south, as Fabens North 1, Fabens North 2 Tributary 1, and Fabens North 2.

The following sections describe the specific problems associated with each problem area shown on Figure 5-6.

5.6.1 FAB1

A privately constructed ponding area located north of the Fabens Community breached during a recent storm event. Per a 2009 site visit, this failure has not been repaired. The basin had been providing some benefit prior to its failure by controlling flows in Fabens North 1, Fabens North 2 Tributary 1, and Fabens North 2, but is providing minimal benefit in its current state.

5.6.2 FAB2

The San Felipe Arroyo, which runs through the developed area, has sufficient flow capacity. However, there is concern that without a drainage easement through the developed portion of the study area, it is very difficult for the County to maintain the existing drainage channel. Without proper maintenance, there are likely to be problems associated with the channel in the future.

5.6.3 FAB3

Fabens Dam is the only TCEQ regulated dam owned by the County. TCEQ regulations require that a dam of this size pass 75% of the flood caused by a Probable Maximum Precipitation (PMP) event without overtopping and potentially breaching the dam. Based on hydrologic analysis, the dam does not currently meet this requirement.

5.7 Tornillo Study Area

Based on information gathered from representatives from El Paso County and field reconnaissance, the primary issue identified in the Tornillo Study Area is the flooding of public and private property due to uncontrolled flows from upstream watersheds. As channels originating in the upstream watersheds reach the developed community of Tornillo, they become less defined and the accumulated flow spreads out resulting in flooding of residents.

One channel of particular concern within the Tornillo Study Area is the High School Channel. The channel conveys large flows from the upstream watersheds, past a high school, to the developed community below. As the channel approaches the high school, it is redirected south to a local basin. During the storm of 2006, the side of the channel was breached, causing the high school and the community downstream to flood. In an attempt to stop erosion of the channel bank, the County has constructed erosion protection along the west side of the channel using a recycled tire-riprap combination. A field visit conducted for this study indicated evidence of undercutting of the erosion protection.

The local basin, which appears to be an old borrow pit, lies south of the high school and collects flow from both High School Channel and South High School Channel. The basin is undersized for the amount of flow which is expected to reach the area.

The other three channels located to the south of the South High School Channel are currently unnamed. For the purpose of this study, these channels will be known as, from north to south: Flow Path T, Tornillo Handle Channel 1, and Tornillo Handle Channel 2. Currently, the crossing located at OT Smith Road does not provide sufficient capacity for the Tornillo Handle Channel

1. As a result, the upstream channel overtops and floods the residents along the road. Flows from Flow Path T, Tornillo Handle Channel 1, and Tornillo Handle Channel 2 travel through unconfined channels before entering the community of Tornillo. The channels become undefined within the community resulting in flooding of residents within the area.

The following sections describe the specific problems associated with each problem area shown on Figure 5-7.

5.7.1 TOR1

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences downstream of High School Channel and South High School Channel. Runoff from undeveloped areas in the watershed enters the upper tributaries that converge to form the channels. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Approximately 1,300 feet downstream of Valley Gin Road, the channels converge before discharging into a local basin. The basin is currently undersized, posing a flood risk to residences downstream.

5.7.2 TOR2

Channel bank instability along the High School Channel poses a flood risk to the high school and to residences downstream of the high school. Near the high school, the High School Channel changes in direction, diverting flows to a localized basin on the south side of the high school. During the storm of 2006, the side of the channel was breached, causing the high school and the community downstream to flood. The County has constructed erosion protection along the west side of the channel using a recycled tire-riprap combination. A field visit conducted for this study indicated evidence of undercutting of the erosion protection. Until this channel is stabilized, the high school and residences downstream of the high school will be at risk of flooding.

5.7.3 TOR3

Uncontrolled flows originating in the upper end of the watershed pose a flood risk to residences downstream of Flow Path T, south of Highland Road. Runoff from undeveloped areas in the watershed enters the upper tributaries that converge to form the channel. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Near Highland Road, the channel discharges into a local basin. The basin previously provided some protection during small storm events, but has breached and is currently proving minimal benefit. The downstream community is at risk of flooding.

5.7.4 TOR4

Uncontrolled flows originating in the upper end of the watershed are causing flooding at the mouth of Tornillo Handle Channel 2, downstream of Big Master Road. Runoff from undeveloped areas in the watershed is conveyed via Tornillo Handle Channel 2. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Downstream of Big Master Road, the arroyo becomes undefined, flooding a number of residences.

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5.7.5 TOR5

Uncontrolled flows originating in the upper end of the watershed are causing flooding at the mouth of Tornillo Handle Channel 1, downstream of Big Master Road. Runoff from undeveloped areas in the watershed is conveyed via Tornillo Handle Channel 1. Additional runoff and sediment are accumulated as flows travel through the steepest part of the watershed. Downstream of Big Master Road, the arroyo becomes undefined, flooding a number of residences.

5.7.6 TOR6

The crossing (two 36-inch pipes) at the intersection of Tornillo Handle Channel 2 and OT Smith Road was reported to have insufficient capacity. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing.

5.8 Montana Sector Study Area

Based on information provided by representatives from El Paso County and field reconnaissance, the primary issues identified in the Montana Sector Study Area are the flooding of county roads that have undersized culverts or no culverts at all, and flooding of private property due to uncontrolled flows from upstream watersheds. As channels originating in the upstream watersheds reach the developed areas, they become less defined and the accumulated flow spreads out resulting in widespread flooding of residents. As these flows fill a series of natural depressions they then result in prolonged flooding of low-lying residences located within the depressions.

The four channels of particular concern within the Montana Sector Study Area are Flowpaths M-2, M-3, M-4, and M-6. These channels convey large flows from the upstream watersheds to the developed areas below, conveying large amounts of debris that overwhelm and damage county road crossing, leading to both access and maintenance issues. According to local residence, minimal or non-existent flood control infrastructure results in flooding over roads every time it rains, and persistent flooding in ponded areas.

One dam located within Hueco Tanks State Park provides flood and debris control for a small portion of the Montana Sector study area, but the majority of the area remains uncontrolled.

The largest regional flood to impact the Montana Sector in recent history was Hurricane Dolly in 2008, in which 2.0"-5.7" of precipitation fell across the study area in a 24-hour period. According to modeling and historical aerial imagery provided by Google, it is estimated that flooding from Hurricane Dolly impacted approximately 44 residences.

The following sections describe the specific problems associated with each problem area shown on Figure 5-8.

5.8.1 MON1

Uncontrolled flows originating in the Fort Bliss Military Reservation accumulate and enter the unincorporated area of the County near the intersection of Hunton Street and Remington Road. Without a defined channel, these flows spread out at low velocities, impacting multiple

residences, until terminating at a large natural depression centered near the intersection of Bradley Road and Desert Willow Drive. Several residences are located within this natural depression and are impacted by major storm events, such as Hurricane Dolly.

5.8.2 MON2

Uncontrolled flows originating in the slopes above Tributary 1 to Flowpath M-4 accumulate and enter a small developed area north of Buckwheat Street. Without a defined channel, these flows spread out, impacting multiple residences, until entering Flowpath M-4, conveying debris through undersized culverts until finally terminating at a large natural depression centered near the intersection of Bradley Road and Desert Willow Drive. Several residences are located within this natural depression and are impacted by major storm events, such as Hurricane Dolly.

5.8.3 MON3

Uncontrolled flows originating in the slopes above Flowpaths M-2, M-3, and M-5 spread out over a vast area, merging and diverging from each other at various points. The majority of the flows concentrate at a narrow opening between hills located approximately 2,000 feet south of the intersection of Stagecoach Drive and Old Butterfield Trail. From here, these flows continue westward down Flowpath M-3 contributing to flooding of numerous residences and conveying debris that overwhelms a series of culvert crossings. These flows ultimately terminate at several large natural depressions. Several residences are located within these natural depression and are impacted by major storm events.

5.8.4 MON4

The at grade crossing at the intersection of Flowpath M-4 and Tamara Road does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance.

5.8.5 MON5

The at grade crossing at the intersection of Flowpath M-4 and Oleary Drive does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance.

5.8.6 MON6

The at grade crossing at the intersection of Flowpath M-4 and Paso View Drive does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance.

5.8.7 MON7

The crossing (two 18-inch pipes) at the intersection of Flowpath M-2 and Stagecoach Drive does not have sufficient capacity to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance, and serves as the only access point to a house located on Alkali Lane.

5.8.8 MON8

The at grade crossing at the intersection of Flowpath M-2 and Indian Trail Road does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance, and serves as the only access point to several structures.

5.8.9 MON9

The at grade crossing at the intersection of Flowpath M-2 and Hueco Tanks Road was reported as requiring frequent maintenance. Based on inspection and hydraulic analysis, the culvert does not have sufficient capacity to convey the 100-year flood through the crossing. This road serves as the primary access point to numerous residences and the Hueco Tanks State Park.

5.8.10 MON10

The at grade crossing at the intersection of Flowpath M-3 and Hueco Mountain Road does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance.

5.8.11 MON11

The at grade crossing at the intersection of Flowpath M-3 and Overland Stage Road does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance.

5.8.12 MON12

The crossing (five 4'x5' concrete box culverts) at the intersection of Flowpath M-3 and Woodrow Road does not have sufficient capacity to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance.

5.8.13 MON13

The crossing (three 18-inch pipes) at the intersection of Flowpath M-3 and Hueco Tanks Road does not have sufficient capacity to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance and serves as the primary access point to numerous residences and the Hueco Tanks State Park.

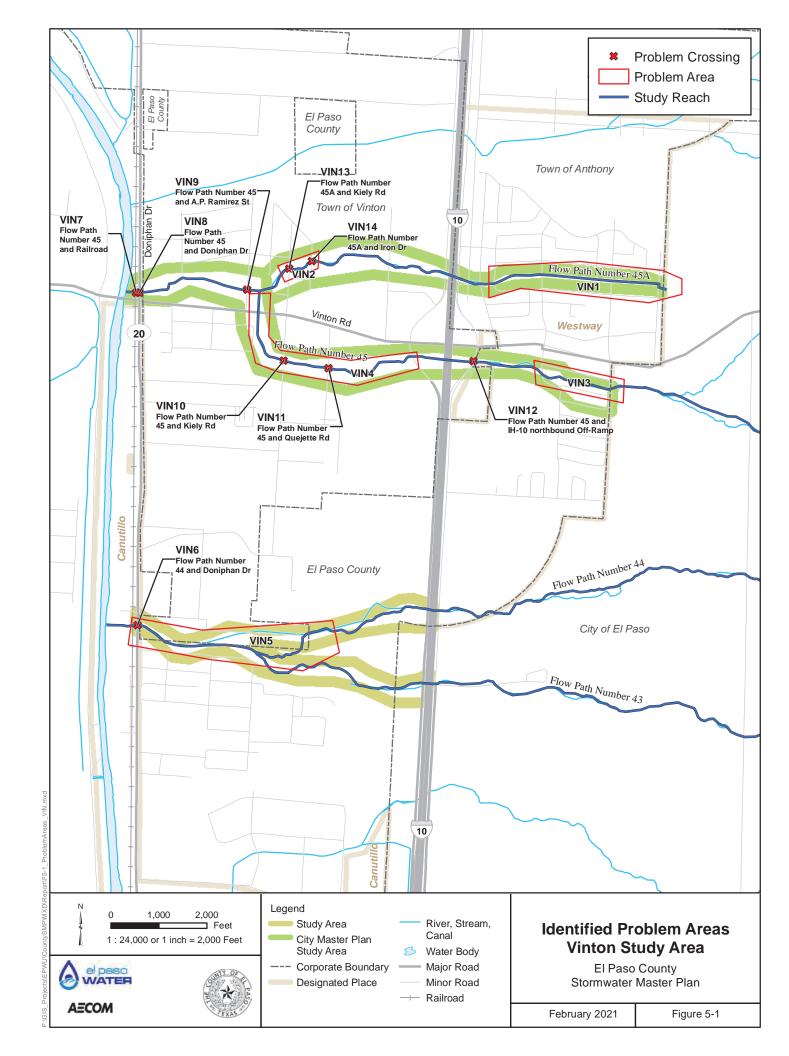
5.8.14 MON14

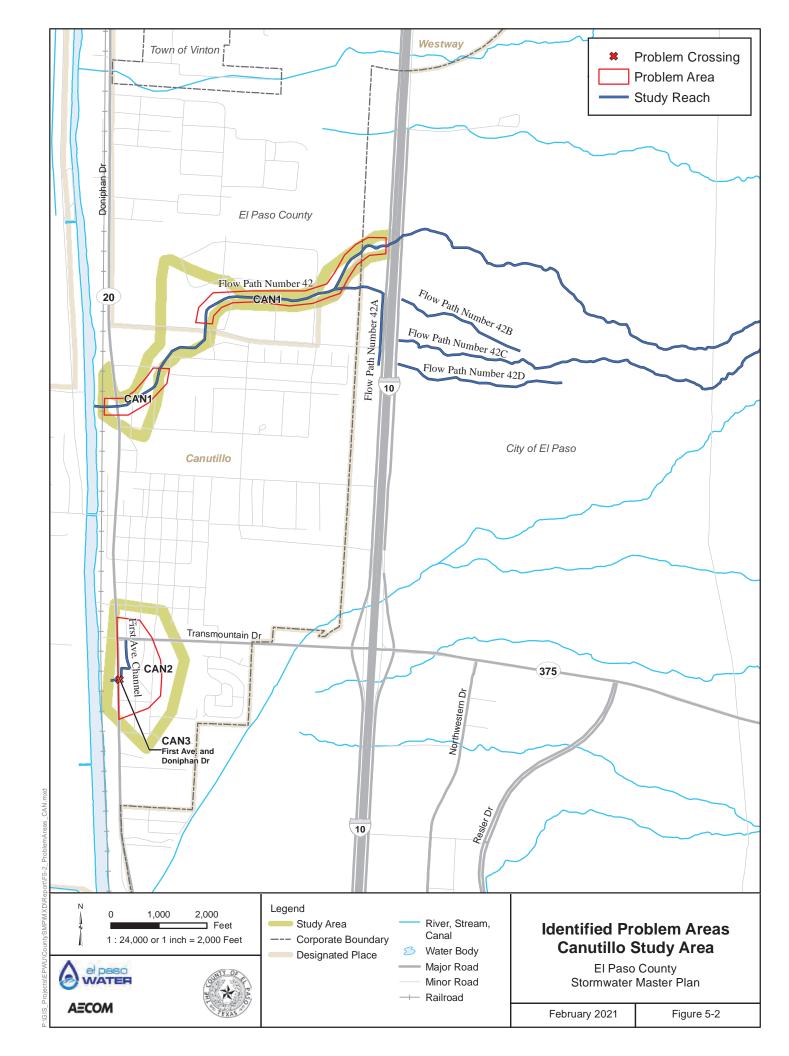
The at grade crossing at the intersection of Flowpath M-6 and Millicent Avenue does not have any culverts or openings to convey storm water or debris under the road. This crossing was identified by County officials as requiring frequent maintenance and serves as the only access point to several structures.

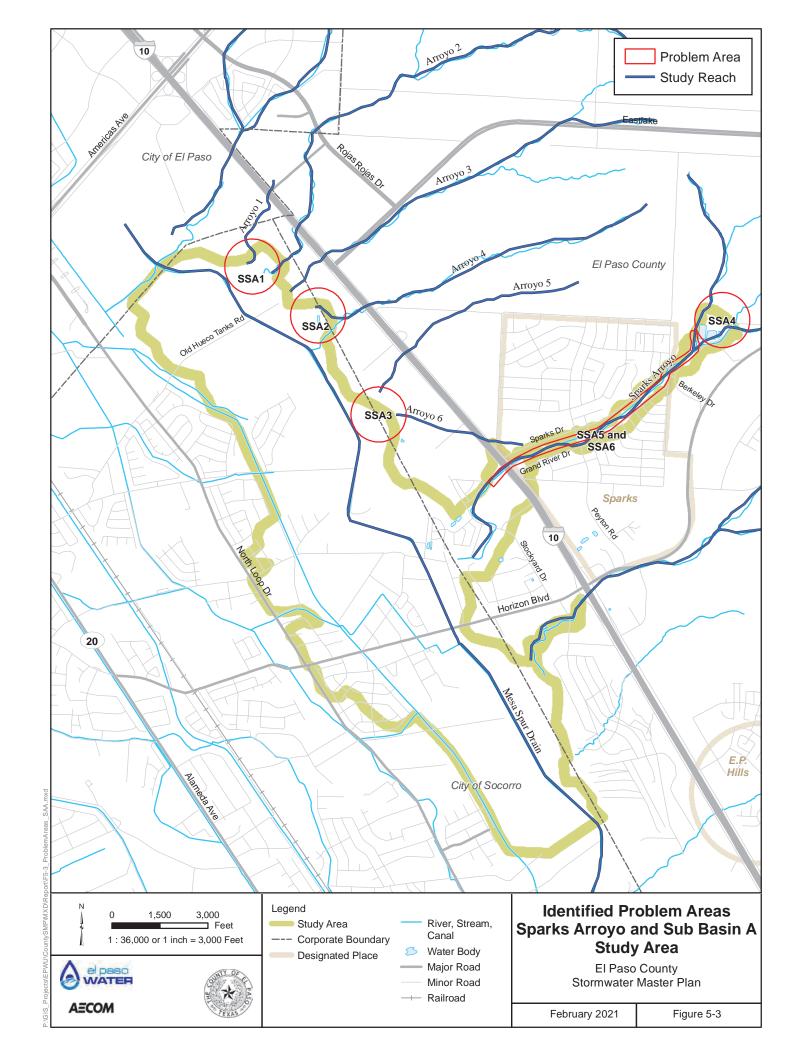
5.8.15 MON15

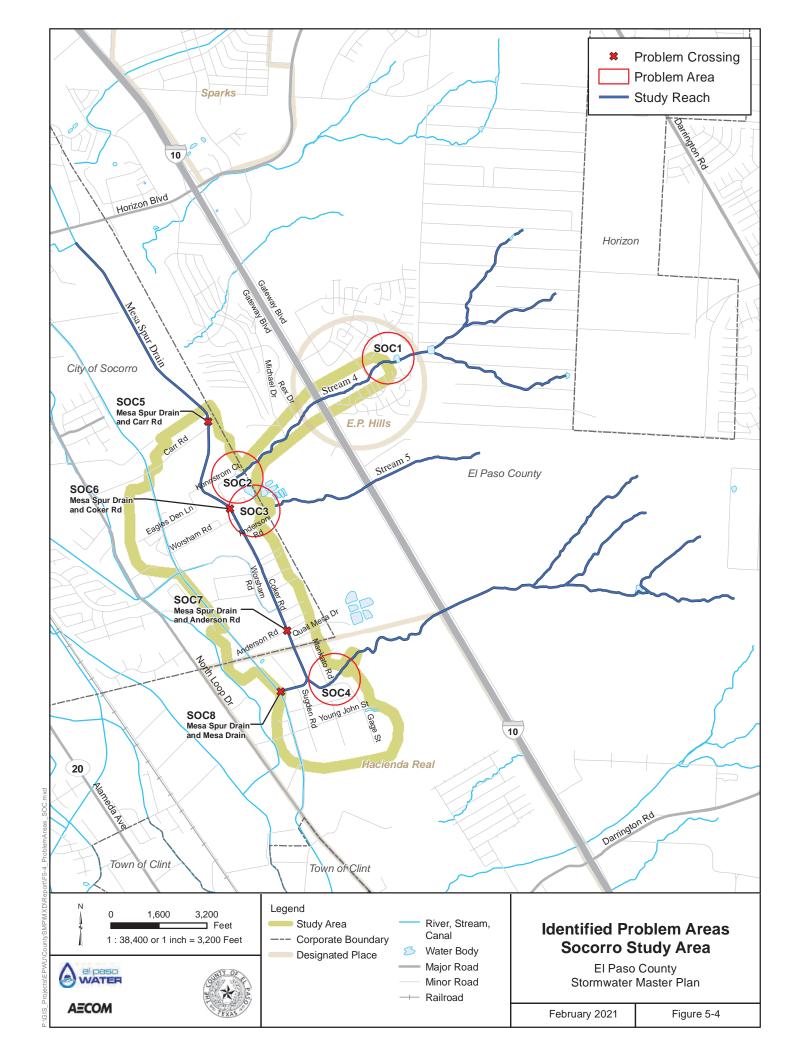
The at grade crossing at the intersection of Flowpath M-6 and Petty Prue Street does not have any culverts or openings to convey storm water or debris under the road. This crossing was

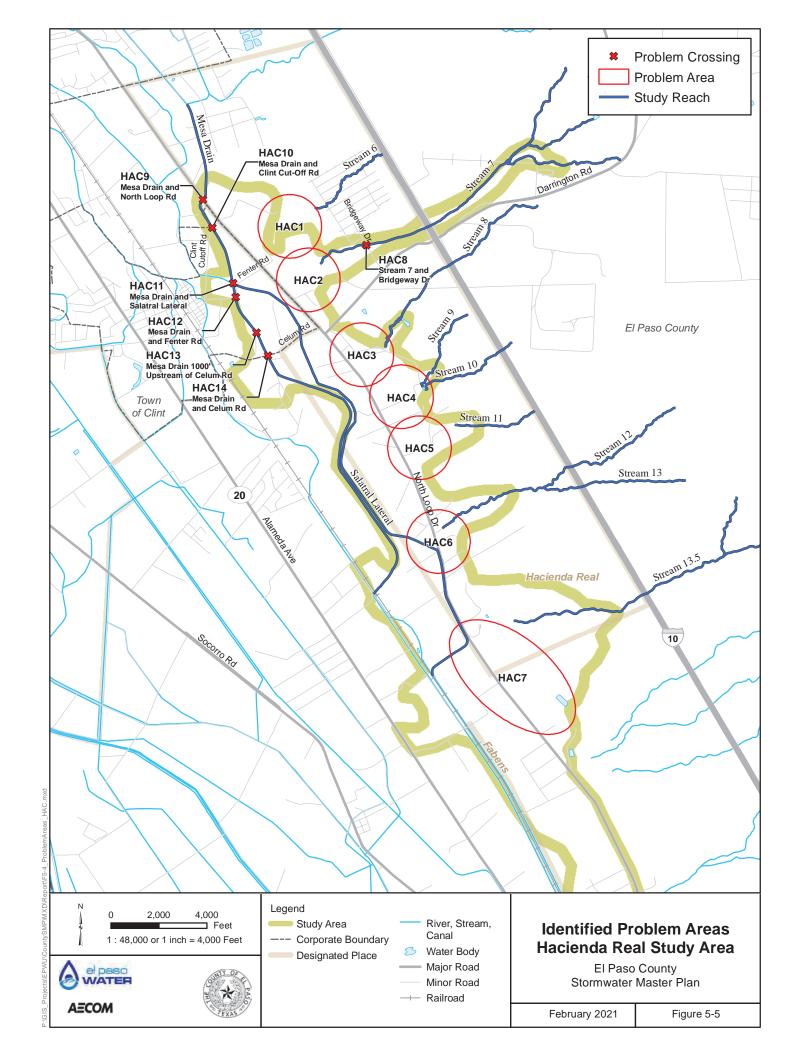
identified by County officials as requiring frequent maintenance and serves as the only access point to several structures.

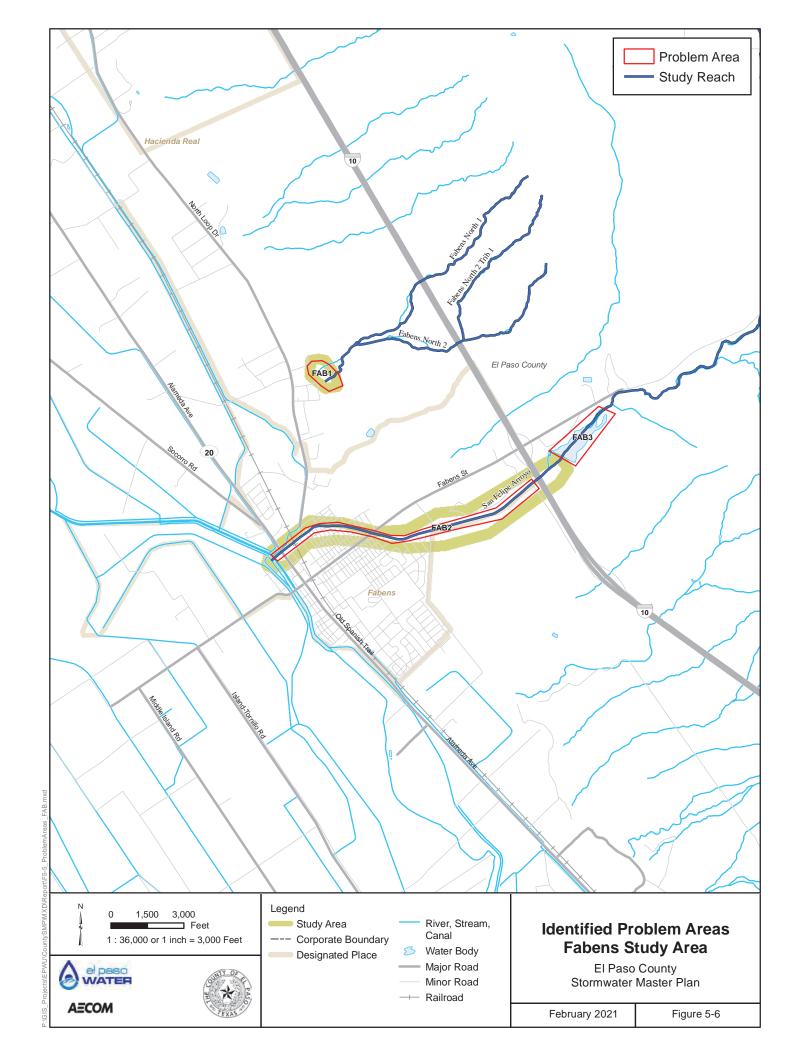


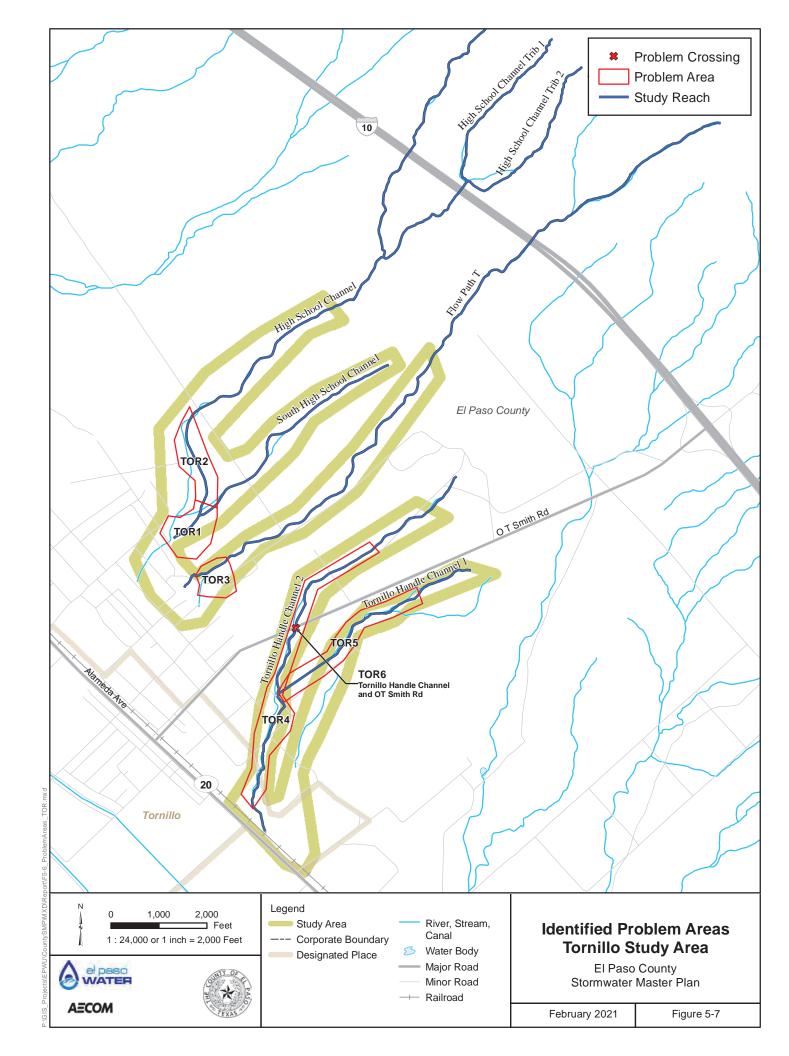


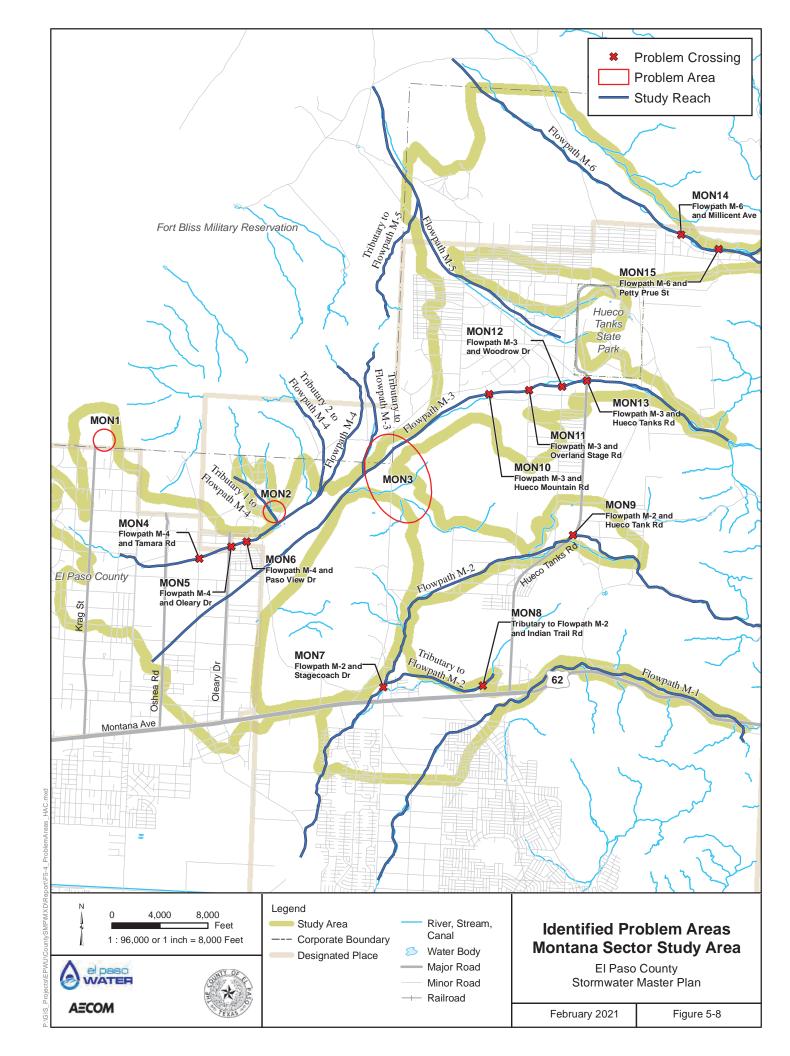












6.0 RECOMMENDED IMPROVEMENTS

As discussed in the earlier sections of the County SMP, stormwater infrastructure deficiencies were identified within each El Paso County Study Area. A series of project alternatives were developed to address these inadequacies. During working meetings with the County and EPW, the various alternatives were discussed and a preferred alternative was selected.

Projects and project costs can be found summarized in Table 6-1. All costs presented in this section are conceptual in nature and were estimated using the methodology provided in Appendix C.

The selected alternative for each project is discussed below. Information on the other alternatives can be found in Appendix C.

6.1 Vinton Study Area

The issues of concern within the Vinton Study Area are largely due to the lack of capacity and access to the drainage facilities along the natural arroyos. Large flows traveling down the mountainside carry a large amount of sediment. As the flow reaches the flatter residential area, the flow slows, depositing much of the sediment. The capacity of the arroyos have been reduced due to the lack of maintenance and residents filling the arroyo to utilize more of their property. To address these inadequacies in the current stormwater facilities, a series of projects was identified.

6.1.1 Specific Projects

6.1.1.1 Flow Path Number 45A Diversion (VIN1)

Figure 6-1 shows Flow Path Number 45 and a tributary to Flow Path Number 45 in the area immediately upstream of the El Paso Natural Gas (EPNG) Pipeline Road. Immediately upstream of the intersection of this tributary with the road, flows from the tributary split during floods, with the bulk of the flows proceeding southwest to the junctions with Flow Path Number 45. The remainder of the flood flow in this tributary heads due west across Westway Boulevard and the EPNG Pipeline Road. This flow is marked "Split Flow" on Figure 6-1. This "Split Flow" is shown on Figure 6-2 arriving from the east and entering Vinton near Banker Road, Flow Path Number 45A, and their intersection with Remington Drive. The "Split Flow" exceeds the capacity of the existing Flow Path Number 45A and causes flood damages in this part of Vinton and downstream to the immediate west.

Project VIN1 incorporates three improvements to address this issue. Basin A (Figure 6-1) is designed to capture flood flows and sediment from the tributary to Flow Path Number 45. A diversion channel (Figure 6-2) is designed parallel to and upstream of Remington Drive to intercept flood flows from the watershed downstream of Basin A. This diversion channel discharges into Flow Path Number 45 upstream of Tom Mays Drive. The diversion would increase flood flows in Flow Path Number 45 without a linked improvement along that channel. Basin B (Figure 6-1) is the proposed improvement on Flow Path Number 45. This basin intercepts flood and sediment flows from Flow Path Number 45; resulting in a net reduction of flows into Vinton along Flow Path Number 45. Project VIN3, which is for channel improvement within Vinton along Flow Path Number 45, is dependent upon the flow reductions achieved by Basins A and B.

The proposed basin on Flow Path Number 45 (Basin B on Figure 6-1) requires approximately 230 acre-feet of excavation for flood and sediment pool storage, and the proposed basin on the flow path contributing to Flow Path Number 45 (Basin A on Figure 6-1) requires approximately 440 acre-feet of excavation for flood and sediment pool storage. Sediment sources are identified in the upstream watershed of Flow Path Number 45 within the City SMP. The sediment portions of the basins are included to accommodate sediment laden flows from these sources.

The estimated cost of this project does not include the cost of property acquisition, as the basins are to be located on EPW property.

6.1.1.2 Flow Path Number 45A Channel Improvements (VIN2)

This project involves improvements to Flow Path Number 45A from approximately 230 feet upstream of Iron Drive to approximately 260 feet downstream of Kiely Road. The existing undersized channel is a V-ditch with a depth of approximately 2 feet and a top width of 40 feet. The proposed channel section is 5 feet deep, with 2 to 1 (horizontal to vertical) side slopes, and a bottom width of 15 feet. The purpose of these improvements is to provide sufficient capacity within the channel to convey the 100-year flood, assuming project VIN1 is completed. The remainder of the downstream channel has capacity for the 100-year flood. These proposed improvements are shown on Figure 6-3.

6.1.1.3 Flow Path Number 45 Upper Section (VIN3)

This project involves improvements to the upper portion of Flow Path Number 45 from Tom Mays Drive to De Alva Drive. The existing channel is a V-ditch that is 1.5 feet deep and has a top width of 45 feet. The proposed channel is 3 feet deep, has 2 to 1 side slopes, and a bottom width of 30 feet. The purpose of these improvements is to provide sufficient capacity within the channel to convey the 100-year flood, assuming project VIN1 is completed. There are currently low water crossings at Tom Mays Drive and De Alva Drive. It is recommended that these remain low water crossings. These proposed improvements are shown on Figure 6-2.

For VIN3 to be successful, VIN1 must be complete.

6.1.1.4 Flow Path Number 45 Middle Section (VIN4)

This project involves acquiring ROW property and making improvements to Flow Path Number 45 from southbound IH-10 on-ramp to the confluence of Flow Path Number 45A. The existing earthen channel is 4 feet deep, with 4 to 1 side slopes, and a bottom width of 2 feet. The proposed channel is earthen, 9.5 feet deep, with 2 to 1 side slopes, and a bottom width of 20 feet. The purpose of these improvements is to provide sufficient capacity within the channel to convey the 100-year flood, assuming project VIN1 is completed. These proposed improvements are shown on Figure 6-3.

6.1.1.5 Flow Path Number 44 (VIN5)

This project involves acquiring ROW property along Flow Path Number 44 within the residential area. This would allow the County to maintain this portion of the channel. In addition, this project involves 2,050 feet of channel improvements. The proposed earthen channel has a bottom width of approximately 25 feet, 3 to 1 side slopes, and would be approximately 6 feet

deep. The purpose of these improvements is to provide enough potential capacity to convey the 100-year flood. These proposed improvements are shown on Figure 6-4.

6.1.1.6 Doniphan Drive Crossing (VIN6)

This project involves removing the existing 16-foot by 5-foot CBC at the intersection of Flow Path Number 44 and Doniphan Drive and replacing it with four 9-foot by 8-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-4.

6.1.1.7 Railroad Crossing (VIN7)

This project involves replacing the existing bridge at the intersection of Flow Path Number 45 and the Railroad with a bridge that does not impede the flow of water in the channel. In order for the bridge to not impede flow, the bridge should match the channel geometry and the low chord of the bridge should be above the channel bank elevation. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing with overtopping the road. This proposed improvement is shown on Figure 6-5.

6.1.1.8 Doniphan Drive Crossing (VIN8)

This project involves replacing the existing two 6-foot by 6-foot CBCs at the intersection of Flow Path Number 45 and Doniphan Drive with a bridge that does not impede the flow of water in the channel. In order for the bridge to not impede flow, the bridge should match the channel geometry and the low chord of the bridge should be above the channel bank elevation. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-5.

6.1.1.9 AP Ramirez Street Crossing (VIN9)

This project involves replacing the existing four 36-inch CMPs at the intersection of Flow Path Number 45 and AP Ramirez Street with a bridge that does not impede the flow of water in the channel. In order for the bridge to not impede flow, the bridge should match the channel geometry and the low chord of the bridge should be above the channel bank elevation. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-3.

6.1.1.10 Kiely Road Crossing (VIN10)

This project involves replacing the existing two 8-foot by 3-foot CBCs at the intersection of Flow Path Number 45 and Kiely Road with a bridge that does not impede the flow of water in the channel. In order for the bridge to not impede flow, the bridge should match the channel geometry and the low chord of the bridge should be above the channel bank elevation. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-3.

6.1.1.11 Quejette Road Crossing (VIN11)

This project involves replacing the existing low water crossing at the intersection of Flow Path Number 45 and Quejette Road with a bridge that does not impede the flow of water in the channel. In order for the bridge to not impede flow, the bridge should match the channel geometry and the low chord of the bridge should be above the channel bank elevation. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-3.

6.1.1.12 IH-10 Northbound Off-ramp Crossing (VIN12)

This project involves the addition of 3 more barrels to the existing 13 barrel structure to make a total of sixteen 9-foot by 5-foot CBCs at the intersection of Flow Path Number 45 and the Northbound off-ramp of IH-10. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road, assuming project VIN1 is completed. This proposed improvement is shown on Figure 6-2.

For VIN12 to be successful, VIN1 must be complete.

6.1.1.13 Kiely Road Crossing with Flow Path Number 45A (VIN13)

This project involves replacing the existing two 30-inch RCPs at the intersection of Flow Path Number 45A and Kiely Road with five 7-foot by 4-foot CBCs. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-3.

6.1.1.14 Iron Drive Crossing (VIN14)

This project involves replacing the existing three 30-inch RCPs at the intersection of Flow Path Number 45A and Iron Drive with six 6-foot by 6-foot CBCs. The purpose of this improvement is to provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-3.

6.2 Canutillo Study Area

6.2.1 Specific Project

Flooding within the Canutillo Study Area is largely a result of a lack of flood and sediment control along the arroyos and within the residential area. Additionally, the lack of drainage facilities in urban areas results in the ponding of water in streets and in residential areas. To address these inadequacies in the current stormwater infrastructure, a series of projects was identified.

6.2.1.1 Flow Path Number 42 (CAN1)

This project involves constructing 1,240 feet of concrete lined channel along Flow Path Number 42, in addition to acquiring ROW property for maintenance of the channel. The proposed concrete channel will consist of a bottom width of approximately 30 feet, 2 to 1 side slopes, and would be approximately 5 feet deep. The purpose of these improvements is to provide sufficient

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capacity within the channel to convey the 100-year flood. These proposed improvements are shown on Figure 6-6.

Additionally, the section of channel located between IH-10 and Los Mochis Road is currently undeveloped. Future development must ensure the channel has capacity to convey the 100-year flood and provide necessary maintenance access to the County.

6.2.1.2 Localized Flooding along First Avenue Channel (CAN2)

This project involves constructing a retention basin on a currently vacant lot east of the intersection of West Avenue and Third Avenue. The proposed embankment is approximately 6 feet tall and provides approximately 21 acre-feet of storage for flood and sediment pool. This project also includes the construction of approximately 1,665 feet of 48-inch RCP storm drain to connect the proposed basin to an existing basin located north of Mowad Road. This storm drain will allow the two basins to act as inter-connected ponds during significant runoff events.

In addition, the project involves constructing a retention basin west of Doniphan Drive across from the flea market. Due to spatial limitations, this basin will not have the capacity to retain the 100-year flood; the basin will act as a temporary holding area and pumping will be required to remove water during significant runoff events. To direct flow to the temporary retention basin, the project calls for constructing 143 feet of concrete lined channel parallel to Doniphan Drive. The proposed channel has a bottom width of approximately 4 feet, 2 to 1 side slopes, and would be approximately 3 feet deep. As part of channel construction, the project requires the replacement of the existing two 12-inch polyvinyl chloride (PVC) pipes at the intersection of First Avenue Channel and West Avenue with a 6-foot by 3-foot CBC. These proposed improvements are shown on Figure 6-7.

6.2.1.3 Doniphan Drive Crossing (CAN3)

This project involves replacing the existing two 6-foot by 3-foot CBCs at the intersection of First Avenue Channel and Doniphan Drive with two 6-foot by 3-foot CBCs, ensuring the culvert is sloped to drain to the proposed basin. Although the existing culvert size provides sufficient capacity, the culvert is not sloping in the correct direction. The proposed culvert size and placement will provide sufficient capacity for the 100-year flood to be conveyed through the crossing without overtopping the road. This proposed improvement is shown on Figure 6-7.

6.3 Sparks Arroyo and Sub Basin A Study Area

Flooding within the Sparks Arroyo and Sub Basin A Study Area is largely a result of a lack of flood and sediment control structures along the natural arroyos. Large flows from the high mesa are uncontrolled and become loaded with sediment as they approach the valley below. When these flows reach the valley, they spread out and sheet flow, forming alluvial fans. In addition, there are capacity and stability issues with the Sparks Arroyo, which runs through the Sparks urban area.

As discussed earlier, the USACE has a ongoing feasibility study evaluating the drainage problems along Sparks Arroyo and Sub Basin A. Seven projects were developed (SSA1 – SSA6) to address these problems based on the general hydrologic information provided by the USACE. The final projects proposed by the USACE may differ from the projects (SSA1 – SSA6) discussed in the following sections.

6.3.1 Specific Projects

6.3.1.1 A1-A3 Basin (SSA1)

This project involves constructing a detention basin at the lower end of Arroyos 1, 2, and 3. The proposed embankment is approximately 41 feet tall and requires approximately 395 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot RCP. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-8.

6.3.1.2 A4 Basin (SSA2)

This project involves constructing a detention basin at the lower end of Arroyo 4. The proposed embankment is approximately 22 feet tall and requires approximately 65 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot RCP. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-8.

6.3.1.3 A5-A6 Basin (SSA3)

This project involves constructing a detention basin near the lower end of Arroyos 5 and 6 at a location owned by the County. The proposed basin approximately 21 feet deep and requires approximately 106 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot RCP. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-9.

6.3.1.4 Sparks Basin (SSA4)

This project involves constructing a detention basin at the upper end of the Sparks Arroyo, just upstream of the WWTP. The proposed basin requires approximately 550 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 4-foot RCP. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-10.

6.3.1.5 Sparks Arroyo (SSA5)

This project involves reshaping and lining approximately 10,300 feet of the Sparks Arroyo, between the proposed Sparks Basin and Stockyard Drive. The proposed channel has a bottom width of approximately 25 feet, 3 to 1 side slopes, and is approximately 5 feet deep. The purpose of the improvements is to stabilize the channel to prevent further erosion and encroachment into adjacent properties. In addition, a crossing structure consisting of six 10-foot by 4-foot CBCs is proposed at Stockyard Drive. These proposed improvements are shown on Figure 6-10.

6.3.1.6 Sparks Ponds (SSA6)

This project involves constructing two retention basins within the Sparks Community along the east side of the Sparks Arroyo. The proposed upper basin (Basin B) is constructed by excavating a basin that is currently owned by the County to a capacity of approximately 8 acrefeet. In addition, concrete lined channels to the north and south of the basin are proposed to intercept flow from the community and divert it to the basin. The proposed lower basin is constructed by excavating approximately 13 acre-feet from an empty lot. In addition, concrete lined channels to the north and south of the basin are proposed to intercept flow from the community and divert it to the basin. The purpose of the improvements is to prevent additional flow and sediment from the Sparks Community from entering the Sparks Arroyo. These proposed improvements are shown on Figure 6-10.

6.4 Socorro Study Area

Flooding within the Socorro Study Area is largely a result of a lack of flood and sediment control structures along the natural arroyos. Large flows from the high mesa are uncontrolled and become loaded with sediment as they approach the valley below. When these flows reach the valley, they spread out and sheet flow, forming alluvial fans. To address these inadequacies in the current stormwater infrastructure, a series of projects was identified.

6.4.1 Specific Projects

6.4.1.1 El Paso Hills Basin Repair (SOC1)

This project involves repairing the existing basin embankment at the EI Paso Hills Detention Basin. The basin embankment failed as a result of a large storm and has not been repaired. The proposed embankment cannot be constructed any higher than the existing embankment, as it would cause flooding of nearby residences, but some additional flood and sediment pool storage can be provided by excavation. Approximately 38 acre-feet of excavation is required for additional flood and sediment pool storage. The outlet structure for this basin consists of two 3-foot by 3-foot CBCs. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements require that the basin be acquired by El Paso County before they can be made. These improvements are also predicated on the assumption that documents can be provided that demonstrate that the original embankment was properly engineered, constructed, and approved. These proposed improvements are shown on Figure 6-12.

6.4.1.2 Stream 4 Basin (SOC2)

This project involves constructing a detention basin at the lower end of Stream 4, below the El Paso Hills Detention Basin. The proposed embankment is approximately 30 feet tall and requires approximately 59 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-13.

6.4.1.3 Stream 5 Basin (SOC3)

This project involves constructing a detention basin at the lower end of Stream 5. The proposed embankment is approximately 26 feet tall and requires approximately 9 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-14.

6.4.1.4 Stream 5.5 Basin (SOC4)

This project involves constructing a detention basin at the lower end of Stream 5.5. The proposed embankment is approximately 29 feet tall and requires approximately 11 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and

2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-15.

6.4.1.5 Carr Road Crossing (SOC5)

This project involves removing the existing 48-inch CMP culvert at the intersection of the Mesa Spur Drain and Carr Road and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-16.

6.4.1.6 Coker Road Crossing (SOC6)

This project involves removing the existing 48-inch CMP culvert at the intersection of the Mesa Spur Drain and Coker Road and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-16.

6.4.1.7 Anderson Road Crossing (SOC7)

This project involves removing the existing 48-inch CMP culvert at the intersection of the Mesa Spur Drain and Anderson Road and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-17.

6.4.1.8 Mesa Drain Crossing (SOC8)

This project involves removing the existing 60-inch CMP culvert at the intersection of the Mesa Spur Drain and the Mesa Drain and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-17.

6.5 Hacienda Real Study Area

Flooding within the Hacienda Real Study Area is largely a result of a lack of flood and sediment control structures along the natural arroyos. Additionally, several crossings in the study area are undersized. To address these inadequacies in the current stormwater infrastructure, a series of projects was identified.

6.5.1 Specific Projects

6.5.1.1 Stream 6 Basin Outlet (HAC1)

This project involves expanding two existing retention basins at the end of Stream 6. Although the existing basins are providing some benefit in its current state, they are not sized and cannot be expanded to such a size that will handle the 100-year flood flows from Stream 6. The proposed improvements include expanding Basin A from 760'x200' to bottom dimensions of 760'x300' with 3:1 side slopes, and expanding Basin B from 260'x100' to bottom dimensions of 260'x200' with 3:1 side slopes. These proposed improvements are shown on Figure 6-18.

6.5.1.2 Stream 7 Basins (HAC2)

This project involves constructing two detention basins along Stream 7. The proposed Basin B requires approximately 115 acre-feet of excavation for flood and sediment pool storage. The proposed Basin A requires approximately 880 acre-feet of excavation for flood and sediment pool storage. The basins have two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Retain the flood flows coming down the arroyos and allow minimal releases.

These proposed improvements are shown on Figure 6-19.

6.5.1.3 Stream 8 Basin (HAC3)

This project involves constructing a retention basin at the lower end of Stream 8. The proposed embankment is approximately 6 feet tall and requires approximately 68 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Retain the flood flows coming down the arroyos and allow minimal releases.

These proposed improvements are shown on Figure 6-18.

6.5.1.4 Streams 9 and 10 Basin (HAC4)

This project involves constructing a retention basin at the lower end of Streams 9 and 10. The proposed embankment is approximately 6 feet tall and requires approximately 39 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Retain the flood flows coming down the arroyos and allow minimal releases.

These proposed improvements are shown on Figure 6-20.

6.5.1.5 Stream 11 Basin (HAC5)

This project involves constructing a retention basin at the lower end of Stream 11. The proposed embankment is approximately 6 feet tall and requires approximately 65 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Retain the flood flows coming down the arroyos and allow minimal releases.

These proposed improvements are shown on Figure 6-20.

6.5.1.6 Streams 12 and 13 Basin (HAC6)

This project involves constructing a retention basin below the convergence of Streams 12 and 13. The proposed embankment is approximately 6 feet tall and requires approximately 136 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-21.

6.5.1.7 Stream 13.5 Basin (HAC7)

This project involves constructing two basins along Stream 13.5. The proposed upper retention basin (Basin B) controls flows from the upper end of the watershed. The proposed Basin B requires approximately 295 acre-feet of excavation for flood and sediment pool storage. The proposed lower basin (Basin A) controls the flows accumulating within the watershed below the upper basin. The proposed embankment for Basin A is approximately 6 feet tall and requires approximately 4 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of two 4-foot by 4-foot CBCs. The basins have two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Retain/Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-21.

6.5.1.8 Bridgeway Drive Crossing (HAC8)

This alternative involves removing the existing five 48-inch CMP culverts at the intersection of Stream 7 and Bridgeway Drive and replacing them with six 4-foot by 4-foot CBCs. This culvert

size provides sufficient capacity if additional storage is provided upstream per HAC2. These proposed improvements are shown on Figure 6-22.

6.5.1.9 North Loop Drive Crossing (HAC9)

This alternative involves removing the existing 60-inch RCP culvert at the intersection of the Mesa Drain and Northloop Drive and replacing it with three 5-foot by 4-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-22.

6.5.1.10 FM 1110 Crossing (HAC10)

This alternative involves removing the existing 42-inch CMP culvert at the intersection of the Mesa Drain and FM 1110 and replacing it with two 8-foot by 7-foot CBCs. This culvert size provides capacity slightly lower than that of channel immediately upstream, but provides the maximum opening allowable for crossing and channel geometry. The existing culvert is collapsed and was identified as a problem crossing. These proposed improvements are shown on Figure 6-22.

6.5.1.11 Salatral Lateral Crossing (HAC11)

This alternative involves removing the existing 36-inch RCP culvert at the intersection of the Mesa Drain and Salatral Lateral and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-22.

6.5.1.12 Fenter Road Crossing (HAC12)

This alternative involves removing the existing 72-inch CMP culvert at the intersection of the Mesa Drain and Fenter Road and replacing it with two 8-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-22.

6.5.1.13 Dirt Road Upstream of Celum Road Crossing (HAC13)

This alternative involves removing the existing 54-inch CMP culvert at the intersection of the Mesa Drain and the dirt road just upstream of Celum Road and replacing it with two 8-foot by 7-foot CBCs. This culvert size provides capacity slightly lower than that of channel immediately upstream, but provides the maximum opening allowable for crossing and channel geometry. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-22.

6.5.1.14 Celum Road Crossing (HAC14)

This alternative involves removing the existing 36-inch CMP culvert at the intersection of the Mesa Drain and Celum Road and replacing it with two 8-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel. Although this crossing was not identified as a problem crossing by the County, this project was included because the existing culvert could restrict the flow of the channel if it were flowing bank-full. These proposed improvements are shown on Figure 6-22.

6.6 Fabens Study Area

The issues of concern within the Fabens Study Area are largely due to the lack of access to the drainage facilities along the arroyos. Additionally, the capacity of flood and sediment control structures is inadequate. To address these inadequacies in the current stormwater facilities, a series of projects was identified.

6.6.1 Specific Projects

6.6.1.1 Fabens North 1 Basin (FAB1)

This project involves repairing the existing basin embankment at the downstream end of Fabens North 1 Arroyo, where the existing basin is currently located, and acquiring ROW property on which the basin lies. The basin embankment failed as a result of a large storm event and has not been repaired because the County does not currently have ownership of the basin. The property acquisition will allow the County to repair and maintain the basin as needed. The basin embankment failed as a result of a large storm event and has not been repaired due to ownership issues. The proposed embankment is approximately 15 feet tall and requires approximately 30 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot by 2-foot CBC. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-23.

6.6.1.2 San Felipe Arroyo (FAB2)

This project involves acquiring ROW property along the channel within the residential area. The channel currently has no identified capacity issues at this time. This project is a preventative measure to ensure the channel continues to function without significant issues, by providing the County with necessary access to continue to maintain the channel and protect the residents of Fabens. This proposed improvement is shown on Figure 6-23.

6.6.1.3 Fabens Dam (FAB3)

Fabens Dam is the only TCEQ regulated dam owned by the County. TCEQ regulations require that a dam of this size pass 75% of the PMP event without overtopping and potentially breaching the dam. The PMP is much larger than the 100-year storm event and is intended to

ensure protection of downstream residents during the most severe storm events. This project consists of constructing approximately 1,165 feet of 4-foot-high concrete parapet wall along the crest of the current dam embankment. In addition, it is required that the east auxiliary spillway be widened 100 feet to a total width of approximately 150 feet. With these improvements, the dam should be able to safely pass the regulatory flood. These proposed improvements are shown in Figure 6-24.

6.7 Tornillo Study Area

Flooding within the Tornillo Study Area is largely a result of a lack of flood and sediment control structures along the natural arroyos. Large flows upstream of the town of Tornillo become loaded with sediment as they approach the town. When these flows from the steep arroyo meet the flatter terrain of the urban area, the sediment is deposited. The arroyo lacks a defined channel in this area of deposition and flood flows are uncontrolled and may cause damage. To address these inadequacies in the current stormwater facilities, a series of projects was identified.

6.7.1 Specific Projects

6.7.1.1 High School Channel (TOR1)

This project involves constructing a retention basin (Basin B) on currently vacant land southeast of the high school at the end of High School Channel, South High School Channel, and Flow Path T. The project consists of improving and extending the existing embankment to catch flow conveyed through all three channels. The proposed embankment is approximately 6 feet tall. The proposed basin is approximately 4 feet deep and requires approximately 54 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot by 2-foot CBC. The purpose of the basin is to retain flows and sediment conveyed by the three channels mentioned above and release them at a controlled rate. Additionally, the project involves constructing a sediment basin (Basin A) upstream on High School Channel at the convergence of High School Channel and High School Channel Trib. 1. This proposed sediment basin is approximately 3-feet deep and requires approximately 5 acre-feet of excavation for sediment pool storage. This sediment basin will assist the lower flood control basin at the bottom of the channel by reducing the sediment load reaching the lower basin. These proposed improvements are shown on Figure 6-25.

6.7.1.2 High School Channel Embankment (TOR2)

This project involves improving the west bank of the diversion channel northeast of the high school. The channel bank improvement consists of 2,030 feet of 5 to 1 side slope riprap reinforcement along the west bank of the existing channel. Channel configuration is not expected to change. The proposed improvements are shown on Figure 6-25.

6.7.1.3 Flow Path T (TOR3)

The project involves constructing a sediment basin upstream on Flow Path T, just upstream of IH-10. The proposed sediment basin is approximately 2-feet deep and requires approximately 3 acre-feet of excavation for sediment pool storage. This sediment basin will assist the lower flood control basin at the bottom of the channel by reducing the sediment load reaching the

lower basin. The proposed basin does not require an embankment. These proposed improvements are shown on Figure 6-25.

If the retention basin (Basin B) discussed in TOR1 has not been constructed prior to this project, it should be constructed as part of this project.

6.7.1.4 Tornillo Handle Channel 2 (TOR4)

This project involves constructing a retention basin on currently vacant land at the confluence of Tornillo Handle Channel 1 and Tornillo Handle Channel 2. The proposed embankment is approximately 10 feet tall. The proposed basin requires approximately 8 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot by 2-foot CBC. The purpose of the basin is to retain flows and sediment conveyed by the Tornillo Handle Channel 1 and Tornillo Handle Channel 2 and release them at a controlled rate. These proposed improvements are shown on Figure 6-26.

6.7.1.5 Tornillo Handle Channel 1 (TOR5)

This project involves the improvement of the existing embankment of the south bank of Tornillo Handle Channel 1. The project does not include any change to the configuration of the channel. The channel bank improvement consists of 1,650 feet of 3 to 1 side slope riprap reinforcement along the south bank. If the retention basin discussed in TOR4 has not been constructed prior to this project, it should be constructed as part of this project. These proposed improvements are shown on Figure 6-26.

6.7.1.6 OT Smith Road Crossing (TOR6)

This project involves replacing the existing two 36-inch pipes at the intersection of Tornillo Handle Channel 2 and OT Smith Road with two 5-foot by 2-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-26.

6.8 Montana Sector Study Area

Flooding within the Montana Study Area is a result of a lack of adequately sized culvert crossings and a lack of flood and sediment control structures along the natural arroyos. Large flows from the Hueco Mountains convey large amounts of sediment down arroyos through the populated areas. When these flows from the steep arroyo meet the flatter terrain of the urban area, the sediment is deposited. The arroyos lack a defined channel in this area of deposition and flood flows are uncontrolled and may cause damage. To address these inadequacies in the current stormwater facilities, a series of projects was identified.

6.7.2 Specific Projects

6.7.2.1 Montana Sector Basin #1 (MON1)

This project involves constructing a retention basin on land that is currently part of the Fort Bliss Military Reservation. The proposed basin requires approximately 750 acre-feet of excavation for flood and sediment pool storage. The basin's primary purpose is to retain flood water.

These proposed improvements are shown on Figure 6-27.

6.7.2.2 Montana Sector Basin #2 (MON2)

This project involves constructing a retention basin at the base of Tributary 1 to Flowpath M-4. The proposed basin requires approximately 378 acre-feet of excavation for flood and sediment pool storage. The basin has two primary purposes:

- 1. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 2. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-28.

6.7.2.3 Montana Sector Basin #3 (MON3)

This project involves constructing a detention basin on Flowpath M-3. The proposed basin controls flows from the upper end of the watershed and contains two embankments. The proposed embankments for the basin are approximately 25 feet tall and 27 feet tall, and require approximately 4 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of two 4-foot by 4-foot CBCs. The basin has two primary purposes:

- 3. Capture sediment being transported down the arroyos and reduce deposition in the downstream channels and floodplains; and
- 4. Detain the flood flows coming down the arroyos and release them slowly from the detention basin at a rate that will reduce flooding downstream.

These proposed improvements are shown on Figure 6-29.

6.7.2.4 Tamara Road Crossing (MON4)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-4 and Tamara Road with seven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-28.

6.7.2.5 Oleary Drive Crossing (MON5)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-4 and Oleary Drive with seven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-28.

6.7.2.6 Paso View Drive Crossing (MON6)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-4 and Paso View Drive with seven 9-foot by 5-foot CBCs. This culvert size will provide sufficient

capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-28.

6.7.2.7 Stagecoach Drive Crossing (MON7)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-2 and Stagecoach Drive with four 7-foot by 4-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-32.

6.7.2.8 Indian Trail Road Crossing (MON8)

This project involves replacing the existing at grade crossing at the intersection of Tributary to Flowpath M-2 and Indian Trail Road with seven 8-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-32.

6.7.2.9 Hueco Tanks Road South Crossing (MON9)

This project involves replacing the existing 2-24" corrugate metal pipe culverts at the intersection of Flowpath M-2 and Hueco Tanks Road with six 7-foot by 4-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-33.

6.7.2.10 Hueco Mountain Road Crossing (MON10)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-3 and Hueco Mountain Road with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-30.

6.7.2.11 Overland Stage Road Crossing (MON11)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-3 and Hueco Mountain Road with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-30.

6.7.2.12 Woodrow Drive Crossing (MON12)

This project involves replacing the existing 5 concrete box culverts at the intersection of Flowpath M-3 and Woodrow Drive with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-30.

6.7.2.13 Hueco Tanks Road North Crossing (MON13)

This project involves replacing the existing 3 - 24" corrugated metal pipe culverts at the intersection of Flowpath M-3 and Hueco Tanks Road with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-30.

6.7.2.14 Millicent Avenue Crossing (MON14)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-6 and Millicent Avenue with fourteen 12-foot by 9-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-31.

6.7.2.15 Petty Prue Street Crossing (MON15)

This project involves replacing the existing at grade crossing at the intersection of Flowpath M-6 and Petty Prue Street with fourteen 12-foot by 9-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing. This proposed improvement is shown on Figure 6-31.

6.9 Summary

Table 6-1 shows a summary of all the selected projects and their estimated costs. Detailed cost estimates are included in Appendix C.

Table 6-1. Stormwater Projects

Study	Project			
Area	No.	Issue to be addressed	Description of Improvements	Total Cost
Vinton	VIN1*	Flooding along channel due to uncontrolled flows from Flow Path Number 45A and Flow Path Number 45.	This project involves constructing a diversion channel upstream of Remington Drive directing the flow to Flow Path Number 45, and two combination sediment/detention basins. One basin on the north portion of the upper watershed (Basin A) and the other on the south portion of the upper watershed (Basin B). Basin A will be 24 feet high. Approximately 440 acre-feet of excavation will be required for flood and sediment pool storage. A principal outlet and an earthen auxiliary spillway will be included in the design. Basin B will be 23 feet high. Approximately 230 acrefeet of excavation will be required for flood and sediment pool storage. A principal outlet and an earthen auxiliary spillway will be included in the design.	\$29,500,000
Vinton	VIN2	Area flooding due to uncontrolled flows from Flow Path Number 45A.	This project involves increasing 950 feet of the lower portion of Flow Path Number 45A channel capacity from 240 feet upstream of Iron Drive to 260 feet downstream of Kiely Road.	\$330,000
Vinton	VIN3	Area flooding due to uncontrolled flows from Flow Path Number 45.	This project involves increasing 1,600 feet of the upper portion of Flow Path Number 45 channel capacity to convey the outflow of the basins associated with VIN1. The effectiveness of VIN3 is dependent on VIN1 being constructed.	\$160,000
Vinton	VIN4	Area flooding due to uncontrolled flows from Flow Path Number 45.	This project involves increasing 4,500 feet of the middle portion of Flow Path Number 45 channel capacity to convey the outflow of the basins associated with VIN1.	\$1,170,000
Vinton	VIN5	Downstream flooding due to uncontrolled flows from Flow Path Number 44.	This project involves increasing 2,054 feet of Flow Path Number 44 channel capacity to convey the 100-year flood.	\$1,210,000
Vinton	VIN6	Crossing capacity at Doniphan Drive and Flow Path Number 44 is less than the necessary capacity.	This project involves removing the existing 16-foot by 5-foot culvert and replacing it with three 9-foot by 8-foot culverts. This culvert size provides sufficient capacity equal to the upstream channel.	\$880,000
Vinton	VIN7	Crossing capacity at Railroad and Flow Path Number 45 is less than the necessary capacity.	This project involves expanding the existing bridge to cross the improved channel. This will provide sufficient capacity equal to the channel improvements.	\$830,000
Vinton	VIN8	Crossing capacity at Doniphan Drive and Flow Path Number 45 is less than the necessary capacity.	This project involves removing the existing two 6-foot by 6-foot culverts and replacing it with a bridge. This will provide sufficient capacity equal to the upstream channel.	\$1,700,000
Vinton	VIN9	Crossing capacity at AP Ramirez and Flow Path Number 45 is less than the necessary capacity.	This project involves removing the existing four 36-inch culverts and replacing it with a bridge. This will provide sufficient capacity equal to the upstream channel.	\$1,910,000
Vinton	VIN10	Crossing capacity at Kiely Road and Flow Path Number 45 is less than the necessary capacity.	This project involves removing the existing two 8-foot by 3-foot culverts and replacing it with a bridge. This will provide sufficient capacity equal to the upstream channel.	\$990,000
Vinton	VIN11	Crossing capacity at Quejette Drive and Flow Path Number 45 is less than the necessary capacity.	This project involves removing the at grade crossing and replacing it with a bridge. This will provide sufficient capacity equal to the upstream channel.	\$940,000
Vinton	VIN12	Crossing capacity at IH-10 Northbound off-ramp and Flow Path Number 45 is less than the necessary capacity.	This project involves adding three more 9-foot by 5-foot culverts to the existing battery of culverts. This addition of culverts provides sufficient capacity equal to the upstream channel.	\$270,000

Table 6-1. Stormwater Projects (Continued)

Study	Project			
Area	No.	Issue to be addressed	Description of Improvements	Total Cost
Vinton	VIN13	Crossing capacity at Kiely Road and Flow Path Number 45A is less than the necessary capacity.	This project involves removing the existing two 30-inch round concrete pipes and replacing it with five 7-foot by 4-foot culverts. This culvert size provides sufficient capacity equal to the upstream channel.	\$340,000
Vinton	VIN14	Crossing capacity at Iron Drive and Flow Path Number 45A is less than the necessary capacity.	This project involves removing the existing three 30-inch round concrete pipes and replacing them with six 6-foot by 6-foot culverts. This culvert size provides sufficient capacity equal to the upstream channel.	\$420,000
Canutillo	CAN1	Downstream flooding and sediment load due to uncontrolled flows from Flow Path Number 42 and lack of maintenance of channel due to ROW issues.	This project involves reconstructing the channel to convey the 100-year flood, with a concrete lining. Additionally, properties that extend into the channel will need to be acquired.	\$1,960,000
Canutillo	CAN2	Localized flooding due to lack of flood control structures.	This project involves constructing two retention basins and utilizing an existing basin. One of the constructed basins (Basin B) will be located at the downstream end of First Avenue Channel and the second (Basin A) in a vacant area east of the intersection of West Avenue and Third Avenue. Basin B will not require an embankment. Approximately 11 acre-feet of excavation will be required for flood pool storage. Basin A will be 6 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Approximately 21 acre-feet of excavation will be required for flood pool storage, of which a portion will be covered with a clay blanket. A low flow principal spillway will be included to convey flow as Basin A reaches capacity. Additionally, improvements will be made to First Avenue Channel.	\$6,030,000
Canutillo	CAN3	Crossing capacity at Doniphan Drive and First Avenue Channel is less than the necessary capacity.	This project involves removing the existing two 6-foot by 3-foot culvert and replacing it with the same size culvert, ensuring the culvert in sloping in the correct direction to drain. This culvert size provides sufficient capacity provided that additional storage is provided upstream per CAN2.	\$200,000
Sparks Arroyo and Sub Basin A	SSA1	Uncontrolled flows from Arroyos A1, A2, and A3 are causing flooding problems in downstream communities.	This project involves constructing a detention basin that will capture flow from Arroyos A1, A2, and A3. The basin will be 41 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 10 feet of freeboard for PMP event. Approximately 306 acre-feet of excavation will be required for flood pool storage, of which a portion will be covered with a clay blanket. Approximately 1,041 acre-feet of flood and sediment pool storage will be provided by this basin.	\$34,530,000
Sparks Arroyo and Sub Basin A	SSA2	Uncontrolled flows from Arroyo A4 are causing flooding problems in downstream communities.	This project involves constructing a detention basin that will capture flow from Arroyo A4. The basin will be 22 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 6 feet of freeboard for PMP event. Approximately 46 acre-feet of excavation will be required for flood pool storage, of which a portion will be covered with a clay blanket. Approximately 121 acre-feet of flood and sediment pool storage will be provided by this basin.	\$7,190,000

Table 6-1. Stormwater Projects (Continued)

Study	Project			
Area	No.	Issue to be addressed	Description of Improvements	Total Cost
Sparks Arroyo and Sub Basin A	SSA3	Uncontrolled flows from Arroyos A5 and A6 are causing flooding problems in downstream communities.	This project involves constructing a detention basin near the lower end of Arroyos 5 and 6 at a location owned by the County. The proposed basin approximately 21 feet deep and requires approximately 106 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 2-foot RCP.	\$1,510,000
Sparks Arroyo and Sub Basin A	SSA4	Flows entering the Sparks Arroyo from the upstream mesa are creating capacity issues for the arroyo and flooding problems downstream.	This project involves constructing a detention basin at the upper end of the Sparks Arroyo, just upstream of the WWTP. The proposed basin requires approximately 550 acre-feet of excavation for flood and sediment pool storage. The outlet structure for this basin consists of a 4 foot RCP.	\$7,400,000
Sparks Arroyo and Sub Basin A	SSA5	The Sparks Arroyo is currently experiencing erosion along its banks.	This project involves defining the Sparks Arroyo and lining it with concrete to prevent further erosion and add capacity. Approximately 10,300 feet of channel improvements. In addition, a crossing will need to be constructed under Stockyard Drive.	\$12,300,000
Sparks Arroyo and Sub Basin A	SSA6	Runoff from the Sparks Community is contributing to flooding problems downstream of the Sparks Arroyo.	This project involves constructing two retention basins within the Sparks Community west of the Sparks Arroyo. The north basin will need to be excavated to a volume of approximately 8 acrefeet and will have a 940-foot long concrete lined channel diverting water to it from the north and a 390-foot concrete lined channel from the south. The south basin will need to be excavated to a volume of approximately 13 acre-feet and will have a 980-foot long concrete lined channel diverting water to it from the north and a 250-foot concrete lined channel from the south.	\$2,700,000
Socorro	SOC1	Downstream flooding and sediment load due to uncontrolled flows from Stream 4 passing through the breached El Paso Hills Dam.	This project involves repairing the existing 15-foot-high embankment, adding 18-inch riprap to the interior embankment, adding principal and auxiliary spillways, and excavating approximately 33 acre-feet from the basin to provide flood and sediment pool storage.	\$1,690,000
Socorro	SOC2	Downstream flooding and sediment load due to uncontrolled flows from Stream 4.	This project involves constructing a combination sediment/detention basin at the base of Stream 4, downstream of SOC1. The basin embankment will be 30 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 5 feet of freeboard for PMP event. Approximately 51 acre-feet of excavation will be required for flood and sediment pool storage, of which a portion will be covered with a clay blanket. A box culvert principal outlet and an earthen auxiliary spillway will be included in the design.	\$3,270,000
Socorro	SOC3	Downstream flooding and sediment load due to uncontrolled flows from Stream 5.	This project involves constructing a combination sediment/detention basin at the base of Stream 5. The basin embankment will be 26 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 5 feet of freeboard for PMP event. Approximately 8 acre-feet of excavation will be required for flood and sediment pool storage, of which a portion will be covered with a clay blanket. A box culvert principal outlet and an earthen auxiliary spillway will be included in the design.	\$1,100,000
Socorro	SOC4	Downstream flooding and sediment load due to uncontrolled flows from Stream 5.5.	This project involves constructing a combination sediment/detention basin at the base of Stream 5.5. The basin embankment will be 29 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 5 feet of freeboard for PMP event. Approximately 10 acre-feet of excavation will be required for flood and sediment pool storage, of which a portion will be covered with a clay blanket. A box culvert principal outlet and an earthen auxiliary spillway will be included in the design.	\$1,500,000

Table 6-1. Stormwater Projects (Continued)

Study Area	Project No.	Issue to be addressed	Description of Improvements	Total Cost
Socorro	SOC5	Crossing capacity at Carr Road and Mesa Spur Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 48-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$200,000
Socorro	SOC6	Crossing capacity at Coker Road and Mesa Spur Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 48-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$170,000
Socorro	SOC7	Crossing capacity at Anderson Road and Mesa Spur Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 48-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$190,000
Socorro	SOC8	Crossing capacity at Carr Road and Mesa Spur Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 60-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$260,000
Hacienda Real	HAC1	Downstream flooding and sediment load due to uncontrolled flows from Stream 6. No low-level outlet in existing flood retention pond.	This project involves expanding two existing retention basins at the end of Stream 6. Although the existing basins are providing some benefit in its current state, they are not sized and cannot be expanded to such a size that will handle the 100-year flood flows from Stream 6. The proposed improvements include expanding Basin A from 760'x200' to bottom dimensions of 760'x300' with 3:1 side slopes, and expanding Basin B from 260'x100' to bottom dimensions of 260'x200' with 3:1 side slopes.	\$1,080,000
Hacienda Real	HAC2	Downstream flooding and sediment load due to uncontrolled flows from Stream 7.	This project involves constructing two detention basins along Stream 7. The proposed Basin B requires approximately 115 acre-feet of excavation for flood and sediment pool storage. The proposed Basin A requires approximately 880 acre-feet of excavation for flood and sediment pool storage.	\$37,810,000
Hacienda Real	HAC3	Downstream flooding and sediment load due to uncontrolled flows from Stream 8.	This project involves constructing a combination sediment/retention basin at the base of Stream 8. The basin embankment will be 6 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Approximately 64 acre-feet of excavation will be required for flood and sediment pool storage.	\$2,710,000
Hacienda Real	HAC4	Downstream flooding and sediment load due to uncontrolled flows from Streams 9 and 10.	This project involves constructing a combination sediment/retention basin at the base of Streams 9 and 10. The basin embankment will be 6 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Approximately 36 acre-feet of excavation will be required for flood and sediment pool storage.	\$1,890,000
Hacienda Real	HAC5	Downstream flooding and sediment load due to uncontrolled flows from Stream 11.	This project involves constructing a combination sediment/retention basin at the base of Stream 11. The basin embankment will be 6 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Approximately 61 acre-feet of excavation will be required for flood and sediment pool storage.	\$2,920,000
Hacienda Real	HAC6	Downstream flooding and sediment load due to uncontrolled flows from Streams 12 and 13.	This project involves constructing a combination sediment/retention basin at the base of Streams 12 and 13. The basin embankment will be 6 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Approximately 127 acre-feet of excavation will be required for flood and sediment pool storage.	\$4,470,000

Table 6-1. Stormwater Projects (Continued)

Study	Project			T
Area Hacienda Real	No. HAC7	Downstream flooding and sediment load due to uncontrolled flows from Stream 13.5.	Description of Improvements This project involves constructing two basins along Stream 13.5. The proposed upper retention basin (Basin B) controls flows from the upper end of the watershed. The proposed Basin B requires approximately 295 acre-feet of excavation for flood and sediment pool storage. The proposed lower basin (Basin A) controls the flows accumulating within the watershed below the upper basin. The proposed embankment for Basin A is approximately 6 feet tall and requires approximately 4 acrefeet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of two 4-foot by 4-foot CBCs.	**Total Cost
Hacienda Real	HAC8	Crossing capacity at Bridgeway Drive and Stream 7 is less than 100- year flood and has a history of sediment and washout issues.	This project involves removing the existing five 48-inch CMP culverts and replacing it with five 4-foot by 4-foot CBCs. This culvert size provides sufficient capacity provided that additional storage is provided upstream per HAC2.	\$570,000
Hacienda Real	HAC9	Crossing capacity at Northloop Drive and Mesa Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 60-inch RCP culvert and replacing it with three 4-foot by 4-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$150,000
Hacienda Real	HAC10	Crossing capacity at FM 1110 and Mesa Drain is less than capacity of channel immediately upstream of crossing. Crossing is silted in and collapsed.	This project involves removing the existing 42-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity slightly lower than that of channel immediately upstream, but provides maximum opening allowable for crossing and channel geometry.	\$620,000
Hacienda Real	HAC11	Crossing capacity at Salatral Lateral and Mesa Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 36-inch RCP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$590,000
Hacienda Real	HAC12	Crossing capacity at Fenter Road and Mesa Drain is less than capacity/crossing size of upstream improved crossings.	This project involves removing the existing 72-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$650,000
Hacienda Real	HAC13	Crossing capacity at dirt crossing upstream of Celum Road and Mesa Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 54-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity slightly lower than that of channel immediately upstream, but provides maximum opening allowable for crossing and channel geometry.	\$270,000
Hacienda Real	HAC14	Crossing capacity at Celum Road and Mesa Drain is less than capacity of channel immediately upstream of crossing.	This project involves removing the existing 36-inch CMP culvert and replacing it with two 7-foot by 7-foot CBCs. This culvert size provides capacity equal to or greater than that of the upstream channel.	\$300,000
Fabens	FAB1	Downstream flooding and sediment load due to uncontrolled flows from Fabens North 1.	This project involves constructing a combination sediment/retention basin at the base of Fabens North 1. The basin embankment will be 15 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 5 feet of freeboard for PMP event. Approximately 27 acre-feet of excavation will be required for flood and sediment pool storage, of which a portion will be covered with a clay blanket. A box culvert principal outlet and an earthen auxiliary spillway will be included in the design.	\$3,310,000

Table 6-1. Stormwater Projects (Continued)

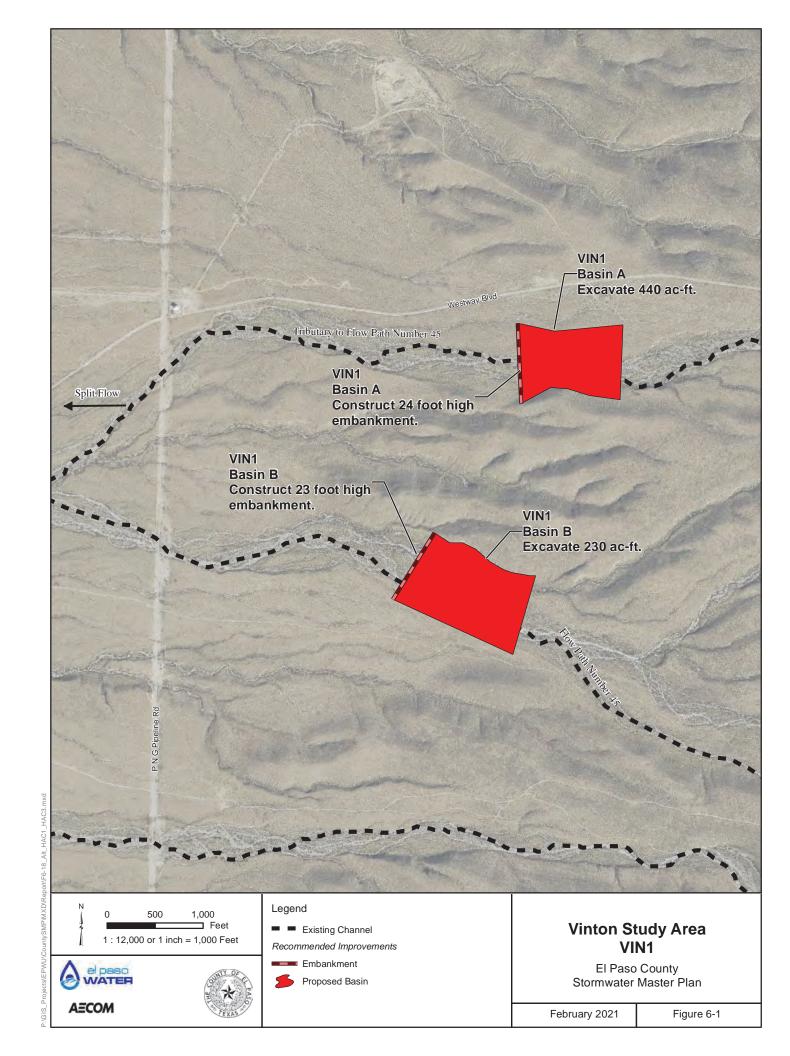
Study	Project			
Area	No.	Issue to be addressed	Description of Improvements	Total Cost
Fabens	FAB2	Lack of ROW acquisition along San Felipe Arroyo to maintain channel capacity.	This project involves obtaining property along San Felipe Arroyo to maintain channel capacity.	\$590,000
Fabens	FAB3	Dam will not pass 75% PMP.	This project involves constructing 1,165 feet of 4-foot-high parapet wall along the crest of Fabens Dam. In addition, the east auxiliary spillway will be widened 100 feet to a total width of 150 feet.	\$1,750,000
Tornillo	TOR1	Downstream flooding and sediment load due to uncontrolled flows from High School Channel and South High School Channel.	This project involves constructing a combination sediment/retention basin at the base of the confluence of High School Channel and South High School Channel (Basin B) and a sediment basin in the upper watershed (Basin A). Basin B will be 6 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Approximately 49 acre-feet of excavation will be required for flood and sediment pool storage, of which a portion will be covered with a clay blanket. A box culvert principal outlet and an earthen auxiliary spillway will be included in the design. Basin A will be for sediment pool storage only, no embankment required. Approximately 4 acre-feet of excavation will be required for sediment pool storage.	\$3,120,000
Tornillo	TOR2	Erosion of West Bank along the redirected portion of High School Channel.	This project involves riprap reinforcement along the west bank of High School Channel.	\$1,040,000
Tornillo	TOR3	Downstream flooding and sediment load due to uncontrolled flows from Flow Path T.	This project involves the utilization of the construction of the combination sediment/retention basin (TOR1, Basin B) addressing issues for TOR1 and the construction of a sediment basin in the upper watershed (TOR3). TOR1, Basin B must be constructed in order for this project to address the flooding issue associated with Flow Path T. The sediment basin TOR3 will be for sediment pool storage only, no embankment required. Approximately 2 acre-feet of excavation will be required for sediment pool storage.	\$60,000
Tornillo	TOR4	Downstream flooding and sediment load due to uncontrolled flows from Tornillo Handle Channel 1 and Tornillo Handle Channel 2.	This project involves constructing a combination sediment/retention basin at the confluence of Tornillo Handle Channel 1 with Tornillo Handle Channel 2. The basin embankment will be 10 feet high and will have a clay core, a polyurethane liner, a chimney drain, and will have 18-inch riprap on the interior face. Embankment height includes 5 feet of freeboard for PMP event. Approximately 7 acre-feet of excavation will be required for flood and sediment pool storage, of which a portion will be covered with a clay blanket. A box culvert principal outlet and an earthen auxiliary spillway will be included in the design.	\$1,750,000
Tornillo	TOR5	Downstream flooding due to uncontrolled flows from Tornillo Handle Channel 1.	This project involves riprap reinforcement along the south bank of Tornillo Handle Channel 1.	\$280,000
Tornillo	TOR6	Crossing capacity at OT Smith Road and Tornillo Handle Channel 2 is less than the necessary capacity.	This project involves removing the existing two 36-inch by 19-inch arch culvert and replacing it with two 4-foot by 2-foot CBCs. This culvert size provides sufficient capacity equal to that of the upstream channel.	\$70,000

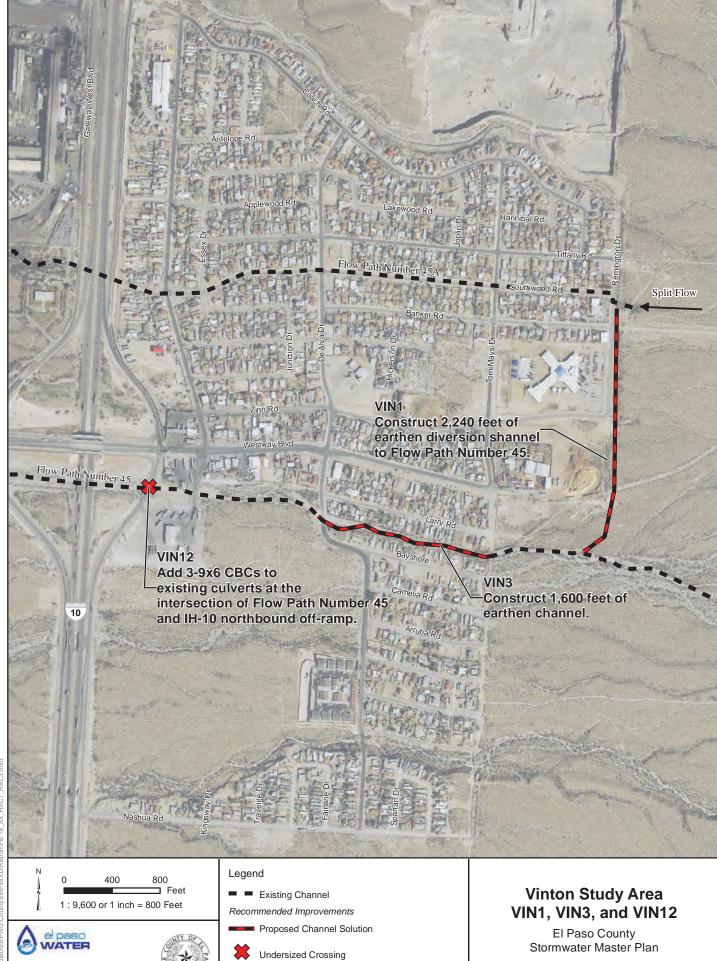
Table 6-1. Stormwater Projects (Continued)

Study	Project			
Area	No.	Issue to be addressed	Description of Improvements	Total Cost
Montana Sector	MON1	Flooding due to uncontrolled flows originating in the Fort Bliss Military Reservation.	This project involves constructing a retention basin on land that is currently part of the Fort Bliss Military Reservation. The proposed basin requires approximately 750 acre-feet of excavation for flood and sediment pool storage.	\$15,780,000
Montana Sector	MON2	Flooding due to uncontrolled flows originating in the slopes above Tributary 1 to Flowpath M-4	This project involves constructing a retention basin at the base of Tributary 1 to Flowpath M-4. The proposed basin requires approximately 378 acre-feet of excavation for flood and sediment pool storage.	\$8,030,000
Montana Sector	MON3	Flooding due to uncontrolled flows originating in the slopes above Flowpaths M-2, M- 3, and M-5	This project involves constructing a detention basin on Flowpath M-3. The proposed basin controls flows from the upper end of the watershed and contains two embankments. The proposed embankments for the basin are approximately 25 feet tall and 27 feet tall, and require approximately 4 acre-feet of excavation for flood and sediment pool storage. The outlet structure for the basin consists of two 4-foot by 4-foot CBCs.	\$25,800,000
Montana Sector	MON4	Crossing capacity at Flowpath M-4 and Tamara Road is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-4 and Tamara Road with seven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$320,000
Montana Sector	MON5	Crossing capacity at Flowpath M-4 and Oleary Drive is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-4 and Oleary Drive with seven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$320,000
Montana Sector	MON6	Crossing capacity at Flowpath M-4 and Paso View Drive is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-4 and Paso View Drive with seven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$320,000
Montana Sector	MON7	Crossing capacity at Flowpath M-2 and Stagecoach Drive is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-2 and Stagecoach Drive with four 7-foot by 4-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$450,000
Montana Sector	MON8	Crossing capacity at Flowpath M-2 and Indian Trail Road is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Tributary to Flowpath M-2 and Indian Trail Road with seven 8-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$210,000
Montana Sector	MON9	Crossing capacity at Flowpath M-2 and Hueco Tanks Road is less than the necessary capacity.	This project involves replacing the existing 2 – 24" corrugate metal pipe culverts at the intersection of Flowpath M-2 and Hueco Tanks Road with six 7-foot by 4-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$610,000
Montana Sector	MON10	Crossing capacity at Flowpath M-3 and Hueco Mountain Road is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-3 and Hueco Mountain Road with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$1,020,000
Montana Sector	MON11	Crossing capacity at Flowpath M-3 and Overland Stage Road is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-3 and Hueco Mountain Road with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$1,020,000

Table 6-1. Stormwater Projects (Continued)

Study Area	Project No.	Issue to be addressed	Description of Improvements	Total Cost
Montana Sector	MON12	Crossing capacity at Flowpath M-3 and Woodrow Road is less than the necessary capacity.	This project involves replacing the existing 5 concrete box culverts at the intersection of Flowpath M-3 and Woodrow Drive with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$1,020,000
Montana Sector	MON13	Crossing capacity at Flowpath M-3 and Hueco Tanks Road is less than the necessary capacity.	This project involves replacing the existing 3 - 24" corrugated metal pipe culverts at the intersection of Flowpath M-3 and Hueco Tanks Road with eleven 9-foot by 5-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$1,390,000
Montana Sector	MON14	Crossing capacity at Flowpath M-6 and Millicent Avenue is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-6 and Millicent Avenue with fourteen 12-foot by 9-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$1,470,000
Montana Sector	MON15	Crossing capacity at Flowpath M-6 and Petty Prue Street is less than the necessary capacity.	This project involves replacing the existing at grade crossing at the intersection of Flowpath M-6 and Petty Prue Street with fourteen 12-foot by 9-foot CBCs. This culvert size will provide sufficient capacity for the 100-year flood to be conveyed through the crossing.	\$1,470,000

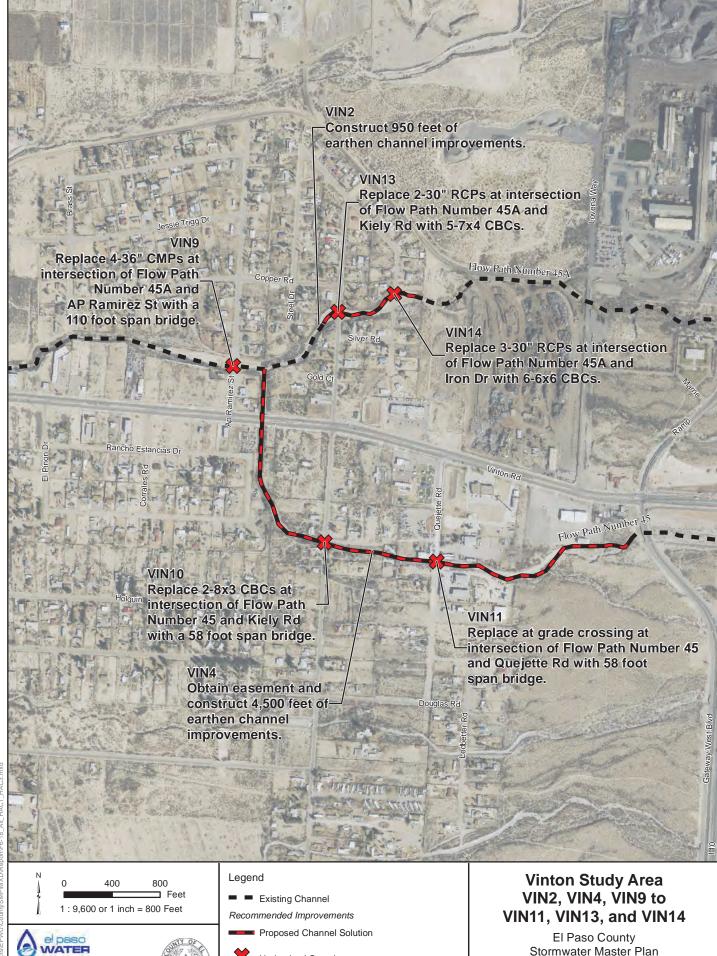




February 2021

Figure 6-2

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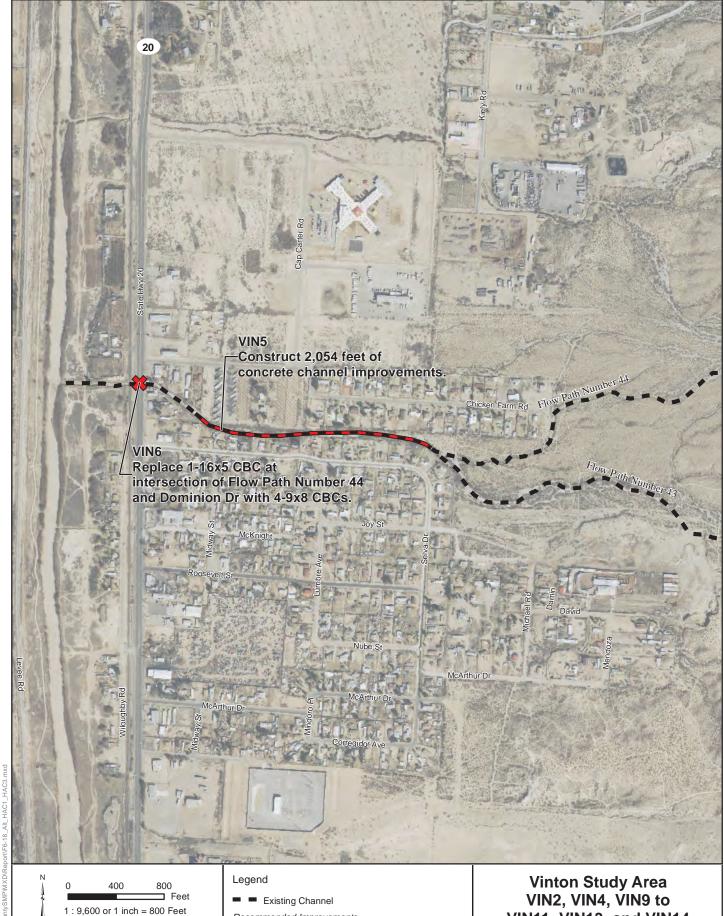
Undersized Crossing

Stormwater Master Plan

Figure 6-3

February 2021

AECOM



AECOM

el paso WATER



Recommended Improvements

Proposed Channel Solution

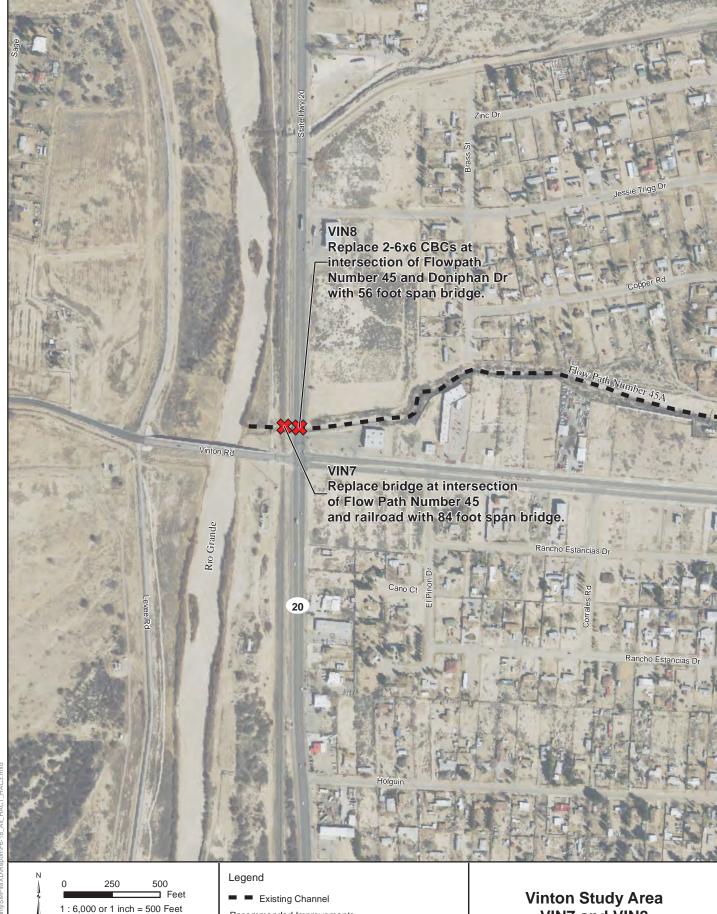


VIN11, VIN13, and VIN14

El Paso County Stormwater Master Plan

February 2021

Figure 6-4



el paso WATER **AECOM**



Recommended Improvements



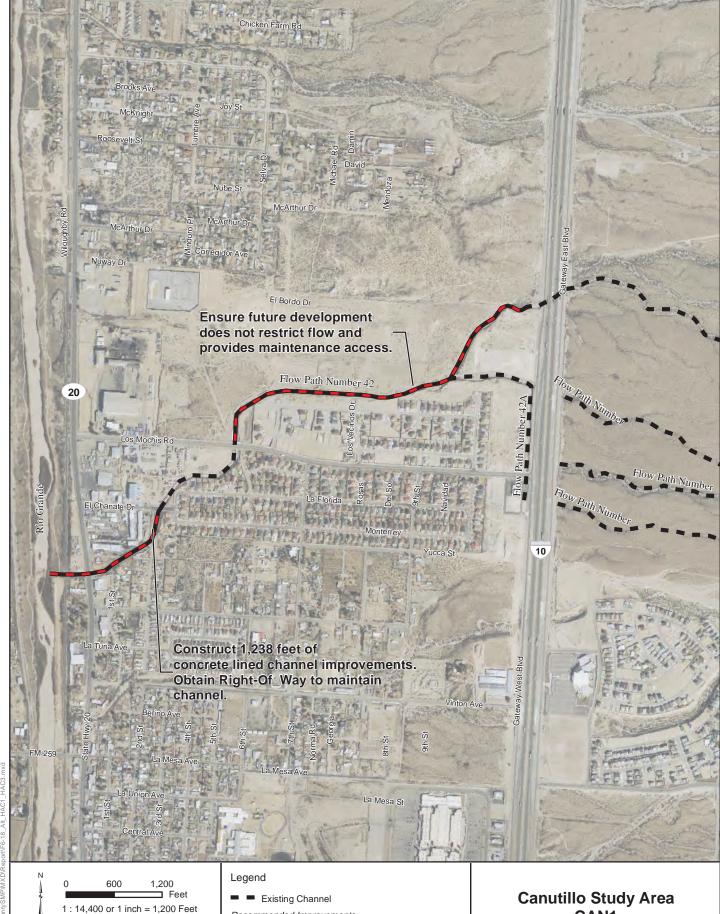
Undersized Crossing

VIN7 and VIN8

El Paso County Stormwater Master Plan

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Figure 6-5



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Recommended Improvements

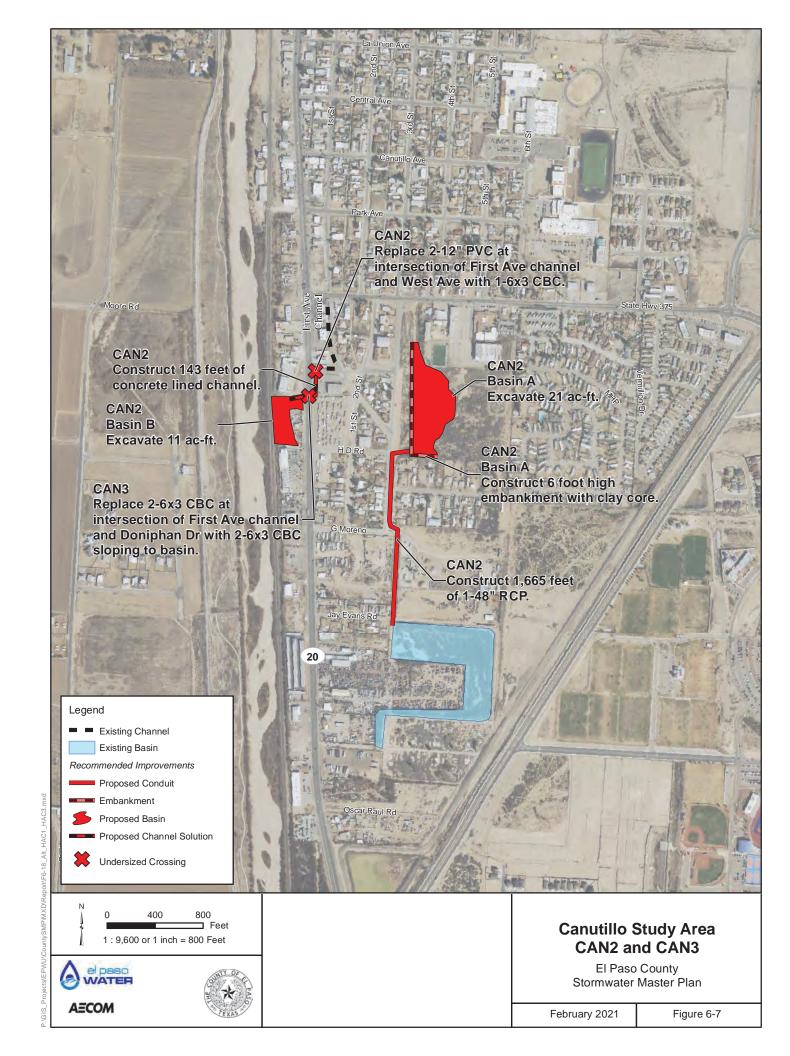
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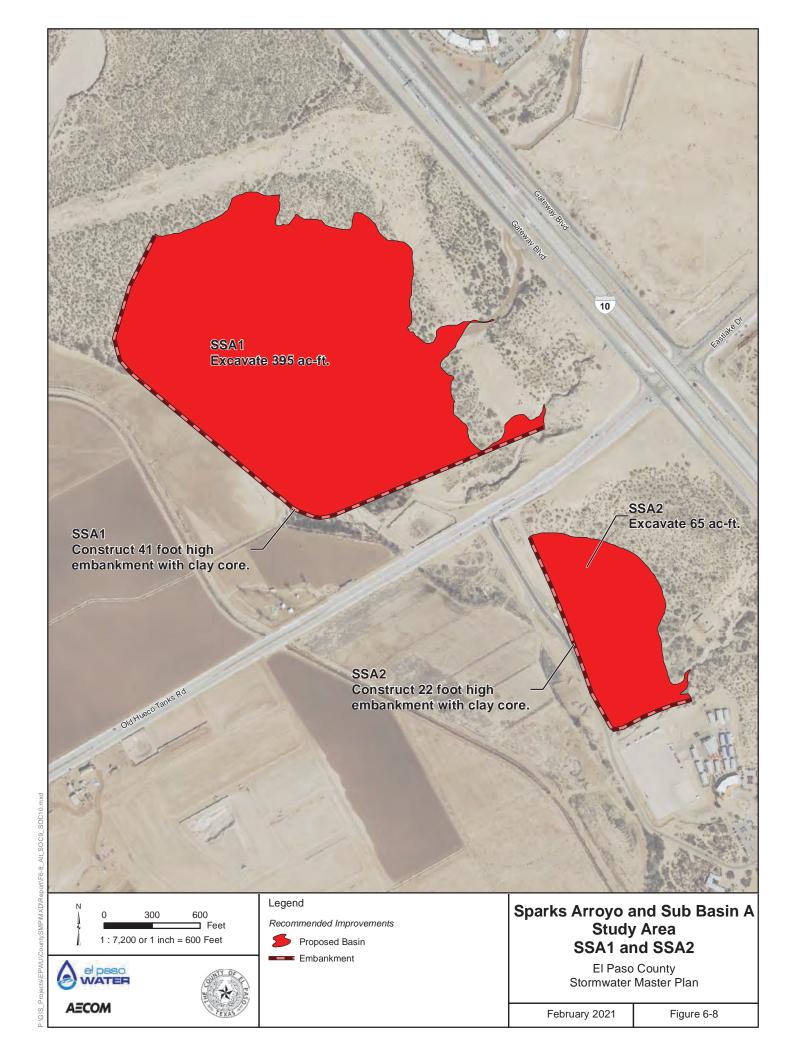
CAN1

El Paso County Stormwater Master Plan

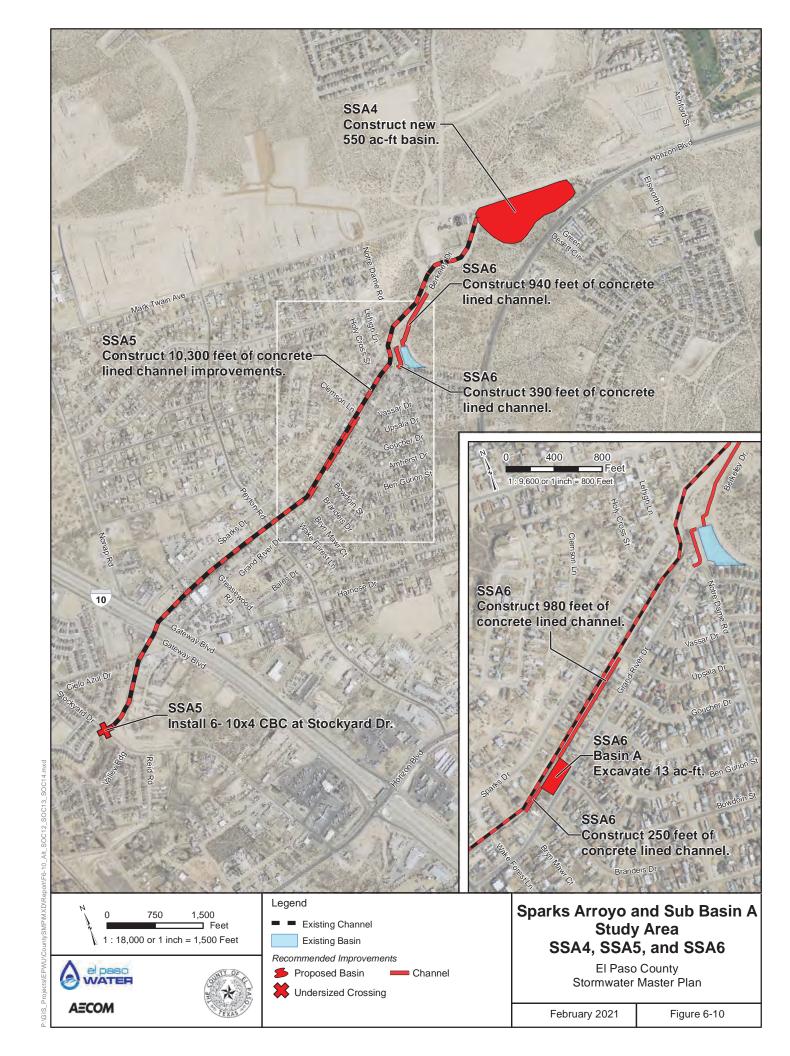
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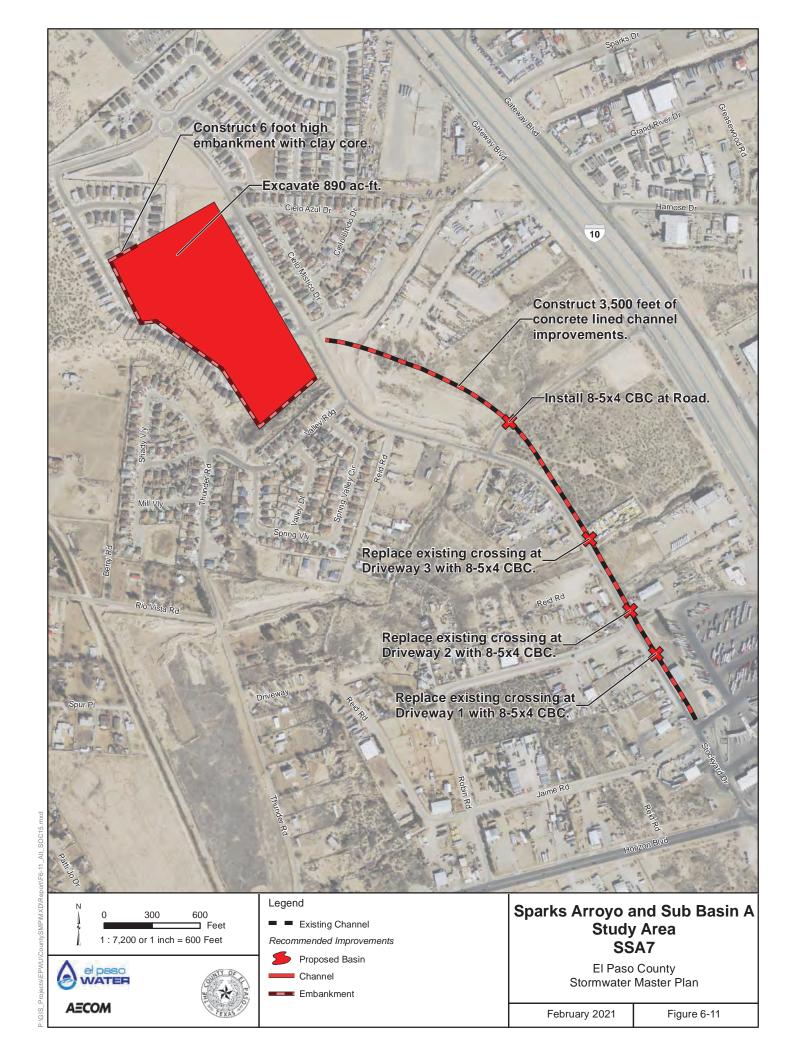
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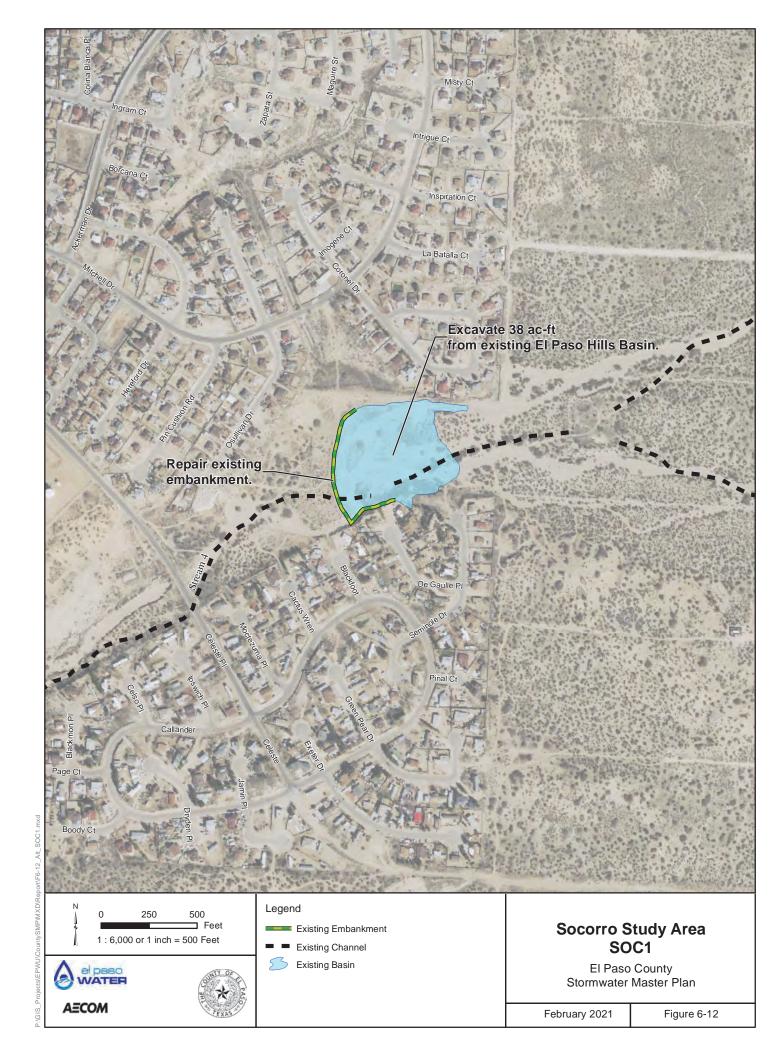


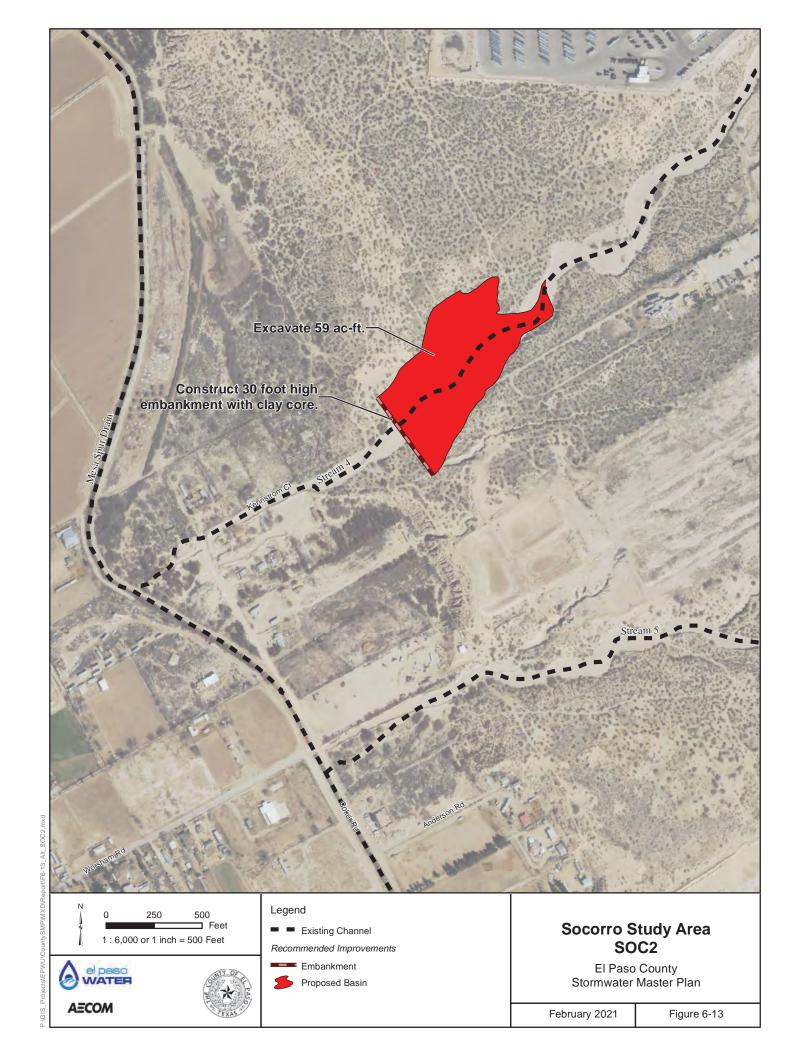


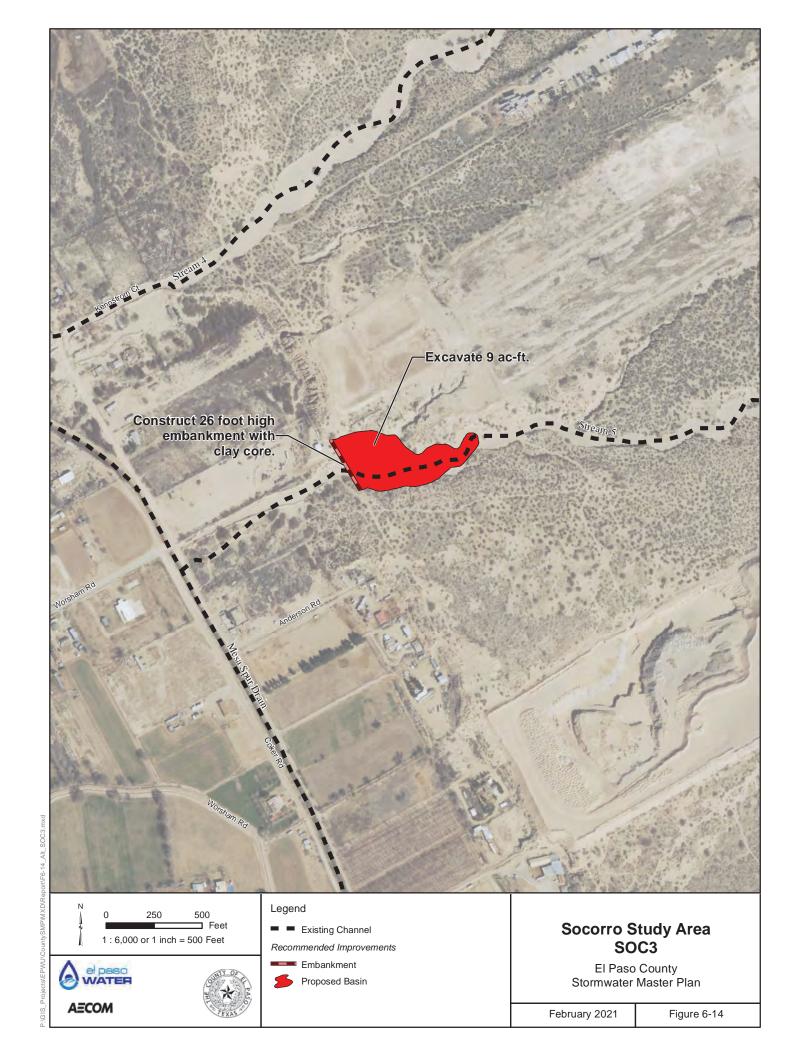


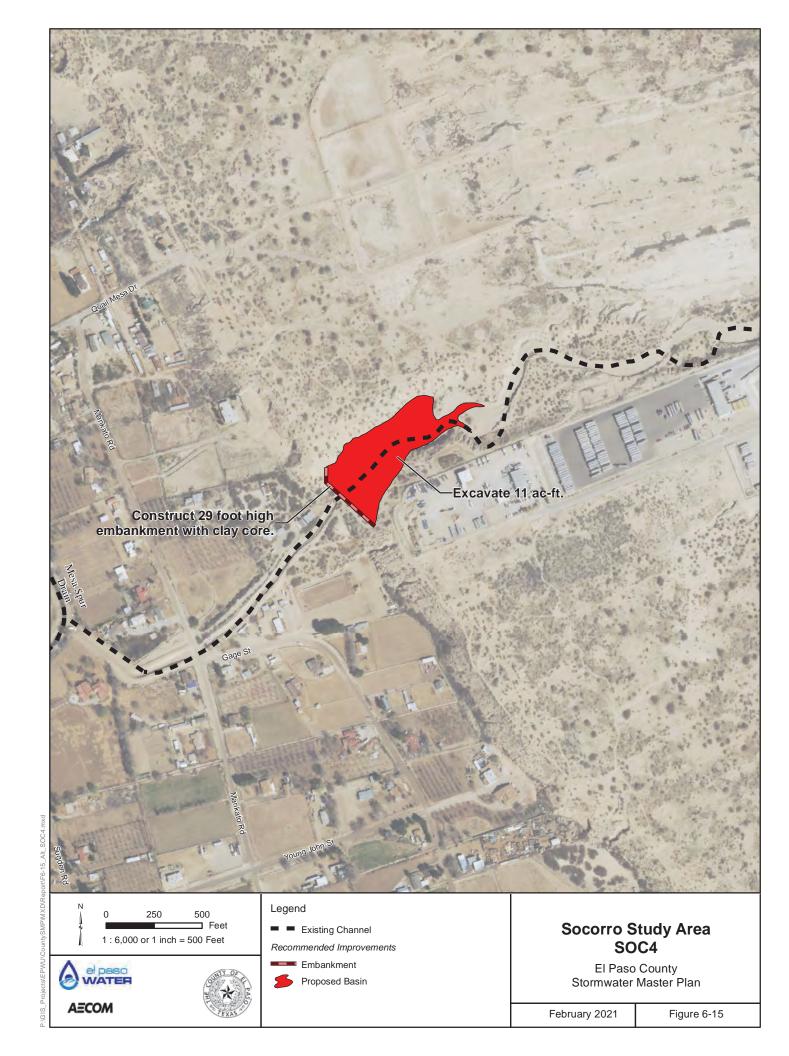


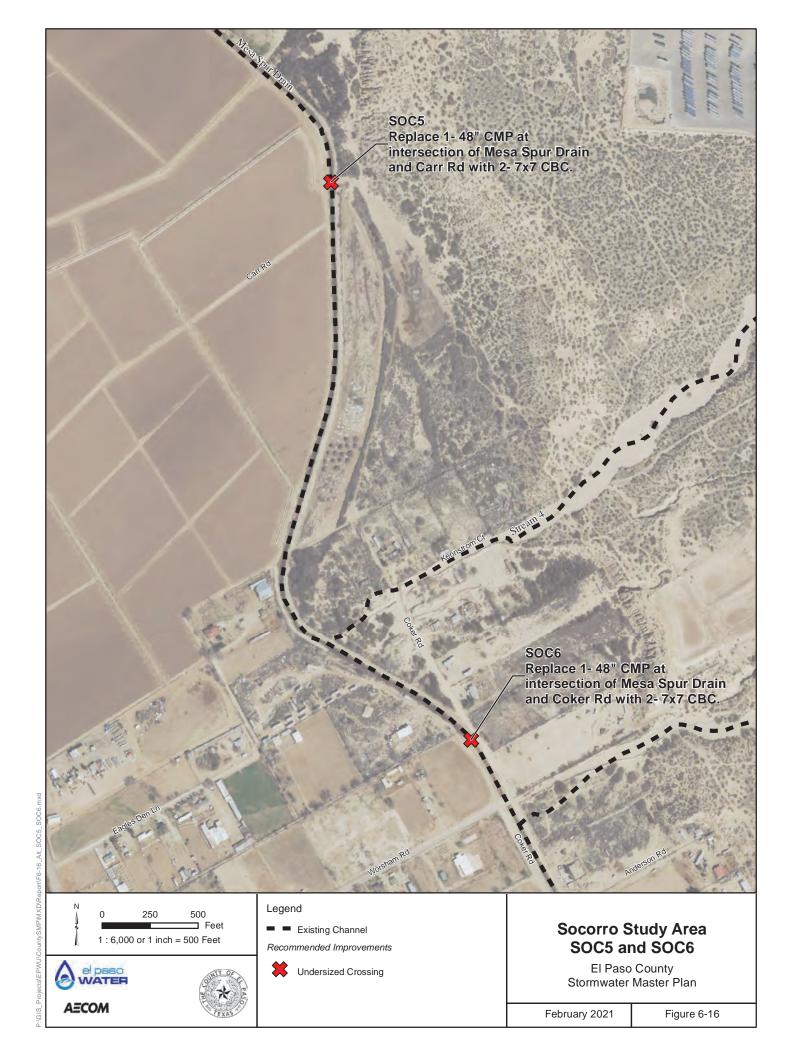


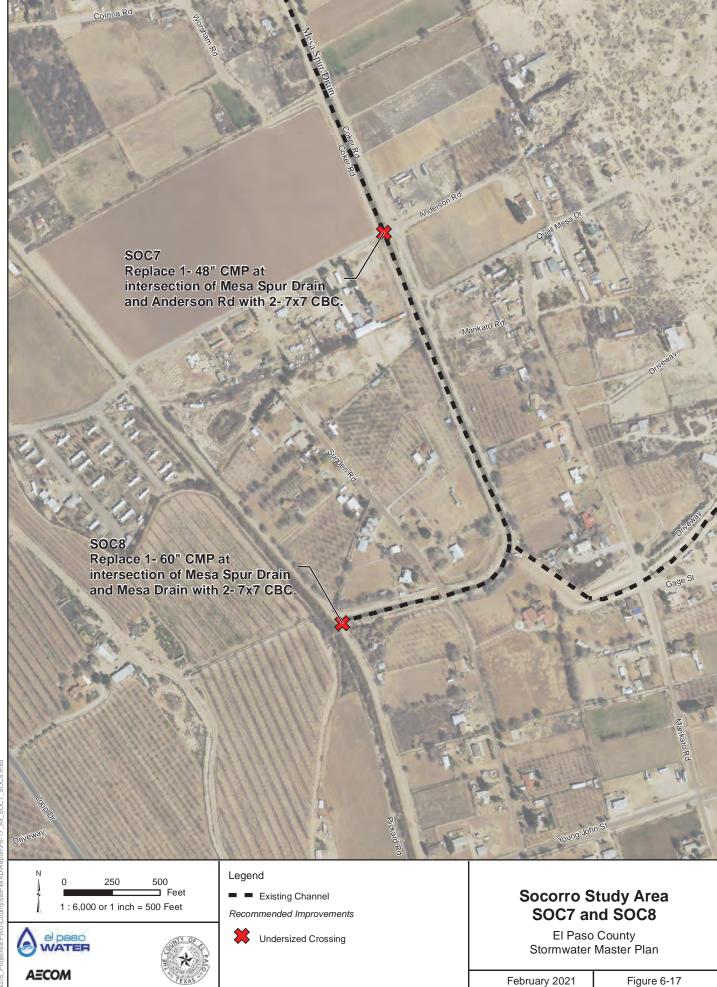




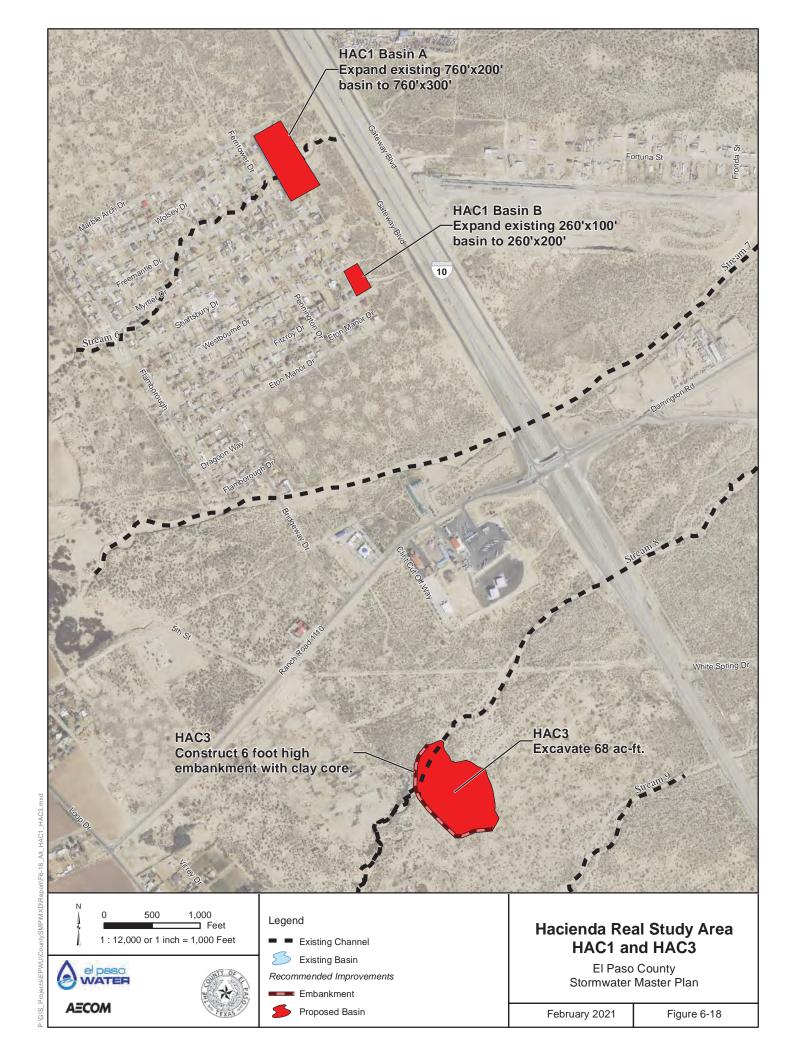


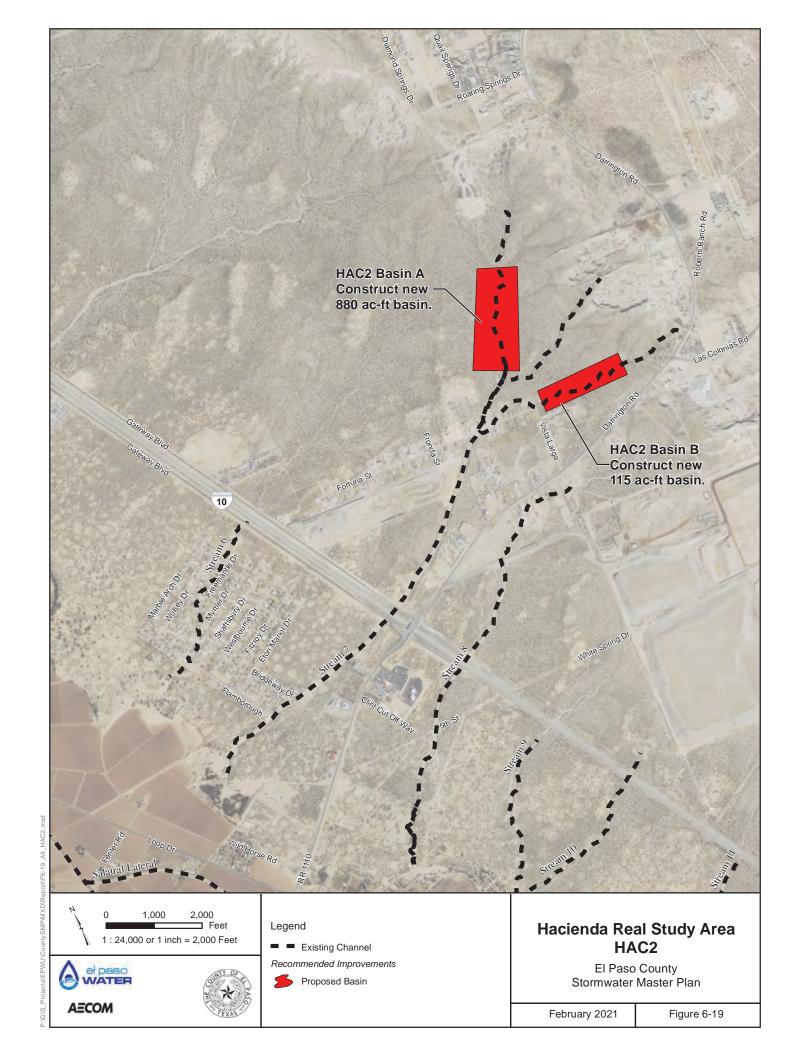


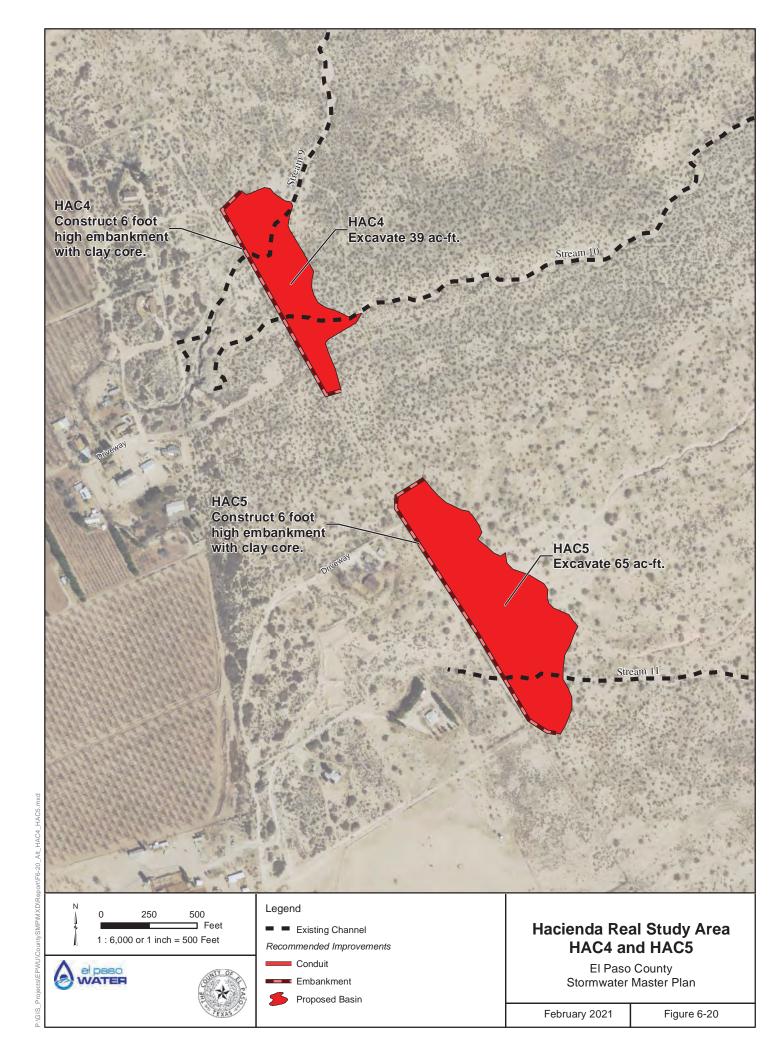


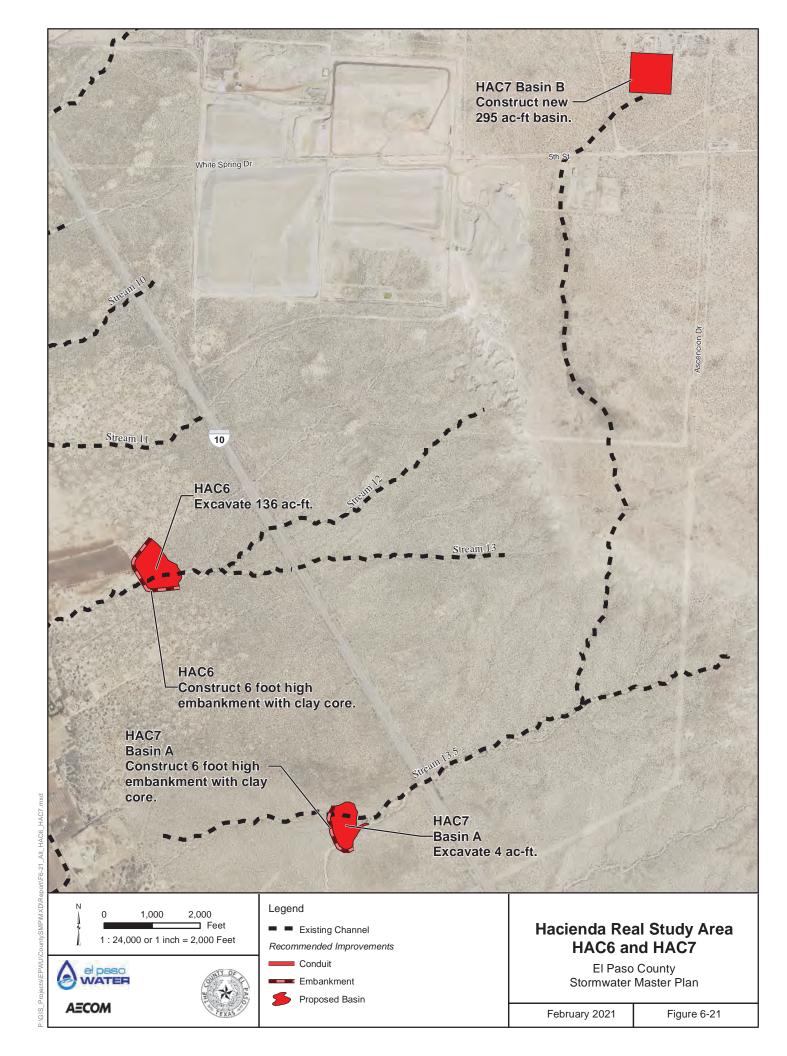


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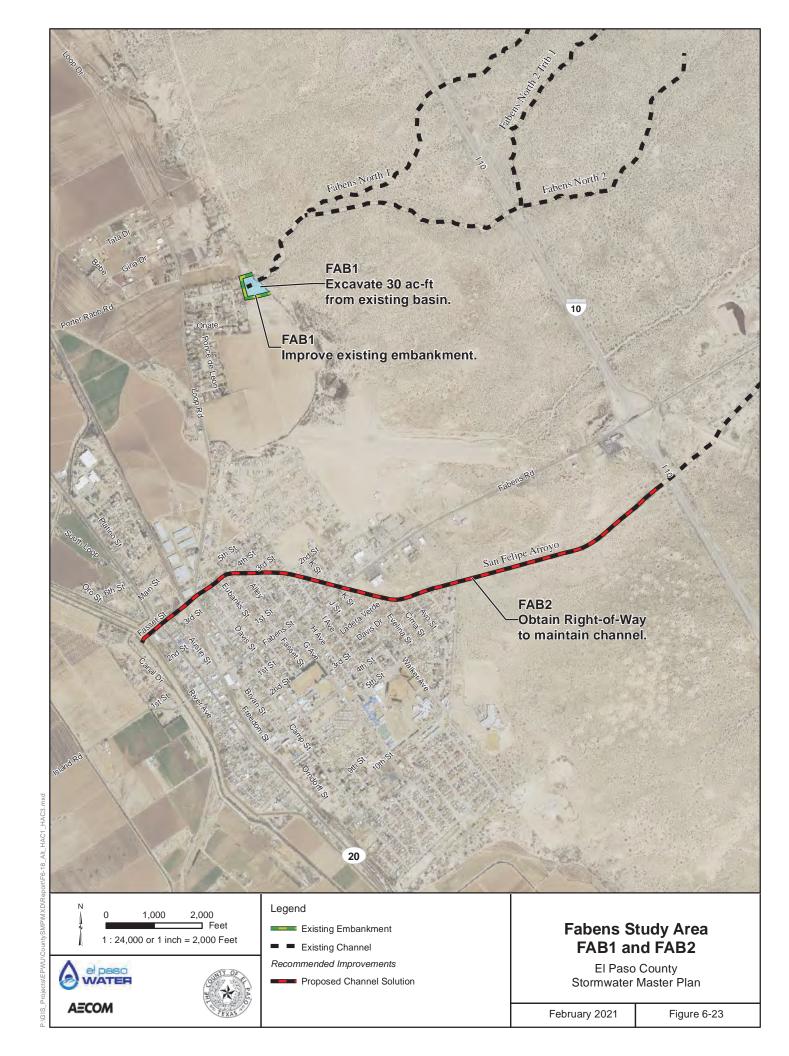


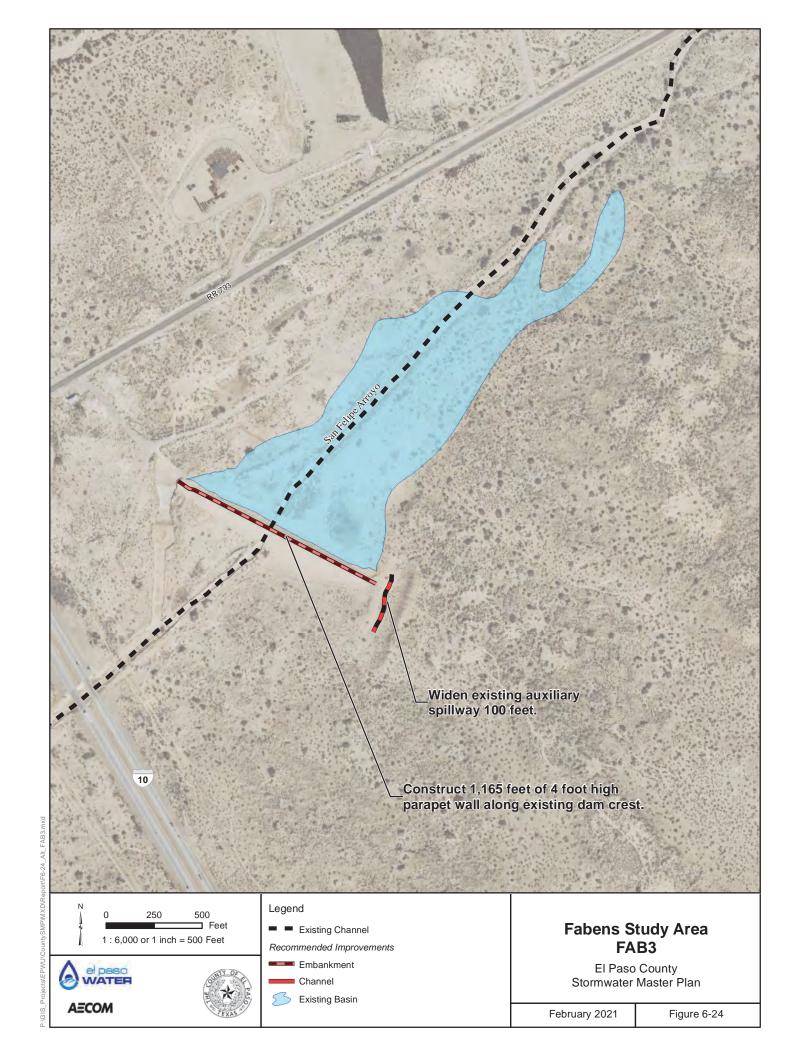


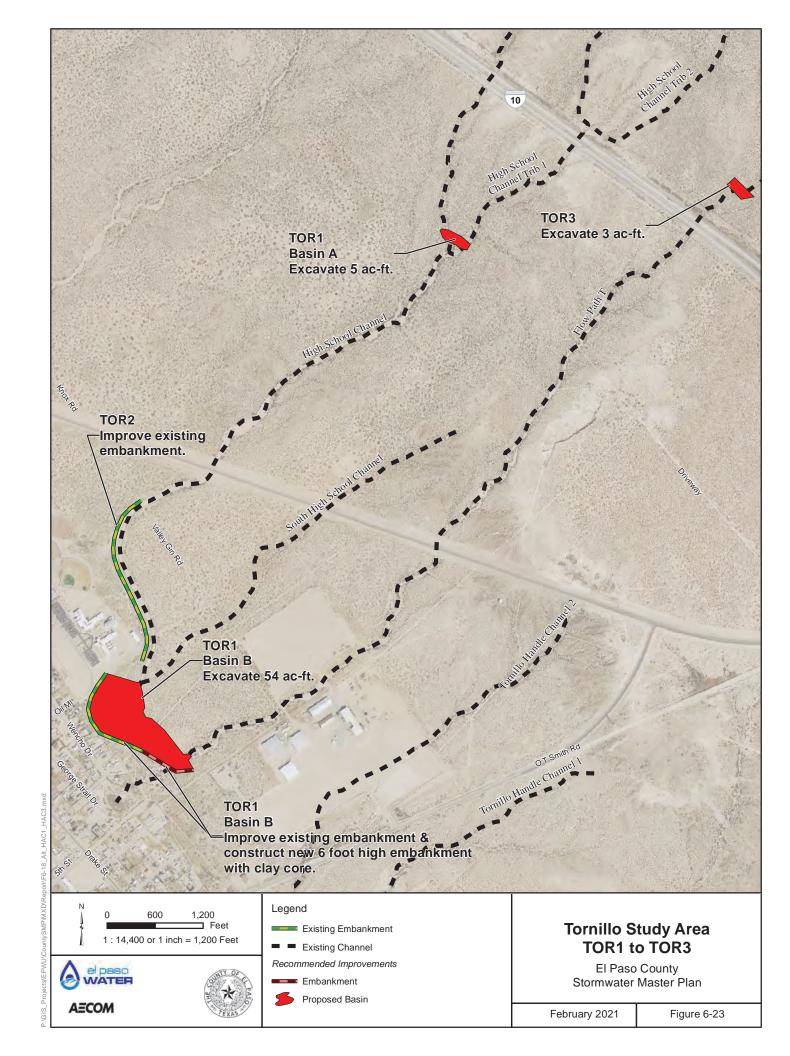


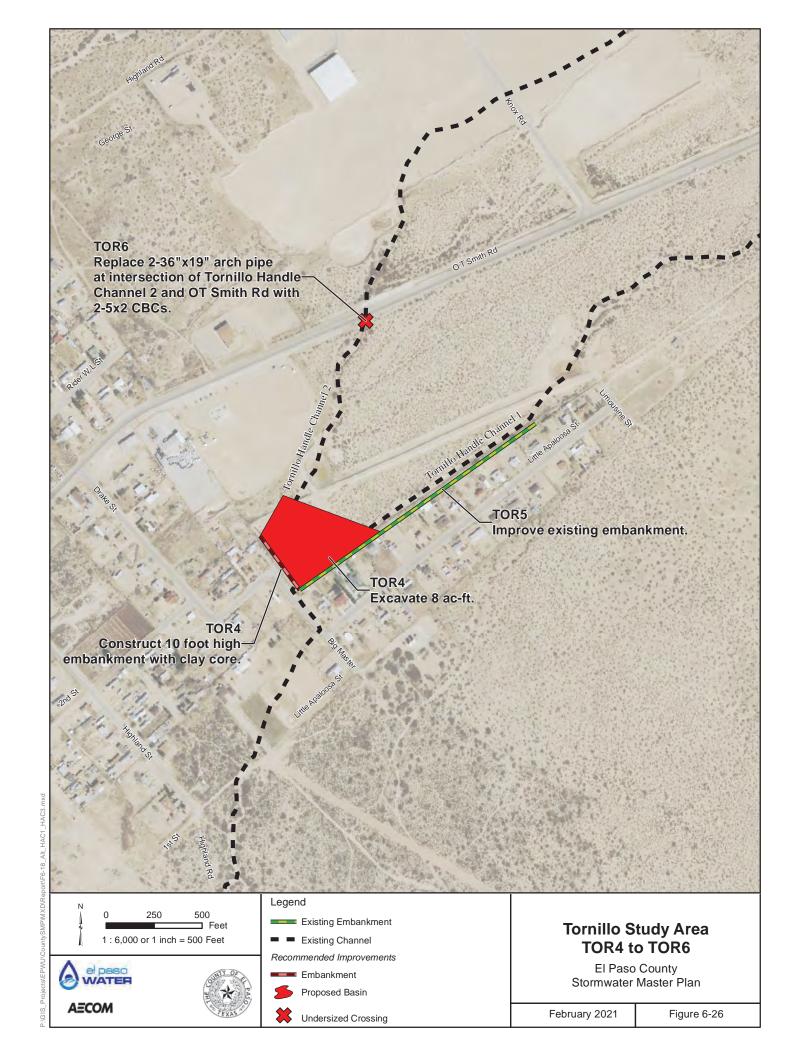




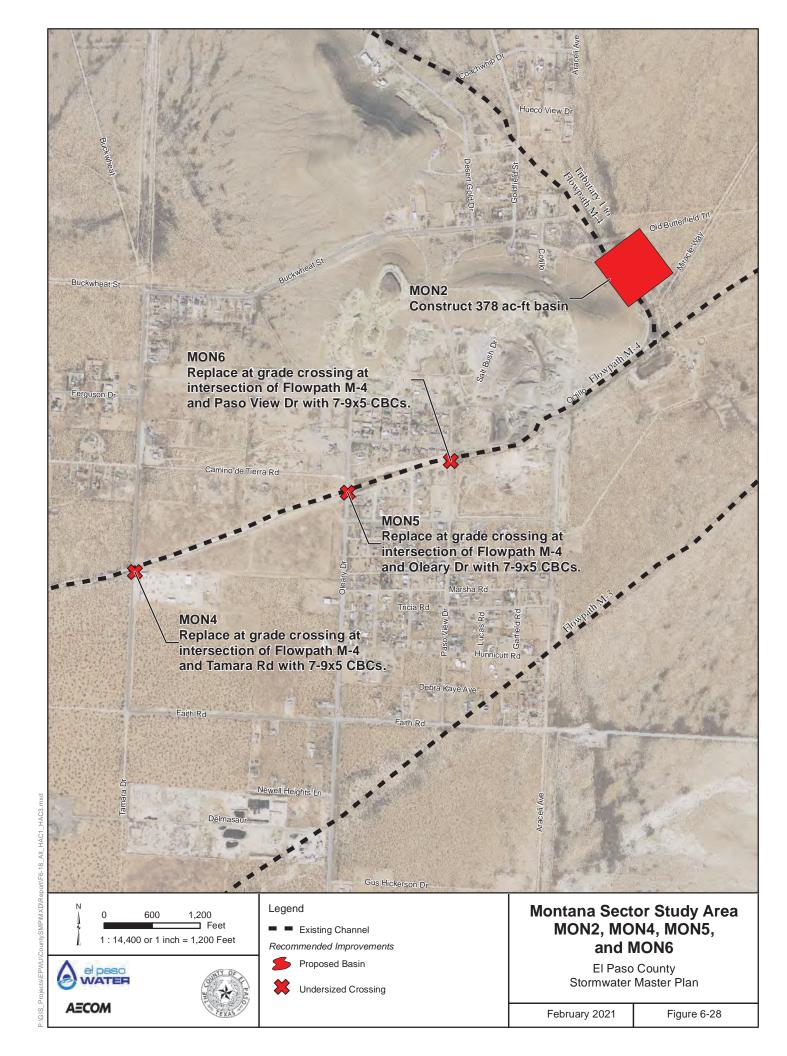


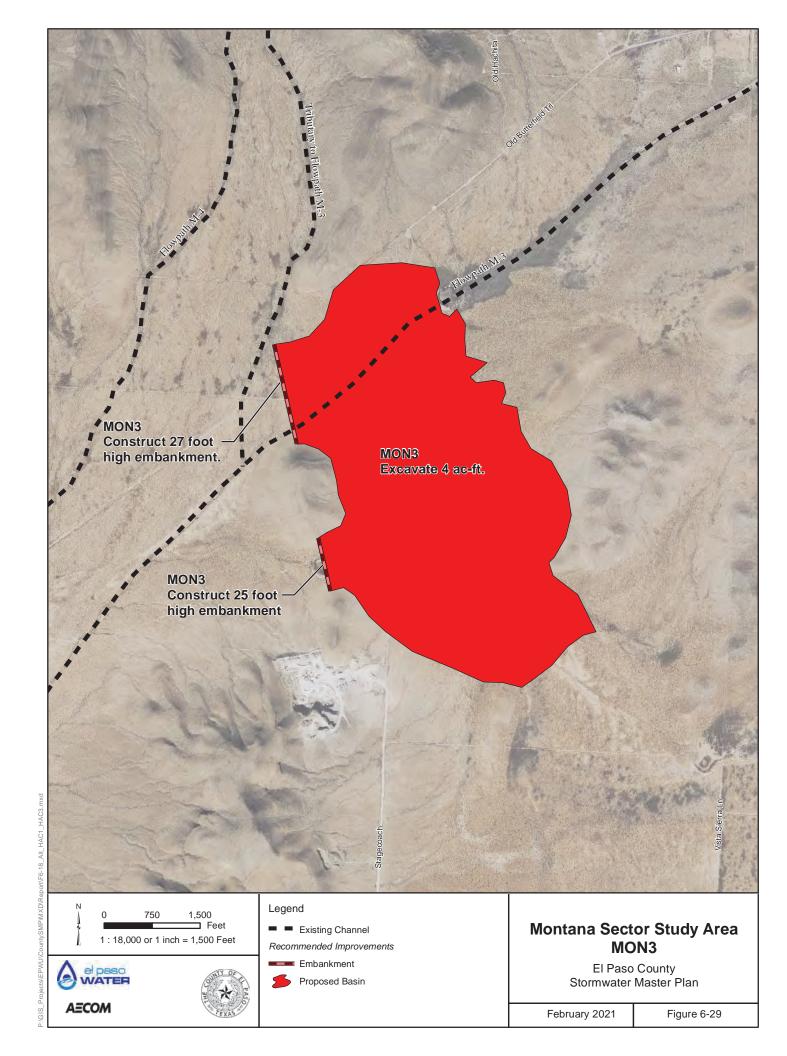


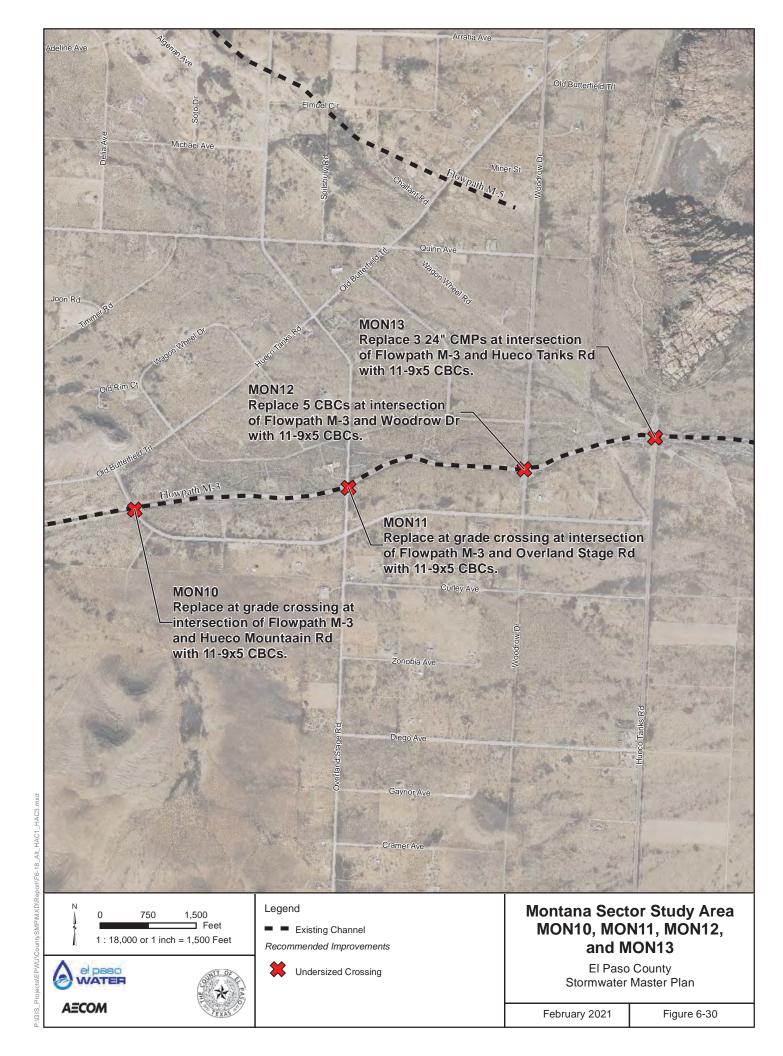


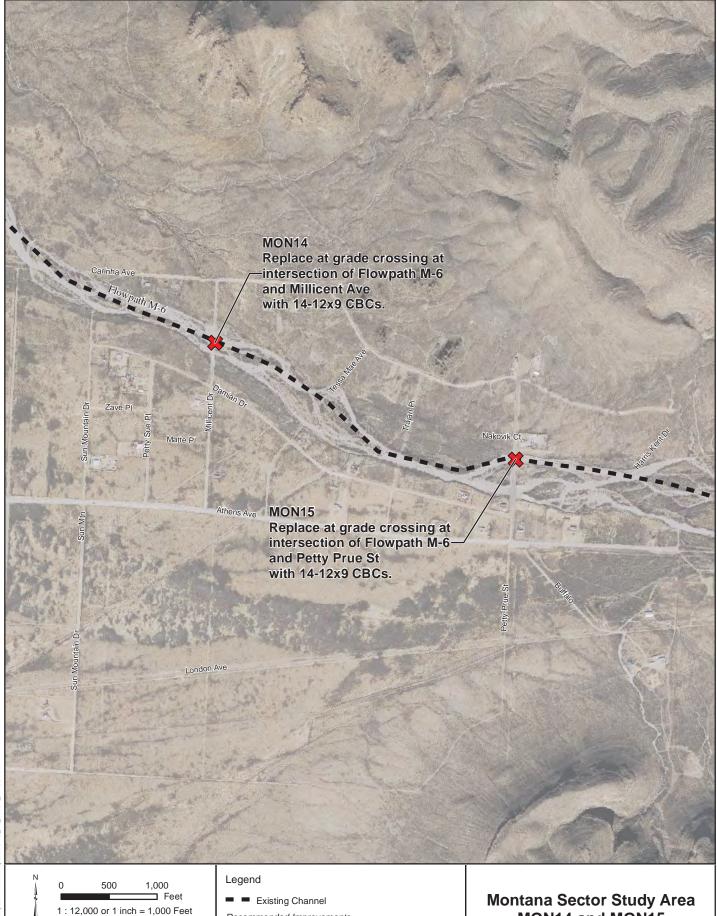












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Recommended Improvements



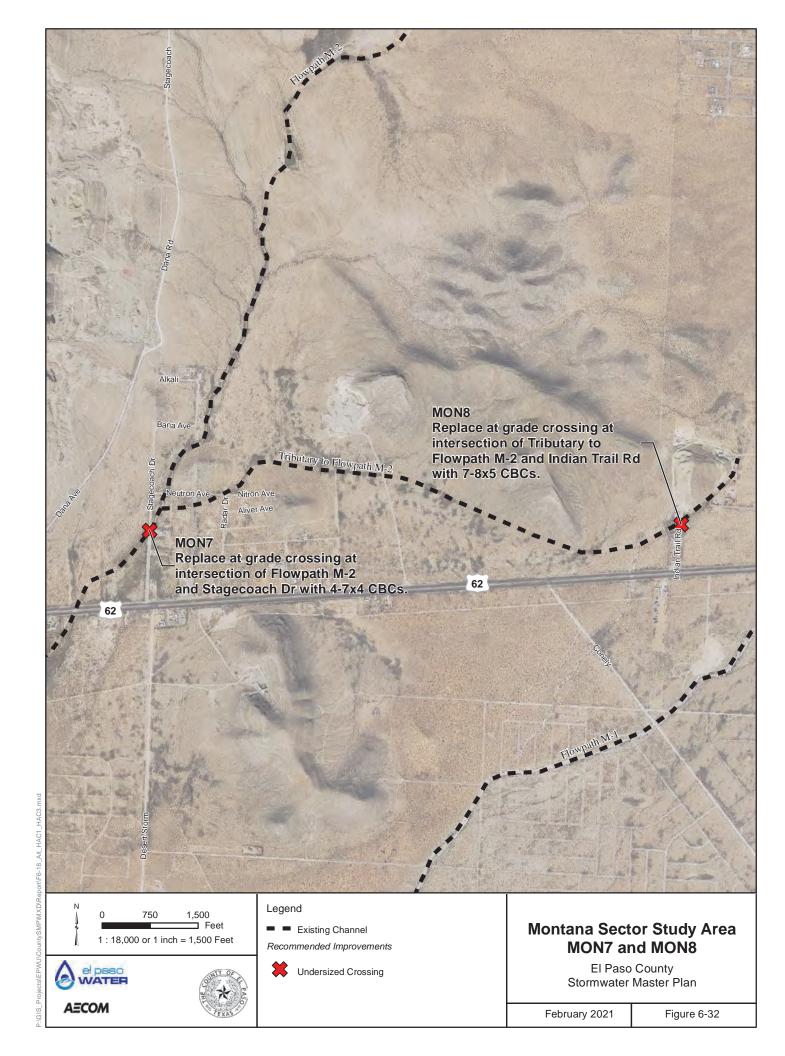
Undersized Crossing

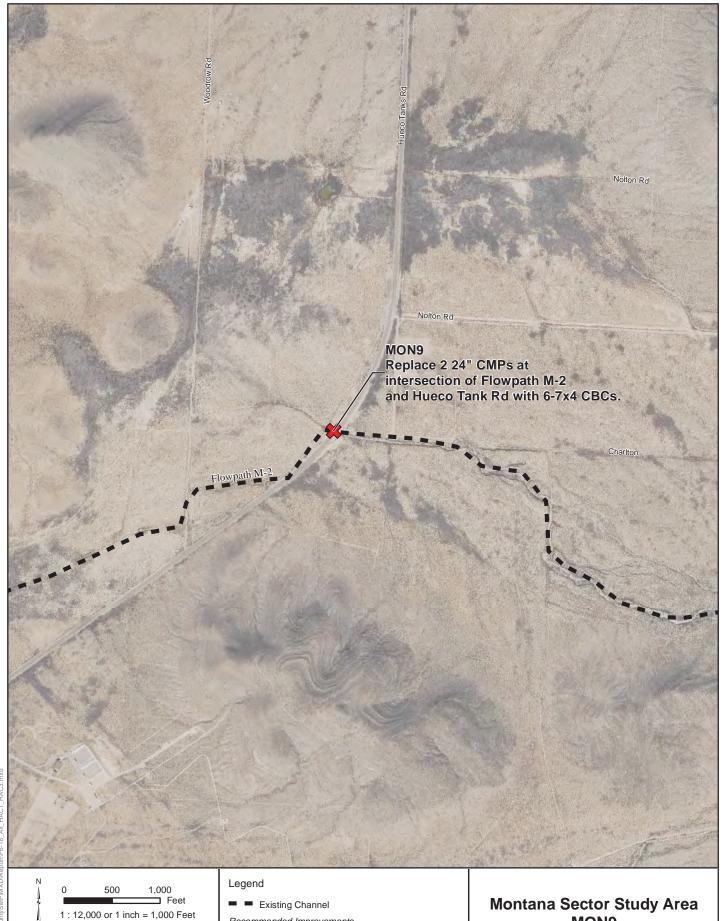
MON14 and MON15

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Figure 6-31





AECOM



Recommended Improvements



Undersized Crossing

MON9

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Figure 6-33

7.0 PRIORITIZATION OF SELECTED PROJECTS

All of the projects discussed in this SMP provide protection from flooding for some group of affected individuals and property. The natural tendency is for everyone to think that their project is the most important and should be constructed first. The reality is that there are limited funds available and that not all the projects can be funded initially. Therefore, an effort was made to rank the projects to provide the County and affected communities a rationale for deciding the relative priority for funding the individual projects.

The first task of the prioritization process was to identify the major concerns associated with stormwater management. The major concerns identified to be addressed by the proposed stormwater improvements were:

- Reduce flooding of real property (residences, commercial/industrial and agricultural land);
- Reduce uncontrolled sediment deposition;
- Reduce flooding of critical transportation arteries (e.g. IH-10, Doniphan Road, etc.);
 and
- Reduce maintenance.

The second task was to develop relative risk index values for each of the above issues for each project. The third task was to use these relative risk index values to assign a priority tier (I, II, and III) to each project. The final task was to rank those projects in within each tier according to benefit-cost ratio.

Representatives from the major stakeholders participated in the prioritization process during Working Meetings 3 and 4 in late April 2010. These meetings included representatives from:

- El Paso County;
- EPW:
- City of Socorro;
- Village of Vinton; and
- TWDB.

Representatives from El Paso County participated in a Working Meeting in December 2020 to discuss updates to the prioritization and prioritization methods.

The results of the prioritization are presented in Table 7-1. Detailed information regarding the estimated project costs and the prioritization process can be found in Appendix C.

The projects listed in Table 7-1 are grouped as follows:

		Number of	
Tier	Priority	Projects	Total Cost
I	High	13	\$169,340,000
II.	Moderate	14	\$55,580,000
III	Less	42	\$33,960,000
Total		69	\$258,880,000

The projects are listed in Table 7-1 within each of the Tiers and Priority groups in order of benefit-cost ration, from high to low. This prioritization is based on the information and assumptions provided in Appendix C. This prioritization process was a subjective, qualitative ranking of the projects and not intended to define the specific order in which projects are funded, but rather to be a tool that can be used to help prioritize projects. Actual prioritization and funding of projects will be determined by the County and affected communities.

Table 7-1. Prioritization Summary

			Type of Improvement		Prioritization		
Project No.	Description	Estimated Total Cost (Rounded to \$10,000)	Basin	Crossing		Tier	Benefit- Cost Ratio (BCR)
HAC7	Sediment/Detention Basin at Location A; Sediment/Retention Basin at Location B	\$3,400,000	х			ı	2.39
SSA1	Detention Basin SSA1	\$34,530,000	Х			I	0.80
SOC1 and SOC 2	Sediment/Detention Basin - SOC1; Sediment/Detention Basin - SOC2	\$4,960,000	х			ı	0.65
SSA4	Detention Basin SSA4	\$7,400,000	X			- 1	0.64
CAN1	Reconstruction of the channel with concrete lining	\$1.960.000			Х	1	0.62
FAB1	Sediment/Retention Basin	\$3,310,000	X			- 1	0.16
CAN2	Retention Basin (CAN2B); 1 - 6' x 3' CBC; 143' Channel Improvements; Retention Basin (CAN2A) - 6-foot embankment; 1,665' principal spillway from CAN2A to existing basin	\$6,030,000	Х			Į	0.14
MON2	Sediment/Detention Basin	\$8,030,000	X				0.09
VIN1	Sediment/Detention Basin (VIN1A) - property acquisition not included; Sediment/Detention Basin (VIN1B) - property acquisition not included; 2,240' of Channel Improvements	\$29,500,000	x			ı	0.09
MON1	Sediment/Retention Basin	\$15,780,000	X				0.04
HAC2	Sediment/Retention Basin at Location A; Sediment/Retention Basin at Location B	\$37,810,000	X			1	0.02
CAN3	2 - 6' x 3' CBC	\$200,000		Х		I	0
SSA5	Sparks Channel; 6 - 10' x 4' CBC	\$12,300,000			Х	ı	0
SOC4	Sediment/Detention Basin	\$1,500,000	X			Ш	0.49
SSA2	Detention Basin SSA2	\$7,190,000	Х			Ш	0.36
SOC3	Sediment/Detention Basin	\$1,100,000	X			Ш	0.33
MON3	Sediment/Detention Basin	\$25,800,000	Х			Ш	0.31
HAC3	Sediment/Retention Basin	\$2,710,000	X			Ш	0.21
HAC6	Sediment/Retention Basin	\$4,470,000	Х			Ш	0.19
TOR1	Sediment/Retention Basin (TOR 1 & TOR3) - 6-foot embankment; Sediment Basin (TOR1A)	\$3,120,000	x			II	0.18
SSA3	Detention Basin SSA3; Concrete Lined Channel	\$1,510,000	Х			Ш	0.12
VIN3	1,600' of Channel Improvements	\$160,000			X	Ш	0.09
HAC1	Low-level/Principal Spillway Outlet	\$1,080,000	X			Ш	0.02
MON7	4 - 7' x 4' CBC	\$450,000		Χ		Ш	0
MON15	14 - 12' x 9' CBC	\$1,470,000		Χ		Ш	0
FAB3	Upgrade Fabens Dam	\$1,750,000	X			Ш	0
VIN6	3 - 9' x 8' CBC	\$880,000		Χ		Ш	0.45
VIN5	2,054' of Channel Improvements	\$1,210,000			X	Ш	0.45
HAC5	Sediment/Retention Basin	\$2,920,000	X			Ш	0.13

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Table 7-1. Prioritization Summary (Continued)

			Type of				
			Improvement		Prior	itization	
Project No.	Description	Estimated Total Cost (Rounded to \$10,000)	Basin	Crossing	Channel	Tier	Benefit- Cost Ratio (BCR)
VIN2	950' of Channel Improvements	\$330,000			Χ	III	0.05
HAC4	Sediment/Retention Basin	\$1,890,000	X			III	0.04
TOR5	165' of Channel Bank Improvements	\$280,000			Χ	III	0.03
VIN4	4,500' of Channel Improvements - property acquisition not included	\$1,170,000			X	III	0.03
SSA6	Sediment Basin SSA6_A; North Channel for Basin at Location A; South Channel for Basin at Location A; Sediment Basin SSA6_B; North Channel for Basin at Location B; South Channel for Basin at Location B	\$2,700,000	x			III	0.01
TOR3	Sediment Basin (TOR3A)	\$60,000	X			III	0
TOR6	2 - 4' x 2' CBC	\$70,000		Х		III	0
HAC9	3 - 4' x 4' CBC	\$150,000		Х		III	0
SOC6	2 - 7' x 7' CBC	\$170,000		Х		III	0
SOC7	2 - 7' x 7' CBC	\$190,000		Х		III	0
SOC5	3 - 4' x 4' CBC	\$200,000		Х		III	0
MON8	7 - 8' x 5' CBC	\$210,000				III	0
SOC8	2 - 7' x 7' CBC	\$260,000		Х		III	0
VIN12	3 - 9' x 5' CBC	\$270,000		Х		III	0
HAC13	2 - 7' x 7' CBC	\$270,000		Х		III	0
HAC14	2 - 7' x 7' CBC	\$300,000		Х		III	0
MON4	7 - 9' x 5' CBC	\$320,000		Х		III	0
MON5	7 - 9' x 5' CBC	\$320,000		Х		III	0
MON6	7 - 9' x 5' CBC	\$320,000		Х		III	0
VIN13	5 - 7' x 4' CBC	\$340,000		X		III	0
VIN14	6 - 6' x 6' CBC	\$420,000		Х		Ш	0
HAC8	5 - 4' x 4' CBC (In conjunction with HAC2 Basin B)	\$570,000		X		III	0
HAC11	2 - 7' x 7' CBC	\$590,000		Х		Ш	0
FAB2	Property	\$590,000			X	III	0
MON9	6 - 7' x 4' CBC	\$610,000		Х		Ш	0
HAC10	2 - 7' x 7' CBC	\$620,000		Х		III	0
HAC12	2 - 7' x 7' CBC	\$650,000		Х		Ш	0
VIN7	84' span bridge	\$830,000		Х		Ш	0
VIN11	58' span bridge	\$940,000		Х		Ш	0
VIN10	58' span bridge	\$990,000		Х		Ш	0
MON10	11 - 9' x 5' CBC	\$1,020,000		Х		Ш	0
MON11	11 - 9' x 5' CBC	\$1,020,000		Х		Ш	0
MON12	11 - 9' x 5' CBC	\$1,020,000		Χ		Ш	0

Table 7-1. Prioritization Summary (Continued)

			Type of Improvement		Prioritization		
Project No.	Description	Estimated Total Cost (Rounded to \$10,000)	Basin	Crossing	Channel	Tier	Benefit- Cost Ratio (BCR)
TOR2	2,030' of Channel Bank Improvements	\$1,040,000			Х	III	0
MON13	11 - 9' x 5' CBC	\$1,390,000		Х		III	0
MON14	14 - 12' x 9' CBC	\$1,470,000		Χ		III	0
VIN8	56' span bridge	\$1,700,000		Х		III	0
TOR4	Sediment/Retention Basin	\$1,750,000	Х			III	0
VIN9	110' span bridge	\$1,910,000		Х		III	0

8.0 COUNTYWIDE STORMWATER POLICY RECOMMENDATIONS

As the El Paso County SMP was being prepared, it became apparent that a number of issues contribute to drainage problems across the County. The primary issues involve construction in arroyos or drainage flow paths. This construction varies from an individual filling in private property that is in a drainage flow path to construction of subdivisions in drainage flow paths. The impacts of all this construction are additional flooding, property damage, and potential safety concerns. These problems have been observed in both incorporated and unincorporated areas of the County.

A number of factors contribute to construction within a flow path:

- Many individuals grade and build on their property without submitting drainage and grading plans to the County for review and without understanding the impacts that they are having on drainage.
- In some areas of the County, there are no clearly defined drainage channels. As a
 result of these ill-defined drainage flow paths, individuals may construct in the
 drainage flow paths without realizing that they are creating a problem. This
 construction can reduce the capacity of the drainage flow path and/or change the
 direction of flood flows.

Another overriding issue is that drainage problems often cross jurisdictional boundaries. It is not uncommon for a drainage flow path to begin in an unincorporated part of the County, and pass from one city or village into another. Therefore, two to four different entities ultimately may be affected by a single drainage flow path. Each of these entities may have its own drainage criteria, development criteria, construction permit requirements, and enforcement standards. In such a case, when one entity does not enforce drainage standards it can cause drainage problems in other entities. With multiple entities, it is also difficult to coordinate solutions and different jurisdictions may have different approaches or timelines to implement their solutions.

There appear to be three primary inter-jurisdictional problems associated with drainage issues that should be addressed:

- 1. Lack of consistent drainage and development standards;
- 2. Lack of consistent enforcement of these standards; and
- 3. Lack of resources to implement and enforce the standards.

8.1 City and County Legal Authority to Control Drainage

Preventing drainage problems is generally less costly than fixing the results of poorly thought out development decisions or lack of standards to guide development. The latitude afforded cities and counties in Texas is guided by and limited by state law as well as local policy. Generally, county discretion is limited and development standards are an important example of that limitation.

Counties in Texas have general statutory authority over platting of subdivisions and management of floodplain areas (under FEMA guidelines). Both of these tools can be used to

manage some of the issues mentioned above. Where property has been formally platted, drainage easements reflecting either channels or swales should be included in plats and enforced at the county level. Some property is developed, however, without formal plats (usually for smaller parcels or where a family subdivides). In both cases, FEMA floodplain management rules can be invoked to prevent property owners from impacting drainage and enforced at the county level.

Border counties and cities have greater latitude to manage such development than non-border counties. A firm understanding of where El Paso County regulation (and El Paso County's municipal regulation authority) could be modified to address current issues and to prevent future problems is desirable. More options may be available to guide development and drainage regulation solutions than are currently being used.

With the passage of the Economically Distressed Areas Program (EDAP) in 1989 and subsequent amendments, the Texas Legislature gave certain cities and counties additional powers to regulate development. Drainage standards are included in those regulatory powers. The local government code (in Chapters 212 and 232) gives significantly greater authority to border counties, cities, and cities' extraterritorial jurisdiction areas (ETJs) to require additional standards for development. A legal review of these powers and duties is recommended so that both El Paso County and other municipalities in the County can fully understand the limits of their authorities, and target those powers to address, prevent, and mitigate costly drainage issues. Many of the potential solutions are dependent on this understanding being appropriately applied.

In addition, the Model Subdivision Rules (MSRs) (a requirement of the EDAP Legislation) only address drainage at a cursory level. This is not surprising given the driving forces behind the EDAP Legislation (water and sewer services in the state's *colonias*). However, integrating these two issues (water service and drainage) can lead to more satisfactory and sustainable solutions to what is ultimately a housing problem. Further clarification and emphasis of drainage requirements in the MSRs by the state agencies charged with developing and enforcing them, might add further substance to the limits and authorities of cities and counties with respect to development and drainage.

8.2 Potential Inter-Jurisdictional Authority to Control Drainage

As described previously, countywide clarification and, perhaps, additional regulation, is needed to address the fact that many drainage issues impact multiple jurisdictions within the County (cities and areas outside of any municipality). Addressing these issues will require a common set of standards and some way of integrating solutions in an appropriate manner. In addition to standards, an explicit policy to address these issues (both methodology and standards) should be developed. Such a goal can be achieved through formal agreements between communities.

8.3 Public Information Program

As the County addresses the various recommendations described above (and perhaps in coordination with others) it will likely find it desirable to develop a public information program to describe the intended new programs and actions, and their rationale to the local community. Many similar public information programs have been quite successful in Texas and these should be reviewed for "lessons learned." The EPW's stormwater management and water

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conservation educational programs are good examples. There are many other examples of successful public information campaigns related to public infrastructure and related issues that could be used as the basis for an El Paso County effort.

8.4 Stormwater Management Information Resources

Information related to stormwater management at a number of jurisdictional levels is available on the internet. Although not all of these resources specifically pertain to the unincorporated portions of El Paso County, they provide information that can be utilized as guidance. Two resources in particular that provide beneficial information are listed below:

- The FEMA National Flood Insurance Program Website
 Found at http://www.fema.gov/plan/prevent/floodplain/index.shtm, this website provides Federal information on floodplain management and contains links to Federal laws, FIRMS, and many additional floodplain management resources. The link for viewing FIRMS is http://msc.fema.gov.
- The City of El Paso Engineering Department Website
 Found at http://www.elpasotexas.gov/engineering, this website provides information on flood zones in El Paso and contains a link to the City of El Paso DDM. The DDM provides guidance and criteria for design of stormwater conveyance within the City of El Paso.

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A.1.0 BACKGROUND

A hydrologic analysis was performed for each of the eight study areas to estimate peak storm flows that would occur for extreme storm events. The analysis consisted of the following steps:

- Watersheds boundaries were delineated;
- Curve Numbers were estimated for each watershed;
- Lag Times were estimated for each watershed;
- Routing parameters were estimated for each flowpath;
- Large detention structures were analyzed;
- The effect of small ponds was analyzed;
- Precipitation was estimated; and
- Hydrologic models were developed for each study area.

Detailed descriptions of the steps, assumptions, and results of the analysis are presented in this Appendix. Summaries of pertinent data, calculations, tables, and figures are located at the end of this Appendix. An overview of the project area is provided on Figure A-1.

Hydrologic analysis for the Sparks Arroyo and Sub Basin A Study Area was performed by the U.S. Army Corp of Engineers (USACE) as part of a feasibility study. Data from the USACE hydrologic analysis were used for this Stormwater Master Plan (SMP), and updated as part of this analysis.

A.2.0 DATA SOURCES

Table A-1 lists the sources used in the hydrologic analysis, as well as the specific calculation(s) each source was used for.

A.3.0 WATERSHED DELINEATION

A.3.1 Method Overview

Watershed boundaries were delineated for much of the El Paso County Stormwater Master Plan (SMP) study area based on 3-foot contours generated from the 2004 Texas Department of Transportation (TxDOT) topography and 2014 Rio Grande LiDAR. ArcGIS Desktop was utilized to digitize the watershed boundaries for use in hydrologic analysis. The purpose of the El Paso County SMP is to develop projects to improve the performance of the natural and constructed drainage infrastructure to provide protection in flood events us large as the 100-year frequency storm. To accomplish this, watersheds were delineated in order to estimate hydrologic flows for the existing condition at the downstream end of identified study reaches, as well as at key crossings and existing dam locations. Each watershed polygon was assigned a unique name based on the element or primary flow path that the watershed contributed to. Successive watersheds contributing to the same flow path were labeled with a number at the end of the name, increasing in the upstream direction.

A.3.2 Watershed Delineation, Vinton Study Area

New watersheds for the Vinton study area were digitized by hand as described above utilizing the 2004 TxDOT topography and 2008 El Paso County Orthophotography. Where available, watershed delineations from the City of El Paso Stormwater Master Plan were used. The overall analyzed drainage area consisted of 25.3 square miles and was delineated into 39 watersheds. Figure A-2 shows the watershed delineations for the Vinton study area.

A.3.3 Watershed Delineation, Canutillo Study Area

Where available, watershed delineations from the Federal Emergency Management Agency (FEMA) update and analysis of the Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS) for El Paso County, were used for the Canutillo study area. New Watersheds for the area were digitized by hand as described above utilizing the 2004 TxDOT topography and 2008 El Paso County Orthophotography. The overall analyzed drainage area consisted of 3.1 square miles and was delineated into 8 watersheds. Figure A-3 shows the watershed delineations for the Canutillo study area.

A.3.4 Watershed Delineation, Sparks Arroyo and Sub Basin A Study Area

Watersheds for the Sparks Arroyo and Sub Basin A Study Area were delineated by USACE. Watershed delineations were subdivided and updated in Sparks Arroyo using 2014 Rio Grande LiDAR as part of a restudy of project SSA4. Figure A-4 shows the watershed delineations for the Sparks Arroyo and Sub Basin A study area.

A.3.5 Watershed Delineation, Socorro Study Area

Watersheds for the Socorro study area were digitized by hand as described above utilizing the 2004 TxDOT topography and 2008 El Paso County Orthophotography. The overall analyzed drainage area consisted of 7.6 square miles and was delineated into 15 watersheds. Figure A-5 shows the watershed delineations for the Socorro study area.

A.3.6 Watershed Delineation, Hacienda Real Study Area

Watersheds for the Hacienda Real study area were digitized by hand as described above utilizing the 2004 TxDOT topography and 2008 El Paso County Orthophotography. The overall analyzed drainage area consisted of 25.3 square miles and was delineated into 39 watersheds. Figure A-6 shows the watershed delineations for the Hacienda Real study area.

A.3.7 Watershed Delineation, Fabens Study Area

New watersheds for the Fabens study area were digitized by hand as described above utilizing the 2004 TxDOT topography and 2008 El Paso County Orthophotography. Where available, watershed delineations from the Federal Emergency Management Agency (FEMA) update and analysis of the Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS) for El Paso County were used and modified as necessary to cover the differences in study area and limits. The overall analyzed drainage area consisted of 26.5 square miles and was delineated into 14 watersheds. Figure A-7 shows the watershed delineations for the Fabens study area.

A.3.8 Watershed Delineation, Tornillo Study Area

Watersheds for the Tornillo study area digitized by hand as described above utilizing the 2004 TxDOT topography and 2008 El Paso County Orthophotography. The overall analyzed drainage area consisted of 3.1 square miles and was delineated into 12 watersheds. Figure A-8 shows the watershed delineations for the Tornillo study area.

A.3.9 Watershed Delineation, Montana Sector Study Area

Watersheds for the Montana Sector study area digitized by hand as described above utilizing the most recent where available of a combination of the 2014 Rio Grande LiDAR and the 2004 TxDOT topography. The overall analyzed drainage area consisted

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of 121.3 square miles and was delineated into 74 watersheds. Figure A-9 shows the watershed delineations for the Montana Sector study area.

A.4.0 CURVE NUMBER ESTIMATION

A.4.1 Method Overview

Runoff losses were modeled in Hydrologic Engineering Center's Hydraulic Modeling System (HEC-HMS) by selecting the Soil Conservation Service (SCS) Curve Number Loss Method. This method requires the user to input the SCS Curve Number, Percent Impervious Cover, and Initial Abstraction. SCS Type II Curve Numbers were assigned based on the combination of hydrologic soil groups (HSGs) and land use cover description according to the El Paso Drainage Design Manual (DDM), Tables 4-9 and 4-10 (City of El Paso, 2008); which is summarized in Tables A-3, A-4 and A-5.

When entering the curve number parameters into the HEC-HMS Model, the percent impervious cover was left as 0 percent (%) because it is already accounted for in the Curve Number Calculation Method described below. The initial abstraction parameter defines the amount of rainfall that must fall before surface runoff occurs. This value was left blank, and by default, HEC-HMS calculates it as 0.2 times the potential retention.

HSGs were determined using the soil type shapefile for El Paso County available from the Soil Survey Geographic Database (SSURGO) (United States Department of Agriculture [USDA], 2004). The SSURGO soil shapefile delineates soil according to soil types, which were correlated to HSG based on a key code also available from SSURGO, summarized in Table A-2. Soils were classified as Soil Group A, B, C, D, Water, or Sink. Sinks are areas such as landfills or quarries that collect water and are thus not included in runoff calculations.

Land use types were estimated using 2008 Orthophotography (El Paso County, 2008) and hand delineated in ArcView. Polygons were digitized according to the land use cover categories provided in the DDM. Each polygon was assigned a Land Use Cover Type text attribute and a Land Use Identification (ID) numerical attribute corresponding to Tables A-6 and A-7 at the end of this Appendix.

A curve number shapefile was created by combining the land use and soils shapefiles using the ArcView Union tool. The curve number shapefile contained both the HSG and Land Use ID for each polygon. Curve numbers were then assigned according to the DDM for each soil group-land use combination. Finally, a union was created between the curve number shapefile and the watershed boundary shapefile, and the area-weighted average curve number for each watershed was calculated using the following equation:

$$CN_{avg} = \frac{\sum AreaxCN}{\sum Area Sum}$$

A.4.2 Curve Number Estimation, Vinton Study Area

Where appropriate, the curve number estimation of the Vinton area was found using the process described above. Flow Path Number 45 and Flow Path Number 45A were not included in this process for the County because the hydrology was completed with the City of El Paso's Stormwater Master Plan. Results for the Vinton study area curve number estimation for the appropriate channels are given in Table A-8. A map of soil types is provided on Figure A-10, and a map showing Land Use categories delineated is provided on Figure A-11, found at the end of this Appendix.

A.4.3 Curve Number Estimation, Canutillo Study Area

Results for the Canutillo study area curve number estimation are given in Table A-9. A map of soil types is provided on Figure A-12, and a map showing Land Use categories delineated is provided on Figure A-13, found at the end of this Appendix.

A.4.4 Curve Number Estimation, Socorro Study Area

Results for the Socorro study area curve number estimation are given in Table A-10. A map of soil types is provided on Figure A-14, and a map showing Land Use categories delineated is provided on Figure A-15, found at the end of this Appendix.

A.4.5 Curve Number Estimation, Hacienda Real Study Area

Results for the Hacienda Real study area curve number estimation are given in Table A-11. A map of soil types is provided on Figure A-16, and a map showing Land Use categories delineated is provided on Figure A-17, found at the end of this Appendix.

A.4.6 Curve Number Estimation, Fabens Study Area

Results for the Fabens study area curve number estimation are given in Table A-12. A map of soil types is provided on Figure A-18, and a map showing Land Use categories delineated is provided on Figure A-19, found at the end of this Appendix.

A.4.7 Curve Number Estimation, Tornillo Study Area

Results for the Tornillo study area curve number estimation are given in Table A-13. A map of soil types is provided on Figure A-20, and a map showing Land Use categories delineated is provided on Figure A-21, found at the end of this Appendix.

A.4.8 Curve Number Estimation, Montana Sector Study Area

Results for the Montana Sector study area curve number estimation are given in Table A-14. A map of soil types is provided on Figure A-20, and a map showing Land Use categories is provided on Figure A-21, found at the end of this Appendix. The National Land Cover Dataset (NLCD) was used to define land use.

A.5.0 LAG TIME ESTIMATION

A.5.1 Method Overview

The lag time was calculated for each modeled watershed using the modified Snyder Method developed for the FIS for Northeast and Central El Paso conducted by US Army Corp of Engineers (USACE) in 1978 (USACE, February 1978). The methodology for the Snyder calculation is shown below:

$$T_{lag} = C_T (L_L * L_{CA})^{0.3}$$

where: $T_{lag} = Lag Time (hrs);$

C_T = Regional Coefficent (Plate A-3, USACE, February 1978);

L_L= Length of longest flow path (mi);

L_{CA} = Length from longest flow path centroid to outlet of watershed (mi).

The regional coefficient, C_T , was estimated according to equivalent slope based on the curves for undeveloped areas and urban areas found in Plate A3 of the USACE 1978 Report (USACE, February 1978). Equivalent slope was assumed to be the slope between the 10% and 85% marker elevations, traveling upstream along the longest flow path.

The Snyder peaking coefficient, cp, was defined according to the following guidelines:

$$640c_p = 430 if slope \left(\frac{ft}{ft}\right) < 0.015$$

$$640c_p = 392 if slope \left(\frac{ft}{ft}\right) > 0.015$$

The longest flowpath was digitized by referencing 2004 TxDOT Contours (TxDOT, 2004). A polyline was created in ArcView connecting the furthest upstream point in the watershed to the watershed outlet, while following a path of decreasing elevation. Physical barriers that were visible in the 2008 Orthophotography (El Paso County, 2008) were taken into account while estimating the longest flow path for each watershed.

A.5.2 Lag Time Estimation, Vinton Study Area

Lag Times for the Vinton study area were estimated using the method described above and are summarized in Table A-15. Longest flowpaths for the Vinton study area are shown on Figure A-24 located at the end of this Appendix. Flow Path Number 45 and Flow Path Number 45A were not included in this estimation because the hydrology used was taken from the City of El Paso Stormwater Master Plan.

A.5.3 Lag Time Estimation, Canutillo Study Area

Lag Times for the Canutillo study area were estimated using the method described above and are summarized in Table A-16. Longest flowpaths for the Canutillo study area are shown on Figure A-25 located at the end of this Appendix.

A.5.4 Lag Time Estimation, Socorro Study Area

Lag Times for the Socorro study area were estimated using the method described above and are summarized in Table A-17. Longest flowpaths for the Socorro study area are shown on Figure A-26 located at the end of this Appendix.

A.5.5 Lag Time Estimation, Hacienda Real Study Area

Lag Times for the Hacienda Real study area were estimated using the method described above and are summarized in Table A-18. Longest flowpaths for the Hacienda Real study area are shown on Figure A-27 located at the end of this Appendix.

A.5.6 Lag Time Estimation, Fabens Study Area

Lag Times for the Fabens study area were estimated using the method described above and are summarized in Table A-19. Longest flowpaths for the Fabens study area are shown on Figure A-28 located at the end of this Appendix.

A.5.7 Lag Time Estimation, Tornillo Study Area

Lag Times for the Tornillo study area were estimated using the method described above and are summarized in Table A-20. Longest flowpaths for the Tornillo study area are shown on Figure A-29 located at the end of this Appendix.

A.5.8 Lag Time Estimation, Montana Sector Study Area

Lag Times for the Montana Sector study area were estimated using the method described above and are summarized in Table A-21. Longest flowpaths for the Montana Sector study area are shown on Figure A-30 located at the end of this Appendix.

A.6.0 HYDROLOGIC ROUTING

A.6.1 Method Overview

Once watershed delineations were completed, flowpaths were identified and the HEC-HMS model was constructed. A routing shapefile was digitized in ArcView containing the reaches corresponding to the HEC-HMS Model. When generating the routing schematic, the assumption was made that flow would be conveyed along the drainage infrastructure and would not be diverted due to insufficient capacity and overtopping. The HEC-HMS Muskingum-Cunge Method of routing was selected for all open channel reaches. In this method, the user first enters the channel shape. If "trapezoid" is selected, the user enters a channel slope, and Manning's Roughness Coefficient and channel bottom width. If "eight point" is selected, then the X-Y coordinates for the channel cross-section are entered into the paired-data editor, along with the Manning's Roughness Coefficient.

Several data sources were available for the estimation of cross-section geometry. The first source utilized was site visit measurements. Additional survey was also performed at crossings which helped to more accurately estimate channel geometry and verify site visit measurements. Where no more reliable data was available, TxDOT 2004 Topography (TxDOT, 2004) was used along with El Paso County 2008 Orthophotography.

Note that hydrologic modeling for the Montana Sector was set up to run with an unsteady 2D hydraulic model. Because 2D hydraulic modeling routes flows, a hydrologic routing analysis was not necessary. Thus routing was not performed for the Montana Sector.

A.6.2 Hydrologic Routing, Vinton Study Area

Routing for the Vinton study area open channels and arroyos was estimated using the method described above. For natural arroyos, no site visit measurements or survey were available, so routing dimensions were based solely on the 2004 Topography (TxDOT) and the 2008 Orthophotography (El Paso County). Channel routing inputs for the Vinton study area are provided in Table A-22. Figure A-31 shows the routing reaches for the Vinton study area. Flow Path Number 45 and Flow Path Number 45A were not included in this process because the hydrology was completed with the City of El Paso Stormwater Master Plan.

A.6.3 Hydrologic Routing, Canutillo Study Area

Routing for the Canutillo study area open channels and arroyos was estimated using the method described above. For natural arroyos, no site visit measurements or survey were available, so routing dimensions were based solely on the 2004 Topography

(TxDOT) and the 2008 Orthophotography (El Paso County). Channel routing inputs for the Canutillo study area are provided in Table A-23. Figure A-32 shows the routing reaches for the Canutillo study area.

A.6.4 Hydrologic Routing, Socorro Study Area

Routing for the Socorro study area open channels and arroyos was estimated using the method described above. For natural arroyos, no site visit measurements or survey were available, so routing dimensions were based solely on the 2004 Topography (TxDOT) and the 2008 Orthophotography (El Paso County). Channel routing inputs for the Socorro study area are provided in Table A-24. Figure A-33 shows the routing reaches for the Socorro study area.

A.6.5 Hydrologic Routing, Hacienda Real Study Area

Routing for the Hacienda Real study area open channels and arroyos was estimated using the method described above. For natural arroyos, no site visit measurements or survey were available, so routing dimensions were based solely on the 2004 Topography (TxDOT) and the 2008 Orthophotography (El Paso County). Channel routing inputs for the Hacienda Real study area are provided in Table A-25. Figure A-34 shows the routing reaches for the Hacienda Real study area.

A.6.6 Hydrologic Routing, Fabens Study Area

Routing for the Fabens study area open channels and arroyos was estimated using the method described above. For natural arroyos, no site visit measurements or survey were available, so routing dimensions were based solely on the 2004 Topography (TxDOT) and the 2008 Orthophotography (El Paso County). Channel routing inputs for the Fabens study area are provided in Table A-24. Figure A-35 shows the routing reaches for the Fabens study area.

A.6.7 Hydrologic Routing, Tornillo Study Area

Routing for the Tornillo study area open channels and arroyos was estimated using the method described above. For natural arroyos, no site visit measurements or survey were available, so routing dimensions were based solely on the 2004 Topography (TxDOT) and the 2008 Orthophotography (El Paso County). Channel routing inputs for the Tornillo study area are provided in Table A-25. Figure A-36 shows the routing reaches for the Tornillo study area.

A.7.0 MODELING OF SIGNIFICANT DETENTION STRUCTURES

A.7.1 Method Overview

Significant detention structures were modeled in HEC-HMS using a stage-areadischarge relationship.

A stage-area-discharge relationship was developed for each existing basin. The relationship dictated how the upstream flow was attenuated by the reservoirs and associated dam structures. The relationship consists of a stage elevation versus a storage area versus a dam discharge, starting at the bottom elevation of the dam's storage reservoir and increasing to the top elevation of the dam embankment. This relationship is defined by the components of the dam, its storage basin, its embankment size and height, and its outflow structures. Reservoirs without outflow structures were assumed to hold flow until the structure overtopped.

Dams identified by the county and consisting of outflow structures were modeled in the Water Resources Site Analysis Program (SITES), which used information from survey data obtained by the County, TxDOT contours and 2008 Orthophotos (El Paso County, 2008). The total stage-area-discharge table produced by SITES was the input used to model the dams in HEC-HMS for this study.

A.7.2 Significant Detention Structures, Vinton Study Area

There are no existing significant detention structures modeled in the Vinton study area.

A.7.3 Significant Detention Structures, Canutillo Study Area

There are no existing significant detention structures modeled in the Canutillo study area.

A.7.4 Significant Detention Structures, Socorro Study Area

There are no existing significant detention structures modeled in the Socorro study area.

A.7.5 Significant Detention Structures, Hacienda Real Study Area

There are no existing significant detention structures modeled in the Hacienda Real study area.

A.7.6 Significant Detention Structures, Fabens Study Area

The Fabens study area consists of six existing detention structures. The analysis of each structure used the process described above. The location and stage-area-discharge was determined in ArcView using available survey data, 2004 Contours (TxDOT) and the 2008 Orthophotography (El Paso County, 2008). Three of the six structures utilized SITES to determine the total stage-area-discharge table to input into HEC-HMS. The existing structures that did not use SITES are located at the downstream end of Fabens North 1 and along San Felipe Arroyo.

Structures along the San Felipe Arroyo that used the SITES program to generate the total stage-area-discharge table are named Roberts Tank, Rattlesnake Lake, and Dam No.6. Outlet information and survey provided by the County, and ArcView information described above, was used for the necessary input data required by the SITES program. The other two basins are Phelps Dodge Detention Basin and Fabens Lake. Fabens Lake was analyzed during the Federal Emergency Management Agency (FEMA) update and analysis of the Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS) for El Paso County. The data from this analysis was used for the HEC-HMS model. Phelps Dodge Detention Basin used CulvertMaster to determine the discharge rating curve of the outlet. Due to the simplicity of the basin outlet consisting of 4 – 8 inch PVC pipes, analysis within CulvertMaster was appropriate.

The locations of the existing structures are shown in Figure A-37 at the end of this Appendix.

A.7.7 Significant Detention Structures, Tornillo Study Area

The Tornillo study area consists of two existing detention structures. Each structure was analyzed using the method described above. The location and stage-storage-discharge relationship was determined in ArcView using available survey data, 2004 Contours (TxDOT) and the 2008 Orthophotography (El Paso County, 2008).

The locations of the existing structures are shown in Figure A-37 at the end of this Appendix.

A.7.8 Significant Detention Structures, Montana Sector Study Area

There are no existing significant detention structures modeled in the Montana Sector study area.

A.8.0 SMALL PONDS

A.8.1 Method Overview

In addition to the significant detention structures described in Section A-7, some study areas have several small ponds that would contribute little to no run-off in the 100-year design storm. These ponds are too small, too numerous, and without sufficient information to incorporate into the existing condition model as reservoirs. To account for these ponds, the total ponding area was removed from the total contributing watershed area.

The location of each pond was determined in ArcView, using 2008 Orthophotos (El Paso County, 2008).

A.8.2 Small Ponds, Vinton Study Area

There are no small ponds to be accounted for in the Vinton study area.

A.8.3 Small Ponds, Canutillo Study Area

There are no small ponds to be accounted for in the Canutillo study area.

A.8.4 Small Ponds, Socorro Study Area

Areas were adjusted for eight watersheds in the Socorro study area, due to the capacity provided by the small ponds not modeled as reservoirs in HEC-HMS. The adjusted watershed areas are provided in Table A-28 at the end of this Appendix.

In addition to the ponds accounted for in the area reduction, there were a number of retention ponds located within the El Paso Hills development. It was determined that reducing the watershed area to account for these ponds would not accurately represent the volume retained by them. For these ponds, the storage provided was accounted for by a reduction in the SCS Curve Number as described below

The location of each pond was determined in ArcView, using 2008 Orthophotos (El Paso County, 2008). TxDOT topography (TxDOT, 2004) data was used to estimate the volume of each pond.

Using the 100-year precipitation depth from the HEC-HMS model using the initial curve number as calculated in Section A.4.0 the watershed runoff was calculated using the following formulas:

$$Q = \frac{(P - 0.2 * S)^2}{(P + 0.8 * S)}$$
 and $S = \frac{1000}{CN} - 10$

where:

Q = Calculated runoff (inches) P = Precipitation (inches) CN = Curve Number

The runoff depth obtained from the initial HEC-HMS run was then adjusted to account for the storage provided by the small ponds within each watershed. The total depth of storage over the watershed was divided by the watershed area to estimate depth of runoff that would potentially be captured. This number was then subtracted from the depth of runoff obtained from the initial run of the HEC-HMS Model with the unadjusted curve numbers to obtain the depth of runoff that might occur with the pond storage accounted for. The curve numbers were then back-calculated using this modified runoff value per the above equations.

Curve numbers were adjusted for 2 watersheds in the Socorro study area due to the capacity provided by the retention ponds not modeled as reservoirs in HEC-HMS. The adjusted curve numbers for the Socorro study area are provided in Table A-29 at the end of this Appendix.

A.8.5 Small Ponds, Hacienda Real Study Area

Areas were adjusted for eight watersheds in the Hacienda Real study area, due to the capacity provided by the small ponds not modeled as reservoirs in HEC-HMS. The adjusted watershed areas are provided in Table A-30 at the end of this Appendix.

A.8.6 Small Ponds, Fabens Study Area

There are no small ponds to be accounted for in the Fabens study area.

A.8.7 Small Ponds, Tornillo Study Area

There are no small ponds to be accounted for in the Tornillo study area.

A.8.8 Small Ponds, Montana Sector Study Area

Because the Montana Sector hydrologic model is set up to run with an unstead 2D hydraulic analysis, which takes ponding into account, a small ponds analysis was not necessary.

A.9.0 ESTIMATION OF RAINFALL

Precipitation was estimated utilizing the "Frequency Storm" function in HEC-HMS along with the depth-duration-frequency data from Atlas-14 at the centroid of the combined west (Vinton & Canutillo) and east (Spark Arroyo and Sub Basin A, Socorro, Hacienda Real, Fabens, Tornillo, and Montana Sector) study areas. Using this method, the user enters the depth of rainfall that occurs for various durations for a given storm. Additional inputs required include the intensity duration, the storm duration and intensity position.

El Paso rainfall totals are provided in Table A-31.

A.10.0 ASSEMBLY OF HYDROLOGIC MODELS

A.10.1 Method Overview

Hydrologic models were developed for each of the six study areas. These models contained the following elements representing the major contributing drainage features of the project area:

- Watershed Area;
- Flow Diversion;
- Junction;
- Routing Reach; and
- Dam/Basin/Sump.

The specific approaches and assumptions used to model the various elements can be found in the individual study area descriptions.

A.10.2 Hydrologic Model - Vinton Study Area

The Vinton study area HEC-HMS model consists of 4 watershed areas, 2 junctions, 2 reaches, and 1 sink. There are two natural arroyos modeled in this study area. The arroyos are Flow Path Number 44 and Flow Path Number 43. A sink was placed at the outlet of the arroyos to represent the convergence with the Rio Grande. HEC-HMS modeling for Flow Path Number 45 and Flow Path Number 45A were not included in this model because the hydrology was completed with the City of El Paso Stormwater Master Plan.

The Vinton study area HEC-HMS model schematic, for the appropriate arroyos, is shown in Figure A-39 at the end of this Appendix.

A.10.3 Hydrologic Model - Canutillo Study Area

The Canutillo study area HEC-HMS model consists of 8 watershed areas, 5 junctions, 4 reaches, and 2 sinks (used to model existing basin endpoint and system outlet to the Rio Grande). There are five natural arroyos and one concrete lined channel that was modeled in this study area. The natural arroyos are Flow Path Number 42, Flow Path Number 42A, Flow Path Number 42B, Flow Path Number 42C, and Flow Path Number 42D. The concrete lined channel was unnamed and was designated First Ave. Channel for the purposes of the SMP. There are no existing detention or retention basins located in the Canutillo study area.

The Canutillo study area HEC-HMS model schematic is shown in Figure A-40 at the end of this Appendix.

A.10.4 Hydrologic Model - Socorro Study Area

The Socorro study area HEC-HMS model consists of 15 watershed areas, nine junctions, and 16 reaches. There were three natural arroyos that were modeled in this study area. These arroyos are named Stream 4, Stream 5, and an unnamed arroyo that is designated as Stream 5.5 for the purposes of this SMP. A portion of the Mesa Spur Drain is also located in the Socorro study area. This drain was not modeled because it was not identified as an issue during initial meetings with the County. This was confirmed through witness accounts during the initial site visits.

The Socorro study area HEC-HMS model schematic is shown in Figure A-41 at the end of this Appendix.

A.10.5 Hydrologic Model - Hacienda Real Study Area

The Hacienda Real study area HEC-HMS model consists of 39 watershed areas, four diversions, 26 junctions, 29 reaches, and three sinks (used to model existing basin storage). There were nine natural arroyos that were modeled in this study area. These arroyos are named Stream 6, Stream 7, Stream 8, Stream 9, Stream 10, Stream 11, Stream 12, Stream 13 and an unnamed arroyo that is designated as Stream 13.5 for the purposes of this SMP. A portion of the Mesa Drain is also located in the Hacienda Real study area. This drain was not modeled because it was not identified as an issue during initial meetings with the County. This was confirmed through witness accounts during the initial site visits. The Clint Landfill was originally removed from the model because it was assumed that the landfill provided onsite detention sufficient to capture all run-off from within the landfill. Per information received from Parkhill Smith & Cooper (PSC), the majority of the ponds were actually only sized to retain the 25-year flood and have no outflow structures. Given this information, the Clint Landfill was incorporated back into the model with sinks were utilized to account for the known storage volumes.

Ponds evident in aerials with no data provided were omitted and the model was run as if the full watershed contributing to that pond ran offsite.

The Hacienda Real study area HEC-HMS model schematic is shown in Figure A-42 at the end of this Appendix.

A.10.6 Hydrologic Model - Fabens Study Area

The Fabens study area HEC-HMS model consists of 14 watershed areas, 6 junctions, 9 reaches, 6 basins and one sink. Five natural arroyos were modeled in this study area. These arroyos are San Felipe Arroyo and San Felipe Arroyo Trib. 1; three unnamed arroyos were designated Fabens North 1, Fabens North 2, and Fabens North 2 Trib. 1 for the purposes of the SMP. There are five dams along the San Felipe Arroyo which were identified by the county, Information obtained from the county led to the development of the input stage-area-discharge table from the SITES program, as described above, within the HEC-HMS model. One detention basin located at the downstream end of Fabens North 1 watershed was modeled to determine if the structure is able to provide sufficient detention for the 100-year storm event. The sink used models the outlet of the San Felipe Arroyo into the River Drain Canal.

The Fabens study area HEC-HMS model schematic is shown in Figure A-43 at the end of this Appendix.

A.10.7 Hydrologic Model - Tornillo Study Area

The Tornillo study area HEC-HMS model consists of 12 watershed areas, 6 juctions, 5 reaches, 2 basins and 1 sink. There are seven natural arroyos modeled in this study area. These arroyos are all unnamed arroyos and have been designated as High School Channel, High School Channel Trib. 1, High School Channel Trib. 2, South High School Channel, Flow Path T, Tornillo Handle Channel 1, and Tornillo Handle Channel 2 for the purposes of this SMP. There are two basins at the downstream end of High School Channel / South High School Channel and Flow Path T. Each existing basin was modeled in HEC-HMS to determine the structures ability to maintain the 100-year storm event volume. The flow from the defined channels designated as Tornillo Handle Channel 1 and Tornillo Handle Channel 2 currently flow to a natural low in the topography. This area was modeled as a sink to determine the amount of flow that needs to be controlled and contained in the area.

The Tornillo study area HEC-HMS model schematic is shown in Figure A-44 at the end of this Appendix.

A.10.8 Hydrologic Model - Montana Study Area

The Montana study area HEC-HMS model consists of 74 watershed areas, and no junctions, reaches, basins, or sinks. The outflow hydrograph from each watershed is designed to be inserted into the 2D hydraulic model directly at the outflow location, and routing and storage are handled in the hydraulic model.

The Montana study area HEC-HMS model schematic is shown in Figure A-45 at the end of this Appendix.

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TABLES

Table A-1. Data Sources Utilized in Hydrologic Analysis

Source	Used For
National Oceanic and Atmospheric Administration (NOAA), 2018, Atlas- 14, Volume 11, Version 2.0 for Texas (Atlas-14)	Precipitation
FEMA Region 6 TX, 2014, Rio Grande LiDAR	Watershed Delineation Lag Time
El Paso County, 2008. Orthophotography.	Watershed Delineation Curve Number Lag Time
ESRI ArcGIS Desktop, Version 9.2 (2006), Version 9.3.1 (2009) and Version 10.6 (2017)	Watershed Delineation Curve Number Lag Time
Texas Department of Transportation (TxDOT), El Paso Office, 2004.	Watershed Delineation
Photogrammetric Topography	Lag Time
US Army Corps of Engineers (USACE), 2018. Hydrologic Engineering Center's Hydrologic Modeling System (HEC-HMS), Version 4.3	HEC-HMS
USACE, September 2008. HEC-HMS Technical Reference Manual.	HEC-HMS
USACE – Albuquerque District, February 1978. Report on Hydrologic Investigations Flood Insurance Study (FIS) – Northeast and Central El Paso, Texas.	Lag Times
U.S. Department of Agriculture (USDA) National Resource Conservation Commission (NRCS), 2004. Soil Survey Geographic Database (SSURGO) Soil Data for El Paso County, Texas.	Curve Number
USDA Soil Conservation Service, Engineering Division, Technical Release 55 (TR-55), June 1986. Urban Hydrology for Small Watersheds.	Curve Number

Table A-2. Hydrologic Soil Groups in the El Paso Region

EL PASO HYDROLOGIC SOIL GROUPS				
Soil Type	Soil Abbreviation	HSG		
Hueco-Wink association, hummocky	HW	С		
Anapra silty clay loam	An	В		
Brazito loamy fine sand	Br	Α		
Gila fine sandy loam	Ga	В		
Gila Ioam	Gc	В		
Glendale loam	Gd	В		
Glendale silty clay loam	Ge	В		
Glendale silty clay	Gs	В		
Harkey loam	На	В		
Harkey silty clay loam	Hk	В		
Made land, gila soil material	Mg	В		
Saneli silty clay loam	Sa	D		
Saneli silty clay	Sc	D		
Tigua silty clay	Tg	D		
Vinton fine sandy loam	Vn	В		
Turney-Berino association, undulating	TBB	В		
Agustin association, undulating	AGB	В		
Badlands	BA	D		
Bluepoint association, rolling	BPC	А		
Bluepoint gravelly association, rolling	BUC	А		
Delnorte-Canutio association, undulating	DCB	D		
Delnorte-Canutio association hilly	DCD	D		
Dune land	DU	Α		
Igneous rock land	IG	D		
Igneous rockland-Brewster association	IN	D		
Rock outcrop-Lozier association	LM	D		
Lozier association, hilly	LOD	D		
Mimbres association, level	MBA	В		
Pajarito association, level	PAA	В		
Simona association, undulating	SMB	D		
Wink association, level	WKA	В		
Water	W	W		
Urban land, sanitary landfill	SLF	SINK		
Pits, gravel	GP	SINK		

Source: U.S. Department of Agriculture (USDA), Natural Resources Conservation Service (NRCS), 2004. Soil Survey Geographic Database (SSURGO) Soil Database for El Paso County, Texas.

Table A-3. Runoff Curve Numbers for Urban Areas

Hydrologic Soil Group	Hydrologic Soil Group		В	С	D
	Poor	68	79	86	89
Open Space	Fair	49	69	79	84
	Good	39	61	74	80
Commercial and Business	NA	89	92	94	95
Industrial	NA	81	88	91	93
Residential (1/8 acre or less)	NA	77	85	90	92
Residential (1/4 acre)	NA	61	75	83	87
Residential (1/2 acre)	NA	54	70	80	85
Residential (1 acre)	NA	51	68	79	84
Newly graded areas	NA	77	86	91	94
Highway	NA	98	98	98	98

Source: U.S. Department of Agriculture (USDA), Soil Conservation Service (SCS), 1986. Technical Release 55 (TR-55) Urban Hydrology for Small Watersheds.

Table A-4. Runoff Curve Numbers for Arid and Semi Arid Rangelands

Hydrologic Soil Grou	p	Α	В	С	D
	Poor		80	87	93
Herbaceous	Fair		71	81	89
	Good		62	74	85
	Poor		66	74	79
Oak-aspen	Fair		48	57	63
	Good		30	41	48
	Poor		75	85	89
Pinyon-juniper	Fair		58	73	80
	Good		41	61	71
	Poor		67	80	85
Sage-grass	Fair		51	63	70
	Good		35	47	55
	Poor	63	77	85	88
Desert Shrub	Fair	55	72	81	86
	Good	49	68	79	84

Source: U.S. Department of Agriculture (USDA), Soil Conservation Service (SCS), 1986. Technical Release 55 (TR-55) Urban Hydrology for Small Watersheds.

Table A-5. Runoff Curve Numbers for Agricultural Lands

Hydrologic Soil Group		Α	В	С	D
	Poor	72	81	88	91
Straight Row Crops	Good	67	68	85	89
	Poor	65	76	84	88
Small Grain – Straight Row Crops	Good	63	75	83	87
	Poor	68	79	86	89
Pasture, grassland, or range-	Fair	49	69	79	84
continuous forage for grazing	Good	39	61	74	80
Meadow		30	58	71	78
	Poor	48	67	77	83
Brush – brush-weeds-grass mixture,	Fair	35	56	70	77
with brush the major element	Good	30	48	65	73
	Poor	57	73	82	86
Woods – grass combination (orchard or	Fair	43	65	76	82
tree farm)	Good	32	58	72	79
	Poor	45	66	77	83
	Fair	36	60	73	79
Woods	Good	30	55	70	77
Farmsteads		59	74	82	86

Source: U.S. Department of Agriculture (USDA), Soil Conservation Service (SCS), 1986. Technical Release 55 (TR-55) Urban Hydrology for Small Watersheds.

Table A-6. Land Use Categories for Urban Areas

Land Use Description	Hydrologic Condition	Land Use ID
Open Space (lawns, parks, golf courses,	Poor (grass cover <50%)	1
cemeteries)	Fair (grass cover 50% to 75%)	2
	Good (grass cover >75%)	3
Commercial and Business	NA	10
Industrial	NA	20
Residential (1/8 acre or less, townhouses)	NA	30
Residential (1/4 acre)	NA	31
Residential (1 acre)	NA	33
Residential (2 acres)	NA	34
Newly graded areas (no vegetation, pervious	NA	40
area only)		
Highway	NA	99

Source: U.S. Department of Agriculture (USDA), Soil Conservation Service (SCS), 1986. Technical Release 55 (TR-55) Urban Hydrology for Small Watersheds.

Table A-7. Land Use Categories for Rural Areas

Land Use Cover Type	Hydrologic Condition	Land Use ID
Herbaceous: mixture of grass, weeds, and low-	Poor	50
growing brush, with brush the minor element	Fair	51
	Good	52
Oak-aspen: mountain brush mixture of oak	Poor	60
brush, aspen, mountain mahogany, bitter brush,	Fair	61
maple, and other brush	Good	62
Pinyon-juniper: pinyon, juniper, or both: grass	Poor	70
understory	Fair	71
	Good	72
Sagebrush with grass understory	Poor	80
	Fair	81
	Good	82
Desert shrub: major plants include saltbush,	Poor	90
greasewood, creosote brush, black brush,	Fair	91
bursage, palo verde, mesquite, and cactus	Good	92

Source: U.S. Department of Agriculture (USDA), Soil Conservation Service (SCS), 1986. Technical Release 55 (TR-55) Urban Hydrology for Small Watersheds.

Table A-8. Curve Number Summary for Vinton Study Area

Watershed Name	Basin ID	Watershed Area (mi²)	Weighted Curve Number
Flow Path Number 43	FPN43_1	105.97	84
Flow Path Number 44	FPN44_1	8.87	70
Flow Path Number 44	FPN44_2	5.81	83
Flow Path Number 44	FPN44_3	178.82	84

Table A-9. Curve Number Summary for Canutillo Study Area

Watershed Name	Basin ID	Watershed Area (mi²)	Weighted Curve Number
First Ave. Channel	FAC_1	31.78	78
Flow Path Number 42	FPN42_1	11.49	68
Flow Path Number 42	FPN42_2	10.88	78
Flow Path Number 42	FPN42_3	163.21	84
Flow Path Number 42A	FPN42A_1	1.12	88
Flow Path Number 42B	FPN42B_1	8.58	85
Flow Path Number 42C	FPN42C_1	22.38	85
Flow Path Number 42D	FPN42D_1	6.37	85

Table A-10. Curve Number Summary for Socorro Study Area

Watershed Name	Watershed Area (mi²)	Weighted Curve Number
A_Mesa Spur 4-1	0.45	63
A_Mesa Spur 4-2	0.11	61
A_Mesa Spur 5.5-1	0.91	63
A_Mesa Spur 5.5-2	0.32	58
A_Mesa Spur 5-1	0.08	68
A_Stream 4-1	0.21	66
A_Stream 4-2	0.44	60
A_Stream 4-2b	0.03	64
A_Stream 4-3A	1.93	76
A_Stream 4-3B	0.65	63
A_Stream 5.5-1	0.09	65
A_Stream 5.5-2	1.34	59
A_Stream 5-1	0.18	62
A_Stream 5-2	0.78	59
A_Stream 5-2a	0.11	62

Table A-11. Curve Number Summary for Hacienda Real Study Area

Watershed Area	WILLIAM N. I
	Weighted Curve Number
	79
	85
	77
	75
	62
1	67
	65
0.63	62
0.42	65
0.64	61
0.27	64
1.99	59
0.08	58
0.06	57
0.41	57
0.11	55
0.16	57
0.87	68
0.03	64
0.38	59
0.24	56
0.46	57
0.04	64
0.53	55
5.67	80
0.49	63
0.02	65
0.38	57
	64
	56
	57
	64
	58
1	78
	57
1	57
	68
<u> </u>	57
	55
	(mi²) 0.11 0.32 0.27 0.28 1.82 0.18 0.51 0.63 0.42 0.64 0.27 1.99 0.08 0.06 0.41 0.11 0.16 0.87 0.03 0.38 0.24 0.46 0.04 0.53 5.67 0.49

Table A-12. Curve Number Summary for Fabens Study Area

Watershed Name	Basin ID	Watershed Area (mi²)	Weighted Curve Number
Fabens North 1	FN1_1	4.08	49
Fabens North 1	FN1_2	8.60	53
Fabens North 1	FN1_3	19.26	52
Fabens North 2	FN2_1	9.34	53
Fabens North 2	FN2_2	21.87	49
Fabens North 2 Trib 1	FN2T1_1	23.35	52
San Felipe Arroyo	SFA_1	60.07	59
San Felipe Arroyo	SFA_FL1	404.75	54
San Felipe Arroyo	SFA_FL2	59.34	52
San Felipe Arroyo	SFA_PDB	158.66	60
San Felipe Arroyo	SFA_RSL	79.31	59
San Felipe Arroyo	SFA_RT	89.43	64
San Felipe Arroyo Trib 1	SFAT1_1	118.22	63
San Felipe Arroyo Trib 1	SFAT1_D6	608.90	77

Table A-13. Curve Number Summary for Tornillo Study Area

Watershed Name	Basin ID	Watershed Area (mi ²)	Weighted Curve Number
Flow Path T	FPT_1	22.15	51
Flow Path T	FPT_2	26.67	61
High School Channel	HSC_1	4.28	56
High School Channel	HSC_2	17.86	49
High School Channel	HSC_3	16.56	58
High School Channel Trib 1	HSCT1_1	6.48	55
High School Channel Trib 1	HSCT1_2	17.34	67
High School Channel Trib 2	HSCT2_1	7.00	53
South High School Channel 1	SHSC_1	12.35	49
Tornillo Handle Channel 1	THC1_1	7.80	49
Tornillo Handle Channel 2	THC2_1	6.55	51
Tornillo Handle Channel 2	THC2_2	23.91	51

Table A-14. Curve Number Summary for Montana Sector Study Area

	Watershed Area	
Basin ID	(mi²)	Weighted Curve Number
SUB_A01	11.20	86
SUB_A02	10.29	83
SUB_A03	0.53	82
SUB_A04	1.76	74
SUB_A05	4.55	76
SUB_A06	0.79	81
SUB_B01	2.69	83
SUB_B02	0.32	88
SUB_B03	0.23	82
SUB_B04	0.10	73
SUB_B05	0.38	77
SUB_B06	0.23	75
SUB_B07	0.36	81
SUB_B08	0.39	72
SUB_B09	1.22	75
SUB_B10	2.80	75
SUB_B11	1.50	77
SUB_B12	3.70	75
SUB_B13	2.70	76
SUB_C01	3.55	85
SUB_C02	3.40	85
SUB_C03	4.88	85
SUB_C04	0.73	78
SUB_C05	0.43	77
SUB_C06	0.75	82
SUB_C07	0.25	77
SUB_C08	0.97	75
SUB_C09	0.47	72
SUB C10	1.42	74
SUB_C11	3.59	78
SUB_D01	4.59	85
SUB D02	4.68	81
SUB_D03	0.86	78
SUB_E01	0.28	80
SUB_E02	2.76	78
SUB E03	1.48	85
SUB_E04	0.48	79
SUB_E05	0.24	76
SUB_E06	0.20	75
SUB_E07	0.22	79
SUB_E08	0.49	78
SUB_F01	2.03	85

Table A-14. Curve Number Summary for Montana Sector Study Area (Continued)

Basin ID	Watershed Area (mi²)	Weighted Curve Number
SUB F02	0.87	80
SUB F03	0.79	84
SUB_F04	1.05	79
SUB F05	0.48	83
SUB F06	0.89	85
SUB F07	0.39	79
SUB F08	0.53	81
SUB F09	2.69	81
SUB F10	0.39	82
SUB_G01	1.07	81
SUB_G02	1.00	76
SUB_G03	1.77	81
SUB_G04	0.75	84
SUB_G05	1.66	83
SUB_G06	2.66	76
SUB_H01	1.49	80
SUB_H02	1.09	81
SUB_H03	0.45	83
SUB_H04	0.34	73
SUB_H05	0.16	82
SUB_H06	0.32	86
SUB_H07	0.28	83
SUB_H08	0.96	79
SUB_H09	0.46	76
SUB_I01	1.36	81
SUB_J01	1.73	81
SUB_J02	0.30	80
SUB_K01	4.44	74
SUB_K02	2.68	78
SUB_K03	0.71	80
SUB_K04	1.90	81
SUB_K05	1.15	81

Table A-15. Summary of Lag Times for the Vinton Study Area

Watershad Name	rehad Namo		L	L _{CA}		C _T	N	T _{lag}	T _{lag}	C _P
Watershed Name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
Flow Path Number 43	19909	3.77	9683	1.83	0.031	0.490	0.3	0.88	52.5	0.6125
Flow Path Number 44	5983	1.13	3012	0.57	0.018	0.275	0.3	0.24	14.5	0.6125
Flow Path Number 44	4692	0.89	2311	0.44	0.024	0.530	0.3	0.40	24.0	0.6125
Flow Path Number 44	30564	5.79	14858	2.81	0.035	0.470	0.3	1.09	65.1	0.6125

Table A-16. Summary of Lag Times for Canutillo Study Area

Watershad Name	L	L _L		CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
Watershed Name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
First Ave. Channel	6914	1.31	3575	0.68	0.021	0.265	0.3	0.26	15.3	0.6125
Flow Path Number 42	6792	1.29	3609	0.68	0.025	0.260	0.3	0.25	15.0	0.6125
Flow Path Number 42	4533	0.86	2257	0.43	0.027	0.510	0.3	0.38	22.7	0.6125
Flow Path Number 42	25349	4.80	12775	2.42	0.029	0.500	0.3	1.04	62.6	0.6125
Flow Path Number 42A	1210	0.23	560	0.11	0.044	0.440	0.3	0.14	8.7	0.6125
Flow Path Number 42B	4046	0.77	2020	0.38	0.028	0.500	0.3	0.35	20.8	0.6125
Flow Path Number 42C	11359	2.15	5880	1.11	0.024	0.530	0.3	0.69	41.3	0.6125
Flow Path Number 42D	4889	0.93	2572	0.49	0.025	0.520	0.3	0.41	24.6	0.6125

Table A-17. Summary of Lag Times Socorro Study Area

Meterohed Nome	L	L	L	-CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
Watershed Name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
A_Mesa Spur 4-1	8122	1.54	5181	0.98	0.022	0.540	0.3	0.61	36.7	0.6125
A_Mesa Spur 4-2	4829	0.91	2150	0.41	0.029	0.250	0.3	0.19	11.2	0.6125
A_Mesa Spur 5.5-1	11068	2.10	7845	1.49	0.015	0.610	0.3	0.86	51.5	0.6719
A_Mesa Spur 5.5-2	4287	0.81	2257	0.43	0.039	0.460	0.3	0.33	20.1	0.6125
A_Mesa Spur 5-1	4136	0.78	2119	0.40	0.027	0.510	0.3	0.36	21.6	0.6125
A_Stream 4-1	4688	0.89	2268	0.43	0.030	0.490	0.3	0.37	22.0	0.6125
A_Stream 4-2	7265	1.38	2481	0.47	0.027	0.255	0.3	0.22	13.4	0.6125
A_Stream 4-2b	1502	0.28	561	0.11	0.043	0.450	0.3	0.16	9.4	0.6125
A_Stream 4-3A	20326	3.85	8792	1.67	0.010	0.690	0.3	1.20	72.3	0.6719
A_Stream 4-3B	10047	1.90	5942	1.13	0.022	0.540	0.3	0.68	40.7	0.6125
A_Stream 5.5-1	4662	0.88	2348	0.44	0.025	0.520	0.3	0.39	23.6	0.6125
A_Stream 5.5-2	12477	2.36	5543	1.05	0.022	0.540	0.3	0.71	42.6	0.6125
A_Stream 5-1	4663	0.88	2489	0.47	0.031	0.495	0.3	0.38	22.8	0.6125
A_Stream 5-2	12173	2.31	5439	1.03	0.022	0.540	0.3	0.70	42.0	0.6125
A_Stream 5-2a	4470	0.85	1842	0.35	0.030	0.490	0.3	0.34	20.4	0.6125

Table A-18. Summary of Lag Times for Hacienda Real Study Area

Watershed Name	L	L	L	CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
watersned Name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
A_Clint Landfill A	2939	0.56	1471	0.28	0.024	0.525	0.3	0.30	18.0	0.6125
A_Clint Landfill B	5873	1.11	3177	0.60	0.021	0.550	0.3	0.49	29.3	0.6125
A_Clint Landfill C	4950	0.94	2495	0.47	0.020	0.560	1.3	0.19	11.7	0.6125
A_Clint Landfill D	4463	0.85	1962	0.37	0.021	0.550	2.3	0.04	2.3	0.6125
A_Hacienda Real-1	16806	3.18	8326	1.58	0.020	0.560	0.3	0.91	54.5	0.6125
A_Hacienda Real-2	4765	0.90	2470	0.47	0.001	1.700	0.3	1.31	78.8	0.6719
A_Hacienda Real-3	14210	2.69	9675	1.83	0.008	0.750	0.3	1.21	72.6	0.6719
A_Hacienda Real-4	11775	2.23	5365	1.02	0.020	0.560	0.3	0.72	42.9	0.6125
A_Hacienda Real-5	8969	1.70	5074	0.96	0.010	0.700	0.3	0.81	48.7	0.6719
A_Hacienda Real-6	11804	2.24	5497	1.04	0.019	0.565	0.3	0.73	43.7	0.6125
A_Hacienda Real-7	5959	1.13	2549	0.48	0.013	0.640	0.3	0.53	32.0	0.6719
A_Hacienda Real-8	18689	3.54	11393	2.16	0.013	0.640	0.3	1.18	70.7	0.6719
A_Stream 10-1	4247	0.80	2455	0.46	0.031	0.490	0.3	0.36	21.9	0.6125
A_Stream 10-2	1887	0.36	783	0.15	0.036	0.470	0.3	0.19	11.7	0.6125
A_Stream 11-1	7555	1.43	3987	0.76	0.030	0.495	0.3	0.51	30.4	0.6125
A_Stream 11-2	4900	0.93	2520	0.48	0.023	0.530	0.3	0.42	24.9	0.6125
A_Stream 12-1	6032	1.14	9564	1.81	0.022	0.540	0.3	0.67	40.3	0.6125
A_Stream 12-2	18863	3.57	3066	0.58	0.018	0.570	0.3	0.71	42.6	0.6125
A_Stream 12-3	1819	0.34	1022	0.19	0.029	0.500	0.3	0.22	13.3	0.6125
A_Stream 12-4	7375	1.40	3857	0.73	0.028	0.505	0.3	0.51	30.5	0.6125
A_Stream 13.5-1-a	7338	1.39	3021	0.57	0.021	0.550	0.3	0.51	30.8	0.6125
A_Stream 13.5-1b	8680	1.64	4402	0.83	0.024	0.525	0.3	0.58	34.6	0.6125
A_Stream 13.5-2	2253	0.43	982	0.19	0.019	0.565	0.3	0.26	15.9	0.6125
A_Stream 13.5-3	6120	1.16	2735	0.52	0.026	0.510	0.3	0.44	26.3	0.6125
A_Stream 13.5-4a	37156	7.04	22279	4.22	0.003	1.050	0.3	2.90	174.2	0.6719
A_Stream 13.5-4b	6248	1.18	2816	0.53	0.020	0.560	0.3	0.49	29.3	0.6125
A_Stream 13-1	2070	0.39	1145	0.22	0.023	0.530	0.3	0.25	15.2	0.6125
A_Stream 13-2	6198	1.17	3797	0.72	0.031	0.490	0.3	0.47	27.9	0.6125
A_Stream 6-1	7022	1.33	3330	0.63	0.028	0.505	0.3	0.48	28.7	0.6125

Table A-18. Summary of Lag Times for Hacienda Real Study Area (Continued)

Watershed Name	L	·L	L	CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
watersned name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
A_Stream 6-2	8007	1.52	3801	0.72	0.025	0.520	0.3	0.53	32.0	0.6125
A_Stream 7-1	6733	1.28	2969	0.56	0.025	0.520	0.3	0.47	28.2	0.6125
A_Stream 7-2	3070	0.58	1364	0.26	0.022	0.540	0.3	0.31	18.3	0.6125
A_Stream 7-3	7567	1.43	2537	0.48	0.024	0.525	0.3	0.47	28.2	0.6125
A_Stream 7-4	26014	4.93	10648	2.02	0.006	0.820	0.3	1.63	98.0	0.6719
A_Stream 8-1	2262	0.43	779	0.15	0.018	0.570	0.3	0.25	14.9	0.6125
A_Stream 8-2	5961	1.13	2757	0.52	0.029	0.500	0.3	0.43	25.6	0.6125
A_Stream 8-3	13250	2.51	6915	1.31	0.017	0.585	0.3	0.84	50.2	0.6125
A_Stream 9-1	6181	1.17	2853	0.54	0.026	0.510	0.3	0.44	26.7	0.6125
A_Stream 9-2	3768	0.71	1871	0.35	0.031	0.490	0.3	0.32	19.5	0.6125

Table A-19. Summary of Lag Times for Fabens Study Area

	L	L	L	CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
Watershed Name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
Fabens North 1	3436	0.65	1888	0.36	0.023	0.530	0.3	0.34	20.5	0.6125
Fabens North 1	5362	1.02	2646	0.50	0.026	0.510	0.3	0.42	25.0	0.6125
Fabens North 1	8032	1.52	3255	0.62	0.020	0.560	0.3	0.55	33.0	0.6125
Fabens North 2	6105	1.16	2340	0.44	0.019	0.570	0.3	0.47	28.0	0.6125
Fabens North 2	7371	1.40	3857	0.73	0.021	0.550	0.3	0.55	33.2	0.6125
Fabens North 2 Trib 1	9830	1.86	4952	0.94	0.019	0.570	0.3	0.67	40.4	0.6125
San Felipe Arroyo	16231	3.07	7937	1.50	0.010	0.700	0.3	1.11	66.5	0.6719
San Felipe Arroyo	33343	6.31	17389	3.29	0.011	0.670	0.3	1.67	99.9	0.6719
San Felipe Arroyo	17144	3.25	8388	1.59	0.009	0.720	0.3	1.18	70.7	0.6719
San Felipe Arroyo	15508	2.94	7966	1.51	0.010	0.700	0.3	1.09	65.6	0.6719
San Felipe Arroyo	11715	2.22	4766	0.90	0.011	0.670	0.3	0.83	49.5	0.6719
San Felipe Arroyo	12548	2.38	5985	1.13	0.012	0.660	0.3	0.89	53.3	0.6719
San Felipe Arroyo Trib 1	21025	3.98	8531	1.62	0.012	0.660	0.3	1.15	69.2	0.6719
San Felipe Arroyo Trib 1	47034	8.91	26287	4.98	0.006	0.820	0.3	2.56	153.5	0.6719

Table A-20. Summary of Lag Times for Tornillo Study Area

Watershed Name	L	L	L	-CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
watersned Name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
Flow Path T	11222	2.13	6067	1.15	0.016	0.600	0.3	0.78	47.1	0.6125
Flow Path T	6874	1.30	3173	0.60	0.017	0.590	0.3	0.55	32.9	0.6125
High School Channel	4399	0.83	2131	0.40	0.015	0.610	0.3	0.44	26.4	0.6719
High School Channel	10172	1.93	5309	1.01	0.016	0.600	0.3	0.73	43.9	0.6125
High School Channel	9319	1.77	4998	0.95	0.018	0.580	0.3	0.68	40.6	0.6125
High School Channel Trib 1	3376	0.64	1631	0.31	0.015	0.610	0.3	0.37	22.5	0.6719
High School Channel Trib 1	7719	1.46	3911	0.74	0.014	0.620	0.3	0.63	38.1	0.6719
High School Channel Trib 2	5302	1.00	2581	0.49	0.022	0.540	0.3	0.44	26.2	0.6125
South High School Channel	7165	1.36	3578	0.68	0.020	0.560	0.3	0.55	32.8	0.6125
Tornillo Handle Channel 1	5913	1.12	3020	0.57	0.018	0.580	0.3	0.51	30.4	0.6125
Tornillo Handle Channel 2	6346	1.20	3625	0.69	0.017	0.590	0.3	0.56	33.4	0.6125
Tornillo Handle Channel 2	10393	1.97	5058	0.96	0.017	0.590	0.3	0.71	42.8	0.6125

Table A-21. Summary of Lag Times for Montana Sector Study Area

Watershed Name	L	L	L	CA	S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
watersned name	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
SUB_A01	29751	5.63	11400	2.16	0.023	0.530	0.3	1.12	67.3	0.6125
SUB_A02	35888	6.80	16500	3.12	0.026	0.515	0.3	1.29	77.3	0.6125
SUB_A03	8399	1.59	4703	0.89	0.075	0.380	0.3	0.42	25.3	0.6125
SUB_A04	17231	3.26	5166	0.98	0.014	0.620	0.3	0.88	52.7	0.6719
SUB_A05	25581	4.84	12541	2.38	0.032	0.485	0.3	1.01	60.6	0.6125
SUB_A06	13150	2.49	2512	0.48	0.052	0.420	0.3	0.44	26.5	0.6125
SUB_B01	14869	2.82	4612	0.87	0.055	0.410	0.3	0.54	32.2	0.6125
SUB_B02	4419	0.84	1643	0.31	0.016	0.600	0.3	0.40	24.0	0.6125
SUB_B03	7212	1.37	2743	0.52	0.017	0.590	0.3	0.53	31.9	0.6125
SUB_B04	2770	0.52	1280	0.24	0.029	0.500	0.3	0.27	16.2	0.6125
SUB_B05	7741	1.47	4277	0.81	0.013	0.630	0.3	0.66	39.8	0.6719
SUB_B06	3898	0.74	1161	0.22	0.016	0.600	0.3	0.35	20.9	0.6125
SUB_B07	7124	1.35	3169	0.60	0.017	0.590	0.3	0.55	33.2	0.6125
SUB_B08	5384	1.02	2598	0.49	0.015	0.610	0.3	0.50	29.8	0.6125
SUB_B09	24659	4.67	6171	1.17	0.017	0.590	0.3	0.98	58.9	0.6125
SUB_B10	20112	3.81	6011	1.14	0.012	0.655	0.3	1.02	61.0	0.6719
SUB_B11	13727	2.60	4049	0.77	0.015	0.610	0.3	0.75	45.0	0.6719
SUB_B12	27052	5.12	12154	2.30	0.017	0.590	0.3	1.24	74.2	0.6125
SUB_B13	22230	4.21	12872	2.44	0.014	0.620	0.3	1.25	74.8	0.6719
SUB_C01	17543	3.32	8660	1.64	0.037	0.470	0.3	0.78	46.9	0.6125
SUB_C02	16076	3.04	9933	1.88	0.058	0.404	0.3	0.68	40.9	0.6125
SUB_C03	23731	4.49	12413	2.35	0.023	0.530	0.3	1.08	64.5	0.6125
SUB_C04	14585	2.76	9237	1.75	0.031	0.490	0.3	0.79	47.2	0.6125
SUB_C05	14467	2.74	7518	1.42	0.014	0.620	0.3	0.93	56.0	0.6719
SUB_C06	13479	2.55	8032	1.52	0.053	0.415	0.3	0.62	37.4	0.6125
SUB_C07	9436	1.79	4312	0.82	0.064	0.390	0.3	0.44	26.2	0.6125
SUB_C08	9405	1.78	2098	0.40	0.014	0.610	0.3	0.55	33.0	0.6719
SUB_C09	8521	1.61	4556	0.86	0.015	0.610	0.3	0.67	40.4	0.6719
SUB_C10	11605	2.20	5102	0.97	0.015	0.610	0.3	0.76	45.9	0.6719

Table A-21. Summary of Lag Times for Montana Sector Study Area (Continued)

Watershed Name	LL		L _{CA}		S _{ST}	Ст	N	T _{lag}	T _{lag}	C _P
	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
SUB_C11	14034	2.66	3693	0.70	0.047	0.430	0.3	0.52	31.1	0.6125
SUB_D01	25006	4.74	6414	1.21	0.024	0.520	0.3	0.88	52.7	0.6125
SUB_D02	20980	3.97	10462	1.98	0.021	0.550	0.3	1.02	61.3	0.6125
SUB_D03	6561	1.24	3005	0.57	0.035	0.480	0.3	0.43	26.0	0.6125
SUB_E01	8138	1.54	3933	0.74	0.053	0.415	0.3	0.43	26.0	0.6125
SUB_E02	15854	3.00	4193	0.79	0.032	0.485	0.3	0.63	37.8	0.6125
SUB_E03	12267	2.32	6516	1.23	0.021	0.550	0.3	0.75	45.3	0.6125
SUB_E04	5429	1.03	2336	0.44	0.073	0.385	0.3	0.30	18.2	0.6125
SUB_E05	6702	1.27	856	0.16	0.057	0.405	0.3	0.25	15.1	0.6125
SUB_E06	7753	1.47	1919	0.36	0.015	0.610	0.3	0.51	30.3	0.6719
SUB_E07	6580	1.25	1201	0.23	0.098	0.350	0.3	0.24	14.4	0.6125
SUB_E08	10118	1.92	2218	0.42	0.015	0.610	0.3	0.57	34.3	0.6719
SUB_F01	11851	2.24	2680	0.51	0.043	0.445	0.3	0.46	27.8	0.6125
SUB_F02	9575	1.81	4908	0.93	0.078	0.375	0.3	0.44	26.3	0.6125
SUB_F03	5600	1.06	2599	0.49	0.093	0.360	0.3	0.30	17.8	0.6125
SUB_F04	7551	1.43	4467	0.85	0.109	0.345	0.3	0.37	21.9	0.6125
SUB_F05	8113	1.54	4664	0.88	0.109	0.345	0.3	0.38	22.7	0.6125
SUB_F06	8008	1.52	4105	0.78	0.088	0.369	0.3	0.39	23.3	0.6125
SUB_F07	8793	1.67	4972	0.94	0.044	0.440	0.3	0.50	30.2	0.6125
SUB_F08	10837	2.05	6194	1.17	0.019	0.565	0.3	0.74	44.1	0.6125
SUB_F09	19509	3.69	8142	1.54	0.033	0.484	0.3	0.82	48.9	0.6125
SUB_F10	9397	1.78	4771	0.90	0.017	0.590	0.3	0.68	40.8	0.6125
SUB_G01	14225	2.69	6445	1.22	0.047	0.430	0.3	0.61	36.9	0.6125
SUB_G02	14698	2.78	11062	2.10	0.040	0.460	0.3	0.78	46.8	0.6125
SUB_G03	15101	2.86	7150	1.35	0.037	0.470	0.3	0.71	42.3	0.6125
SUB_G04	9222	1.75	5786	1.10	0.024	0.520	0.3	0.63	37.9	0.6125
SUB_G05	13823	2.62	8711	1.65	0.057	0.405	0.3	0.63	37.7	0.6125

Table A-21. Summary of Lag Times for Montana Sector Study Area (Continued)

Watershed Name	LL		L _{CA}		S _{ST}	C _T	N	T _{lag}	T _{lag}	C _P
	(ft)	(mile)	(ft)	(mile)	(ft/ft)	(-)	(-)	(hr)	(min)	(-)
SUB_G06	21329	4.04	3542	0.67	0.007	0.790	0.3	1.07	63.9	0.6719
SUB_H01	19316	3.66	10050	1.90	0.041	0.455	0.3	0.81	48.9	0.6125
SUB_H02	14795	2.80	11873	2.25	0.037	0.470	0.3	0.82	49.0	0.6125
SUB_H03	8130	1.54	4557	0.86	0.074	0.383	0.3	0.42	25.0	0.6125
SUB_H04	9955	1.89	4583	0.87	0.017	0.590	0.3	0.68	41.0	0.6125
SUB_H05	6357	1.20	3146	0.60	0.059	0.402	0.3	0.36	21.8	0.6125
SUB_H06	7617	1.44	4997	0.95	0.088	0.369	0.3	0.41	24.3	0.6125
SUB_H07	6162	1.17	2615	0.50	0.086	0.370	0.3	0.31	18.8	0.6125
SUB_H08	9789	1.85	4136	0.78	0.043	0.445	0.3	0.50	29.9	0.6125
SUB_H09	7899	1.50	2982	0.56	0.024	0.520	0.3	0.49	29.7	0.6125
SUB_I01	9100	1.72	3093	0.59	0.006	0.830	0.3	0.83	49.9	0.6719
SUB_J01	12143	2.30	4863	0.92	0.048	0.425	0.3	0.53	31.9	0.6125
SUB_J02	5895	1.12	3073	0.58	0.007	0.790	0.3	0.69	41.6	0.6719
SUB_K01	12229	2.32	3791	0.72	0.057	0.405	0.3	0.47	28.3	0.6125
SUB_K02	15396	2.92	7575	1.43	0.037	0.470	0.3	0.72	43.3	0.6125
SUB_K03	8213	1.56	3059	0.58	0.003	1.050	0.3	1.02	61.1	0.6719
SUB_K04	14509	2.75	7466	1.41	0.005	0.870	0.3	1.31	78.4	0.6719
SUB_K05	13096	2.48	6400	1.21	0.005	0.870	0.3	1.21	72.6	0.6719

Table A-22. Muskingum-Cunge Routing Inputs for Vinton Study Area

	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Trapezoid		Eight Point	
Reach Name							Bottom Width (ft)	Side Slope (xH:1V)	X	Y
									0	3807
R_FPN44_1 J_FPN44_FF	J_FPN44_FPN43	S_FPN44			0.013 0.030 Eight Pt. N/A				14	3803
									19	3801
			707	0.013		N/A	28	3801		
				0.0.0		Pt.			34	3801
									38	3803
									56	3805
									65	3806
R_FPN44_2	A_FPN44_3								0	3912
									7	3912
									227	3909
		J_FPN44_2	4246	0.005	0.043	Eight	N/A	N/A	228	3907
			4316	0.025	0.043	Pt.	N/A	N/A	295	3907
									297	3909
									363	3912
									383	3913

Table A-23. Muskingum-Cunge Routing Inputs for Canutillo Study Area

Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	Х	Y
									0	3810
									23	3804
									32	3795
R_FPN42_1	J_FPN42_2	S_FPN42_1	3191	0.011	0.030	Eight Pt.	N/A	N/A	48	3795
	J_111N 4 Z_Z	0_111142_1	3131	0.011	0.030	Light i t.	IN/A	IN//	52	3801
									81	3804
									89	3807
									102	3808
									0	3846
									168	3843
									198	3840
R_FPN42_2	J FPN42A,3	J_FPN42_2	3200	0.021	0.030	Eight Pt.	N/A	N/A	207	3834
	, , ,					3			241	3831
									259	3840
									273	3843
									338	3844
									0	3900
									51 74	3897
									71	3885
R FPN42A 1		I EDNI42A	1046	0.023	0.030	Eight Dt	N/A	N/A	81 98	3883 3883
K_FPIN4ZA_I	J_FPN42B,C,D	J_FPN42A	1046	0.023	0.030	Eight Pt.	IN/A	IN/A	98 102	
									102	3885 3894
									130	3898
İ									104	3916

Table A-23. Muskingum-Cunge Routing Inputs for Canutillo Study Area (Continued)

Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	х	Y
									0	3914
									32	3912
									43	3906
R_FPN42C_1	A_FPN42D_1	J_FPN42D_C	1096	0.016	0.030	Eight Pt.	N/A	N/A	49	3904
K_FFN42C_I	A_FFN42D_1	J_FFN42D_C	1090	0.016	0.030	Eight Pt.	IN/A	IN/A	61	3904
									64	3906
				78	3915					
									104	3916

Table A-24. Muskingum-Cunge Routing Inputs for Socorro Study Area

							Trape	zoid	Eight	Point
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	Х	Y
R_Mesa Drain 5.5	R_Mesa Spur 5.5 DS	J_AMS551_RMD55_OUT	1569.7	0.00154	0.05	Trapezoid	15	2	N/A	N/A
R_Mesa Spur 4	R_Mesa Spur 4-2	J_AMS41_RS4_RMS4_OUT	3709.8	5.5E-05	0.05	Trapezoid	10	1	N/A	N/A
R_Mesa Spur 4-2	A_Mesa Spur 4-2	R_Mesa Spur 4	3755	0.03572	0.03	Rectangle	40	N/A	N/A	N/A
R_Mesa Spur 5	R_Stream 5-1	J_AMS51_RMS5_OUT	425.32	5.5E-05	0.05	Trapezoid	10	1	N/A	N/A
R_Mesa Spur 5.5 DS	J_RMS55US_RS551	R_Mesa Drain 5.5	979.85	5.5E-05	0.05	Trapezoid	10	1	N/A	N/A
R_Mesa Spur 5.5 US	R_Mesa Spur 5.5-2	J_RMS55US_RS551	1673.2	5.5E-05	0.05	Trapezoid	10	1	N/A	N/A
R_Mesa Spur 5.5-2	A_Mesa Spur 5.5-2	R_Mesa Spur 5.5 US	5367.1	0.03132	0.03	Rectangle	40	N/A	N/A	N/A
R_Stream 4-1	J_AS41_RS42	J_AMS41_RS4_RMS4_OUT	1061.7	0.01484	0.03	Rectangle	40	N/A	N/A	N/A
R_Stream 4-2	J_AS42_RS43	J_AS41_RS42	4021.3	0.0279	0.03	Rectangle	90	N/A	N/A	N/A
R_Stream 4-2b	A_Stream 4-2b	J_AS41_RS42_RS42b	4030.1	0.03226	0.03	Rectangle	10	N/A	N/A	N/A
R_Stream 4-3	J_AS43A_AS43B	J_AS42_RS43	2805.9	0.0218	0.03	Rectangle	80	N/A	N/A	N/A
R_Stream 4-3	J_AS43A_AS43B	J_AS42_RS43	2805.9	0.0218	0.03	Rectangle	80	N/A	N/A	N/A
R_Stream 5.5-1	J_AS551_R552	J_RMS55US_RS551	1891.9	0.01455	0.03	Rectangle	40	N/A	N/A	N/A
R_Stream 5.5-1	J_AS551_R552	J_RMS55US_RS551	1891.9	0.01455	0.03	Rectangle	40	N/A	N/A	N/A
R_Stream 5.5-2	A_Stream 5.5-2	J_AS551_R552	4074	0.02947	0.03	Rectangle	50	N/A	N/A	N/A
R_Stream 5.5-2	A_Stream 5.5-2	J_AS551_R552	4074	0.02947	0.03	Rectangle	50	N/A	N/A	N/A
R_Stream 5-1	J_AS551_R552	R_Mesa Spur 5	811.76	0.05397	0.03	Rectangle	50	N/A	N/A	N/A
R_Stream 5-1	J_AS551_R552	R_Mesa Spur 5	811.76	0.05397	0.03	Rectangle	50	N/A	N/A	N/A
R_Stream 5-2	A_Stream 5-2	J_AS551_R552	4096.7	0.02682	0.03	Rectangle	60	N/A	N/A	N/A
R_Stream 5-2	A_Stream 5-2	J_AS551_R552_RS52a	4096.7	0.02682	0.03	Rectangle	60	N/A	N/A	N/A
R_Stream 5-2a	A_Stream 5-2a	J_AS551_R552_RS52a	4049.4	0.02698	0.03	Rectangle	10	N/A	N/A	N/A

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Table A-25. Muskingum-Cunge Routing Inputs for Hacienda Real Study Area

					<u>.</u>		Trape	zoid	Eight	Point
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	Х	Y
R_Clint Landfill A	A_Clint Landfill A	J_AS8-3	4454	0.028	0.030	Rectangle	50	N/A	N/A	N/A
R_Clint Landfill B	A_Clint Landfill B	J_AS9-2	2758	0.029	0.030	Rectangle	60	N/A	N/A	N/A
R_Clint Landfill C	A_Clint Landfill C	J_AS10-2	1287	0.043	0.030	Rectangle	200	N/A	N/A	N/A
R_Clint Landfill D	A_Clint Landfill D	J_A11-2	3411	0.030	0.030	Rectangle	100	N/A	N/A	N/A
R_Stream 10-2	J_AS10-2	J_AS10-2&AS9-1	4244	0.030	0.030	Rectangle	25	N/A	N/A	N/A
R_Stream 11-1	J_AS11-1	J_AHR6	5066	0.004	0.035	Rectangle	200	N/A	N/A	N/A
R_Stream 11-2	A_Stream 11-2	J_AS11-1	4990	0.029	0.030	Rectangle	30	N/A	N/A	N/A
R_Stream 12-1	J_AS12-1	J_AHR7	1018	0.001	0.040	Rectangle	200	N/A	N/A	N/A
R_Stream 12-2	J_AS12-2	J_AS12-1	3288	0.020	0.030	Rectangle	60	N/A	N/A	N/A
R_Stream 12-3 and Stream 13-1	J_AS12-3&AS13-1	J_AS12-2	1966	0.021	0.030	Rectangle	60	N/A	N/A	N/A
R_Stream 12-4	A_Stream 12-4	J_AS12-3&AS13-1	1670	0.031	0.030	Rectangle	40	N/A	N/A	N/A
R_Stream 13.5-1a	A_Stream 8-3	J_AS8-3	5406	0.003	0.040	Rectangle	200	N/A	N/A	N/A
R_Stream 13.5-1b	J_AS13.5-1b	J_AHR8	4823	0.007	0.040	Rectangle	200	N/A	N/A	N/A
R_Stream 13.5-2a	D_AS13.5-2	J_AS13.5-1a	5709	0.021	0.030	Rectangle	40	N/A	N/A	N/A
R_Stream 13.5-2b	D_AS13.5-3	J_AS13.5-1b	3712	0.026	0.030	Rectangle	60	N/A	N/A	N/A
R_Stream 13.5-3	J_AS13.5-3	D_AS13.5-2	1684	0.029	0.030	Rectangle	50	N/A	N/A	N/A
R_Stream 13.5-4	J_AS13.5-4a&AS13.5- 4b	J_AS13.5-3	3724	0.015	0.030	Rectangle	45	N/A	N/A	N/A
R_Stream 13-2	A_Stream 13-2	J_AS12-2&AS13-1	1788	0.033	0.030	Rectangle	35	N/A	N/A	N/A
R_Stream 6-1	J_AS6-1	J_AHR2	4564	0.006	0.04	Rectangle	200	N/A	N/A	N/A
R_Stream 6-2	J_AS6-2	J_AS6-1	4711	0.026	0.03	Rectangle	200	N/A	N/A	N/A
R_Stream 7-1	J_AS7-1	J_AHR3	4501	0.002	0.035	Rectangle	200	N/A	N/A	N/A
R_Stream 7-2	J_AS7-2	J_AS7-1	3754	0.026	0.03	Rectangle	75	N/A	N/A	N/A
R_Stream 7-3	J_AS7-3	J_AS7-2	2381	0.021	0.03	Rectangle	90	N/A	N/A	N/A
R_Stream 7-4	A_Stream 7-4	 J_AS7-3	4157	0.012	0.03	Rectangle	90	N/A	N/A	N/A
R_Stream 8-1	J_AS8-1	J_AHR4	3359	0.004	0.04	Rectangle	200	N/A	N/A	N/A
R_Stream 8-2	J_AS8-2	J_AS8-1	1886	0.033	0.03	Rectangle	25	N/A	N/A	N/A

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Table A-25. Muskingum-Cunge Routing Inputs for Hacienda Real Study Area (Continued)

		Channel		01		Trape	zoid	Eight Point		
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	X	Y
R_Stream 8-2	J_AS8-2	J_AS8-1	1886	0.033	0.03	Rectangle	25	N/A	N/A	N/A
R_Stream 8-3	J_AS8-3	J_AS8-2	3252	0.025	0.03	Rectangle	50	N/A	N/A	N/A
R_Stream 9-1 and Stream 10-1	J_AS10-2&AS9-1	J_AHR5	6183	0.005	0.04	Rectangle	200	N/A	N/A	N/A
R_Stream 9-2	J_AS9-2	J_AS10-2&AS9-1	4666	0.026	0.03	Rectangle	45	N/A	N/A	N/A

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Table A-26. Muskingum-Cunge Routing Inputs for the Fabens Study Area

					01 1		Trape	zoid	Eight Point	
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	х	Y
									0	3669
									97	3666
									482	3660
R_FN1_1	J_FN1_2,3	S_FN1_1	2181	0.022	0.040	Eight Pt.	N/A	N/A	493	3657
K_FINI_I	J_FN1_2,3	S_FINI_1	2101	0.022	0.040	Eight Ft.	IN/A	IN/A	518	3657
									528	3660
									568	3663
									657	3671
									0	3744
					150	3738				
								N/A	413	3729
R_FN1_2	A_FN1_3	J_FN1_2	4481	0.024	0.043	Eight Pt.	N/A		456	3728
1_1\1\1_2	/	0_1111_2	1401	0.024	0.040	Lighti	14/7		515	3728
									560	3729
									772	3732
									933	3741
									0	3738
									252	3732
					254	3731				
R_FN2_1	J_FN2T1_1,FN2_2	J_FN2_1	4832	0.019	0.040	Eight Pt.	N/A	N/A	326	3731
'_' \		<u> </u>		0.0.0	0.0.0	g	1 4/7 1	1 1// 1	328	3732
									497	3735
									567	3738
									597	3739

Table A-26. Muskingum-Cunge Routing Inputs for the Fabens Study Area (Continued)

					01 1		Trape	zoid	Eight	Point
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	X	Y
									0	3630
									15	3633
									17	3633
R_SFA_1	S_SFA_FL1	S_SFA_1	13536	0.007	0.043	Eight Pt.	N/A	N/A	23	3630
K_SFA_1	3_3FA_FLI	3_3FA_1	13330	0.007	0.043	Eight Ft.	IN/A	IN/A	29	3627
									59	3627
									66	3630
									89	3630
									0	3783
								N/A	181	3771
									533	3765
R_SFA_FL1	J_SFA_FL_2,SFAT1	S_SFA_FL1	16463	0.005	0.040	Eight Pt.	N/A		574	3763
11_017_121	0_01 /(_1 L_2,01 /(1 1	0_017(_121	10400	0.000	0.040				610	3763
									654	3765
									786	3768
									973	3775
									0	3819
									107	3813
									277	3810
R_SFA_FL2	S_SFA_RSL	J_SFA_FL2	4203	0.006	0.045	Eight Pt.	N/A	N/A	342	3808
R_SFA_FL2									385	3808
									402	3810
									487	3813
									755	3820

Table A-26. Muskingum-Cunge Routing Inputs for the Fabens Study Area (Continued)

							Trape	zoid	Eight	Point
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	х	Y
									0	3864
									188	3852
									377	3849
R_SFA_RSL	S_SFA_PDB	S_SFA_RSL	7351	0.005	0.045	Eight Pt.	N/A	N/A	412	3848
						, o			488	3848
									503 725	3849 3852
									985	3858
									0	3915
									141	3909
									395	3903
									416	3902
R_SFA_PDB	S_SFA_RT	S_SFA_PDB	7683	0.009	0.040	Eight Pt.	N/A	N/A	451	3902
									458	3903
									592	3906
									841	3918
									0	3825
									95	3822
									152	3819
		J_SFA_FL2,							201	3816
R_SFAT1_1	S_SFAT1_D6	SFAT1	2318	0.008	0.030	Eight Pt.	N/A	N/A	222	3807
									239	3807
									266	3813
									288	3816

Table A-27. Muskingum-Cunge Routing Inputs for Tornillo Study Area

					Channel		Trape	zoid	Eight Point	
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	х	Υ
									0	3768
									130	3765
									231	3762
R_FPT_1	A_FPT_2	S_FPT_1	11222	0.017	0.040	Eight Pt.	N/A	N/A	266	3761
K_FFI_I	A_FF1_2	S_FF1_1	11222	0.017	0.040	Eight Ft.	IN/A	IN/A	324	3761
									344	3762
									434	3765
									584	3768
									0	3649
									166	3648
									368	3645
R_HSC_1	J_HSC_2,SHSC_1	S_HSC_1	710	0.021	0.035	Eight Pt.	N/A	N/A	391	3644
11.100_1	0_1100_2,01100_1	0_1100_1	710	0.021	0.000	Ligiter ti	14// (14/7	410	3644
									431	3645
									645	3646
									820	3648
									0	3729
									190	3723
									368	3720
R_HSC_2	J_HSC_3,HSCT1	J_HSC_2	7746	0.015	0.040	Eight Pt.	N/A	N/A	387	3719
				2.0.3	3.3.3		,, .		460	3719
									474	3720
									602	3723
									684	3726

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Table A-27. Muskingum-Cunge Routing Inputs for Tornillo Study Area (Continued)

					01 1		Trape	zoid	Eight	Point
Reach Name	From Element	To Element	Length (ft)	Slope (ft/ft)	Channel Manning's n	Shape	Bottom Width (ft)	Side Slope (xH:1V)	х	Y
									0	3792
									162	3786
									308	3783
R_HSCT1_1	J_HSCT1,2	J_HSCT1_1	2558	0.015	0.040	Eight Pt.	N/A	N/A	319	3782
	,					3			335	3782
						339	3783			
									458 558	3789 3792
									0	3604
									57	3603
									82	3602
R_THC2_1	R_THC2_1	Eight Pt.	N/A	N/A	83	3601				
					111	3601				
					112	3602				
							135	3603		
									190	3604

Table A-28. Adjusted Areas for Socorro Study Area

Watershed Name	Unadjusted Watershed Area (mi²)	Unmodeled Storage Area (mi2)	Adjusted Watershed Area (mi²)
A_Mesa Spur 4-1	0.45	0.033	0.42
A_Mesa Spur 4-2	0.11	0.006	0.11
A_Mesa Spur 5.5-1	0.91	0.036	0.87
A_Mesa Spur 5.5-2	0.32	0.000	0.32
A_Mesa Spur 5-1	0.08	0.008	0.07
A_Stream 4-1	0.21	0.000	0.21
A_Stream 4-2	0.44	0.001	0.44
A_Stream 4-2b	0.03	0.000	0.03
A_Stream 4-3A	1.93	0.000	1.93
A_Stream 4-3B	0.65	0.000	0.65
A_Stream 5.5-1	0.09	0.001	0.09
A_Stream 5.5-2	1.34	0.000	1.34
A_Stream 5-1	0.18	0.001	0.18
A_Stream 5-2	0.78	0.000	0.78
A_Stream 5-2a	0.11	0.000	0.11

Table A-29. Adjusted Curve Numbers for for Socorro Study Area

Watershed Name	Initial CN	Storage Adjusted CN
A_Stream 4-2	60	48
A_Stream 4-3A	76	63

Table A-30. Adjusted Areas for Hacienda Real Study Area

Watershed Name	Unadjusted Watershed Area (mi²)	Unmodeled Storage Area (mi2)	Adjusted Watershed Area (mi²)		
A_Clint Landfill A	0.11	0.000	0.11		
A_Clint Landfill B	0.32	0.000	0.32		
A_Clint Landfill C	0.27	0.000	0.27		
A_Clint Landfill D	0.28	0.000	0.28		
A_Hacienda Real-1	1.82	0.002	1.82		
A_Hacienda Real-2	0.18	0.000	0.18		
A_Hacienda Real-3	0.51	0.001	0.51		
A_Hacienda Real-4	0.63	0.001	0.63		
A_Hacienda Real-5	0.42	0.000	0.42		
A_Hacienda Real-6	0.64	0.000	0.64		
A_Hacienda Real-7	0.27	0.004	0.27		
A_Hacienda Real-8	1.99	0.003	1.99		
A_Stream 10-1	0.08	0.000	0.08		
A_Stream 10-2	0.06	0.000	0.06		
A_Stream 11-1	0.41	0.000	0.41		
A_Stream 11-2	0.11	0.000	0.11		
A_Stream 12-1	0.16	0.000	0.16		
A_Stream 12-2	0.87	0.000	0.87		
A_Stream 12-3	0.03	0.000	0.03		
A_Stream 12-4	0.38	0.000	0.38		
A_Stream 13.5-1a	0.24	0.000	0.24		
A_Stream 13.5-1b	0.46	0.000	0.46		
A_Stream 13.5-2	0.04	0.000	0.04		
A_Stream 13.5-3	0.53	0.000	0.53		
A_Stream 13.5-4a	5.67	0.027	5.64		
A_Stream 13.5-4b	0.49	0.000	0.49		
A_Stream 13-1	0.02	0.000	0.02		
A_Stream 13-2	0.38	0.000	0.38		
A_Stream 6-1	0.34	0.009	0.33		
A_Stream 6-2	0.51	0.000	0.51		
A_Stream 7-1	0.25	0.000	0.25		
A_Stream 7-2	0.08	0.000	0.08		
A_Stream 7-3	0.47	0.000	0.47		
A_Stream 7-4	4.91	0.033	4.88		
A_Stream 8-1	0.04	0.000	0.04		
A_Stream 8-2	0.29	0.000	0.29		
A_Stream 8-3	0.64	0.000	0.64		
A_Stream 9-1	0.24	0.000	0.24		
A_Stream 9-2	0.14	0.000	0.14		

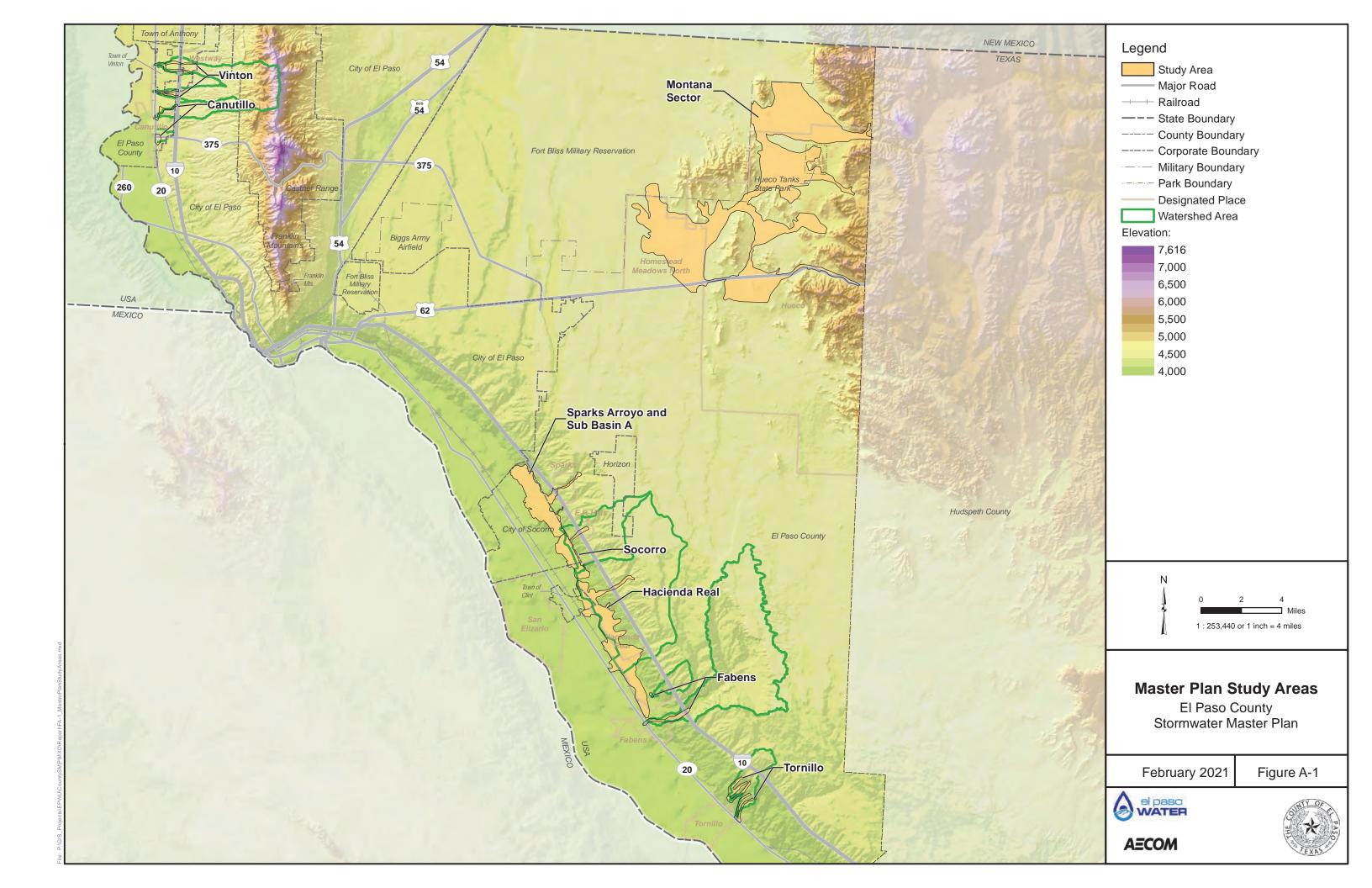
Table A-31. Estimation of Rainfall Depth by Annual Exceedance Probability

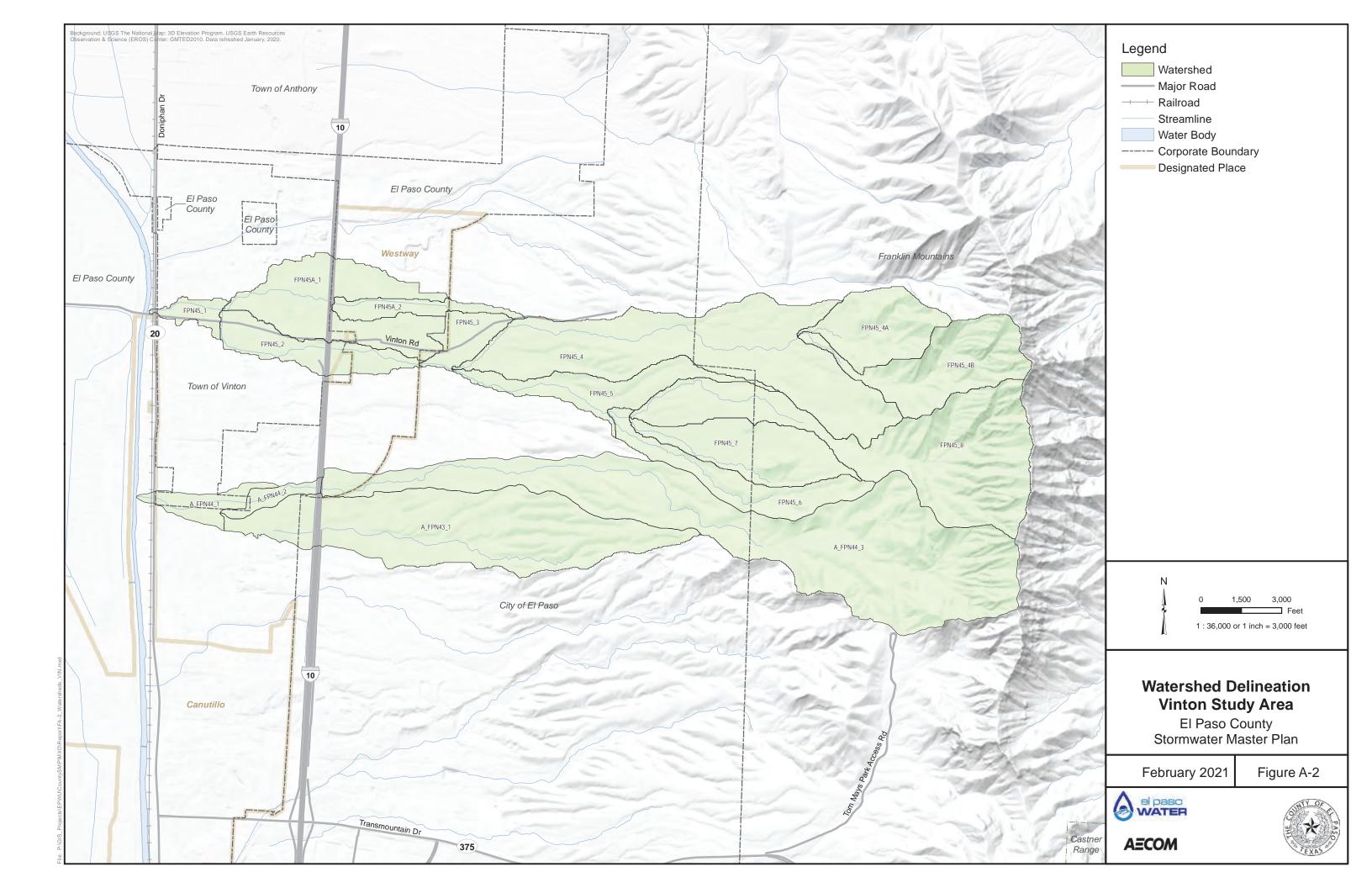
	Total Rainfall Depth (inches) by Duration								
Return Frequency	5 min	15 min	1 hr	2 hr	3 hr	6 hr	12 hr	24 hr	
	West El Paso								
1	0.238	0.460	0.701	0.814	0.880	1.00	1.13	1.28	
2	0.311	0.601	0.915	1.06	1.14	1.29	1.45	1.64	
5	0.424	0.818	1.25	1.44	1.55	1.74	1.95	2.19	
10	0.522	1.01	1.54	1.77	1.90	2.14	2.39	2.67	
25	0.664	1.28	1.95	2.25	2.41	2.71	3.02	3.38	
50	0.778	1.51	2.29	2.63	2.83	3.18	3.54	3.96	
100	0.901	1.74	2.65	3.04	3.27	3.68	4.10	4.60	
200	1.03	2.00	3.04	3.50	3.76	4.23	4.73	5.31	
500	1.23	2.37	3.60	4.14	4.45	5.02	5.64	6.35	
	East El Paso								
1	0.235	0.451	0.671	0.786	0.855	0.966	1.05	1.14	
2	0.301	0.578	0.859	1.00	1.09	1.23	1.35	1.49	
5	0.404	0.777	1.15	1.34	1.45	1.64	1.82	2.01	
10	0.494	0.949	1.41	1.63	1.77	2.00	2.23	2.49	
25	0.622	1.19	1.77	2.05	2.21	2.51	2.82	3.19	
50	0.723	1.39	2.06	2.37	2.56	2.91	3.31	3.78	
100	0.832	1.60	2.37	2.73	2.94	3.35	3.84	4.43	
200	0.957	1.84	2.73	3.14	3.38	3.86	4.45	5.17	
500	1.14	2.20	3.25	3.74	4.04	4.62	5.36	6.26	

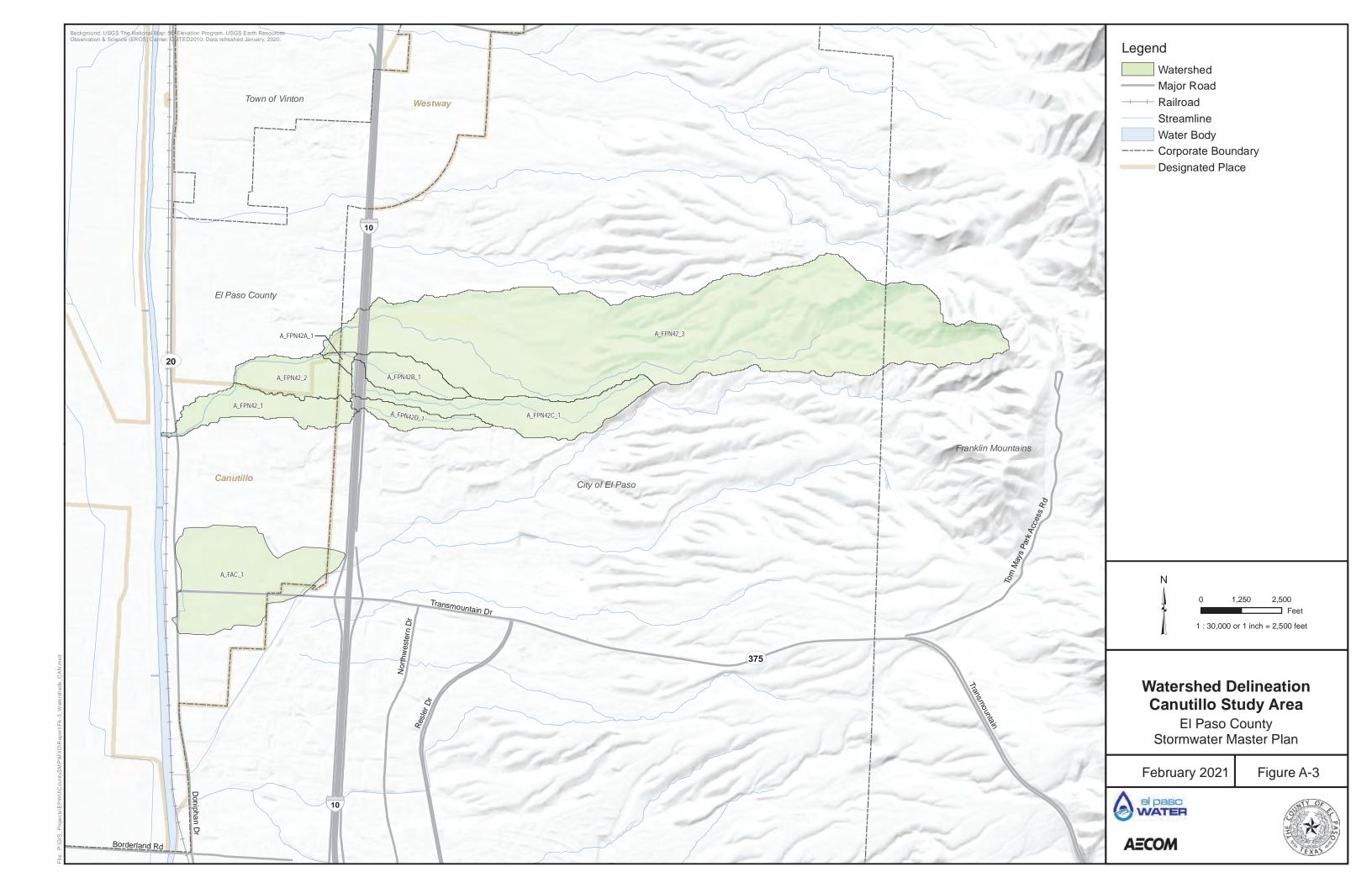
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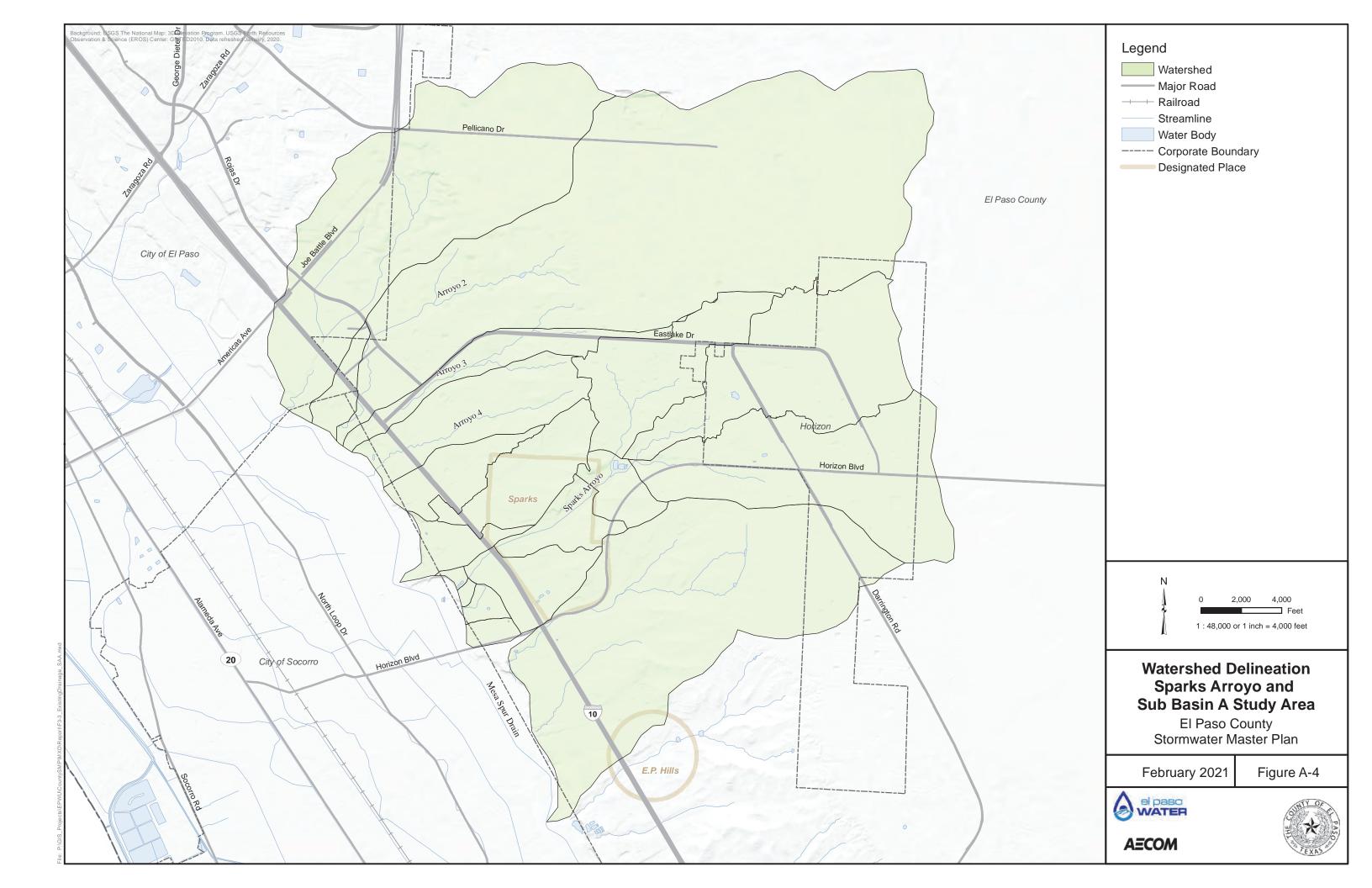
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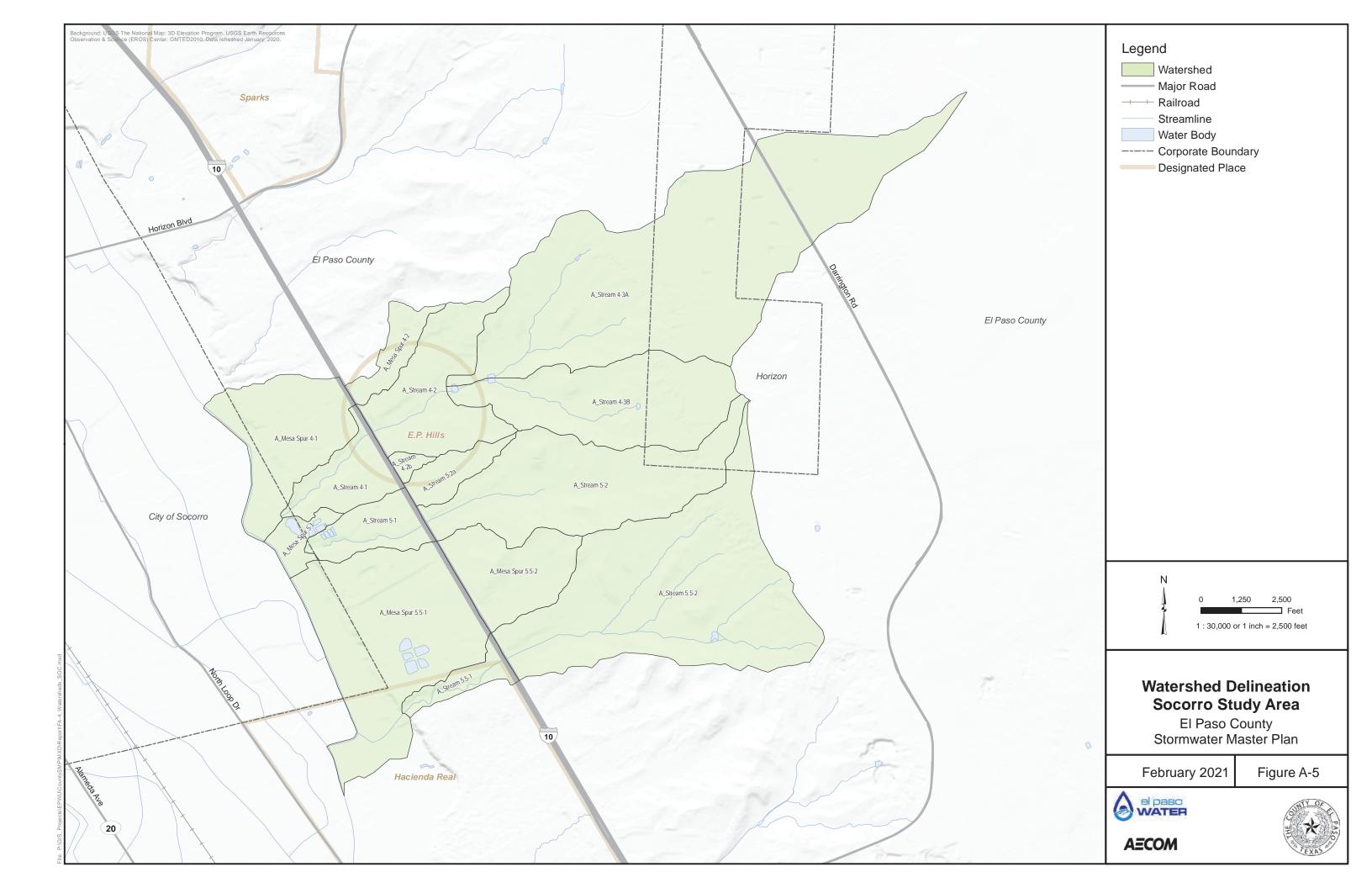
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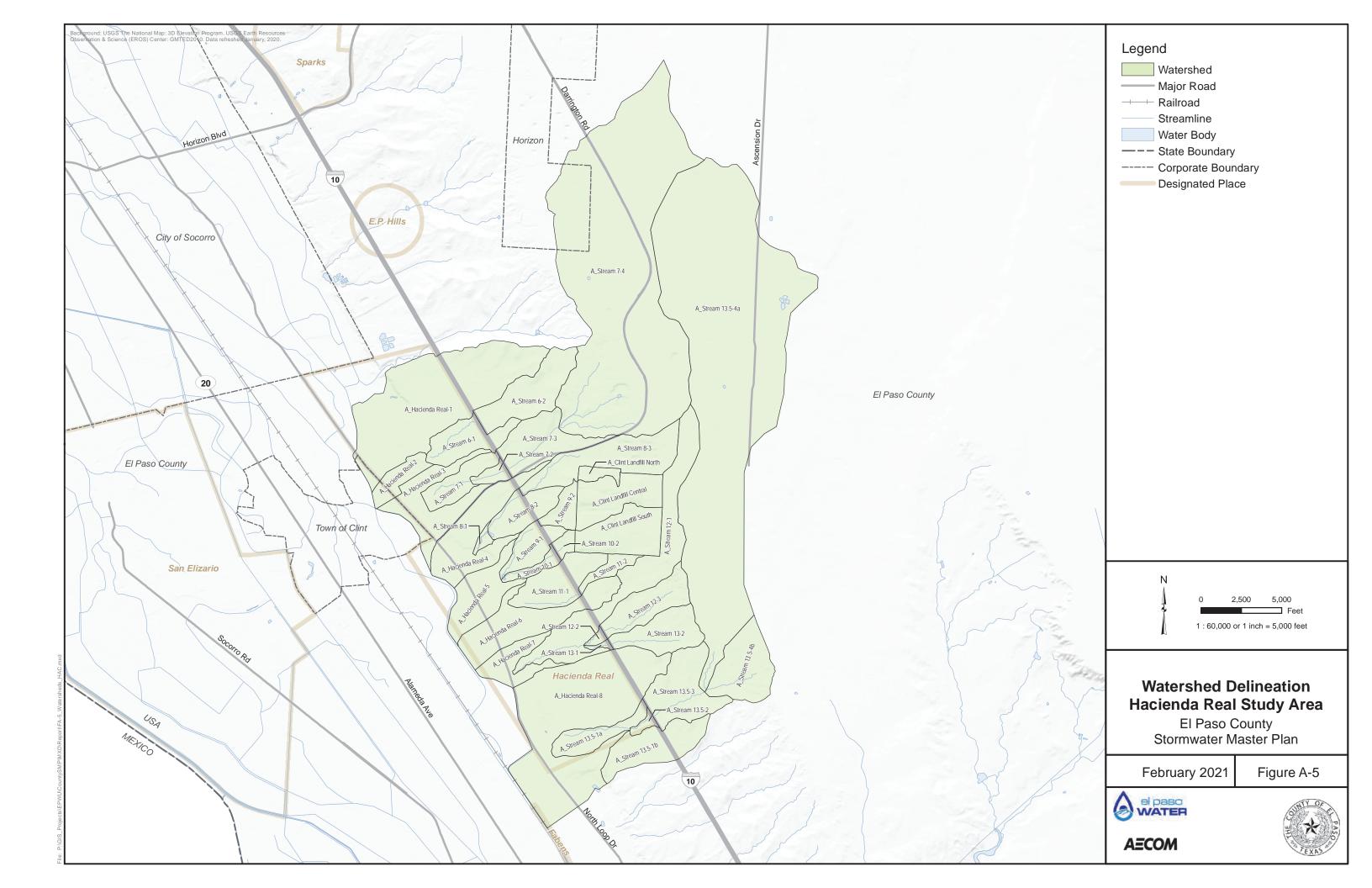


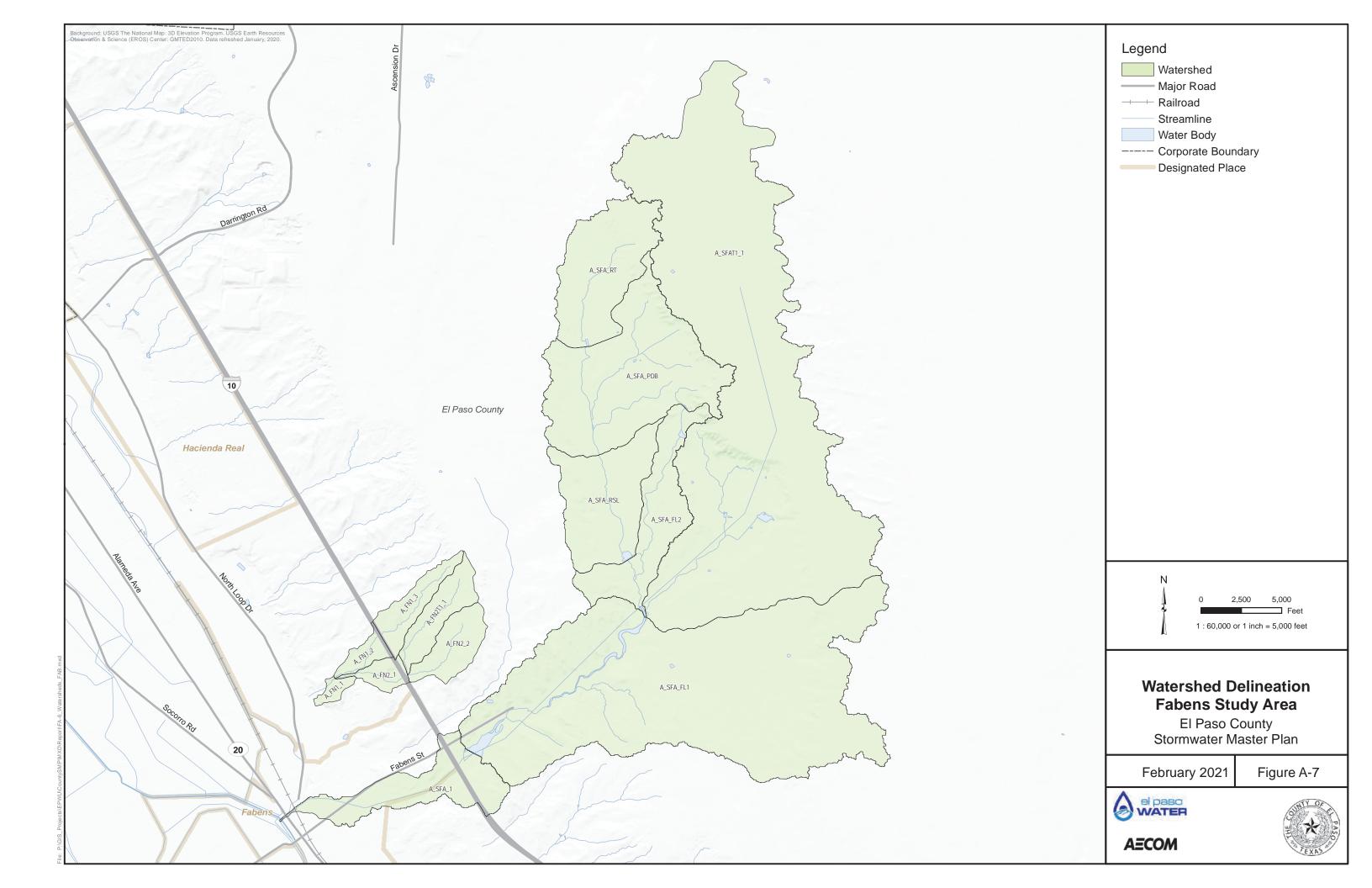


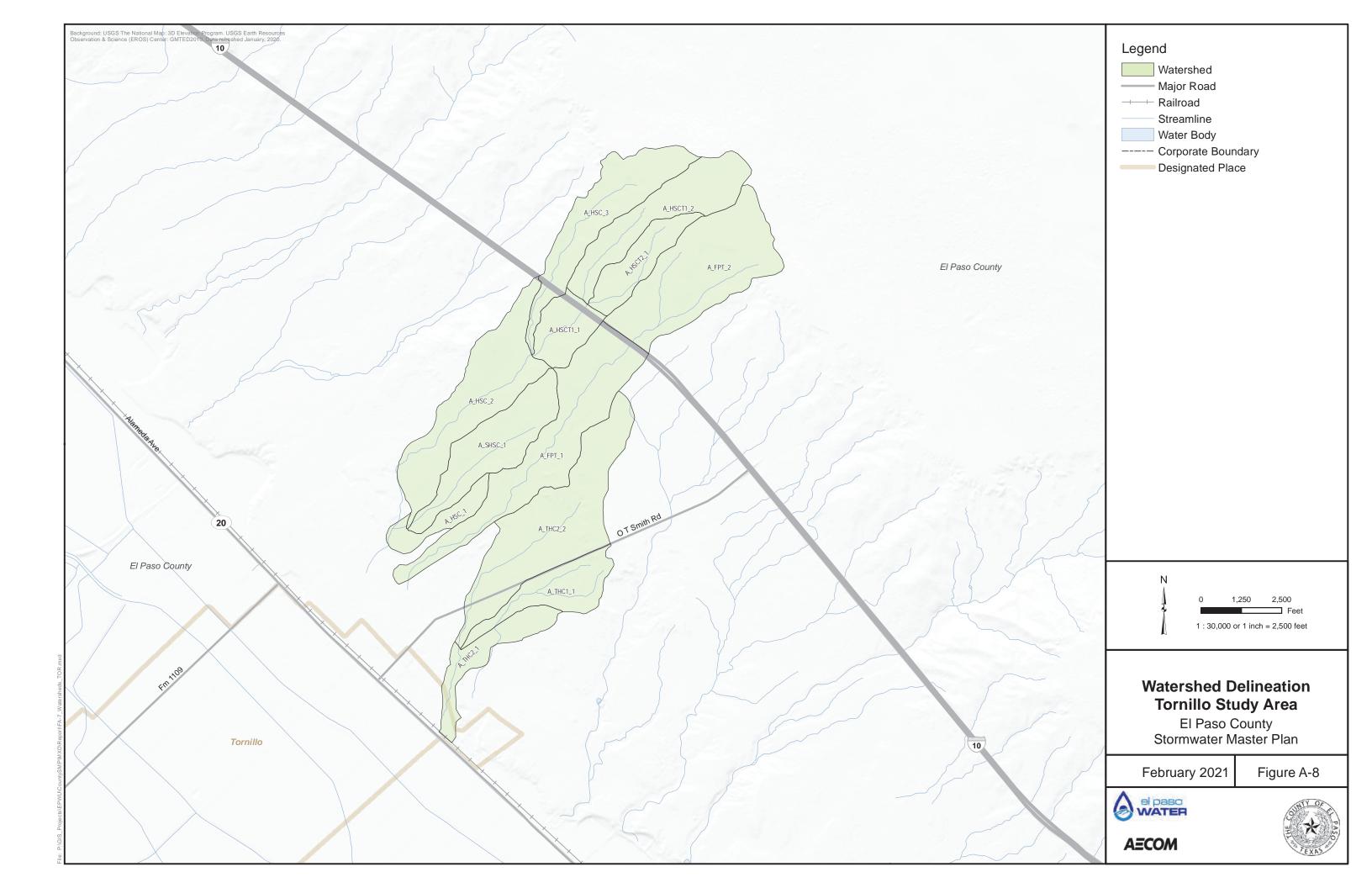


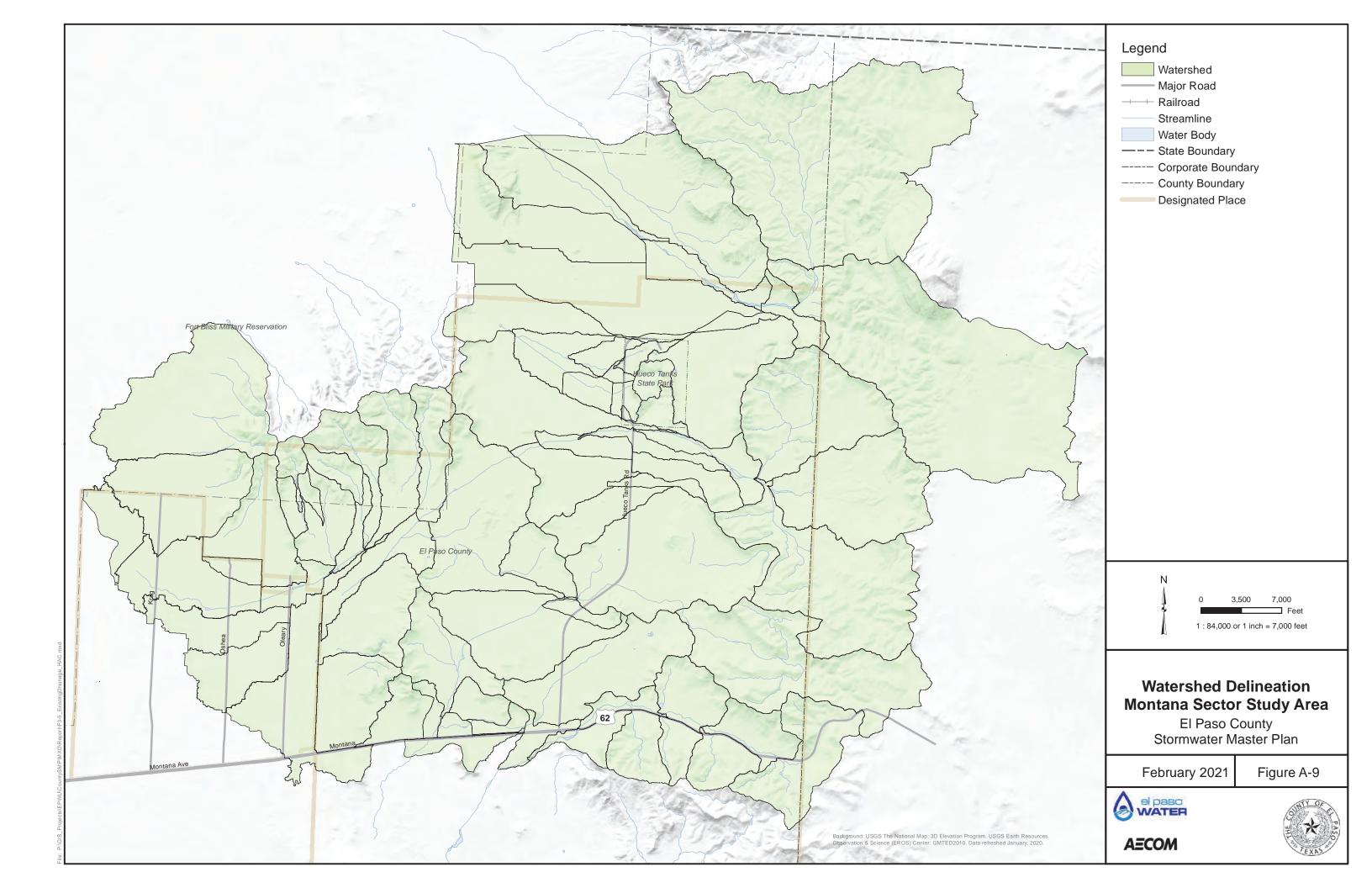


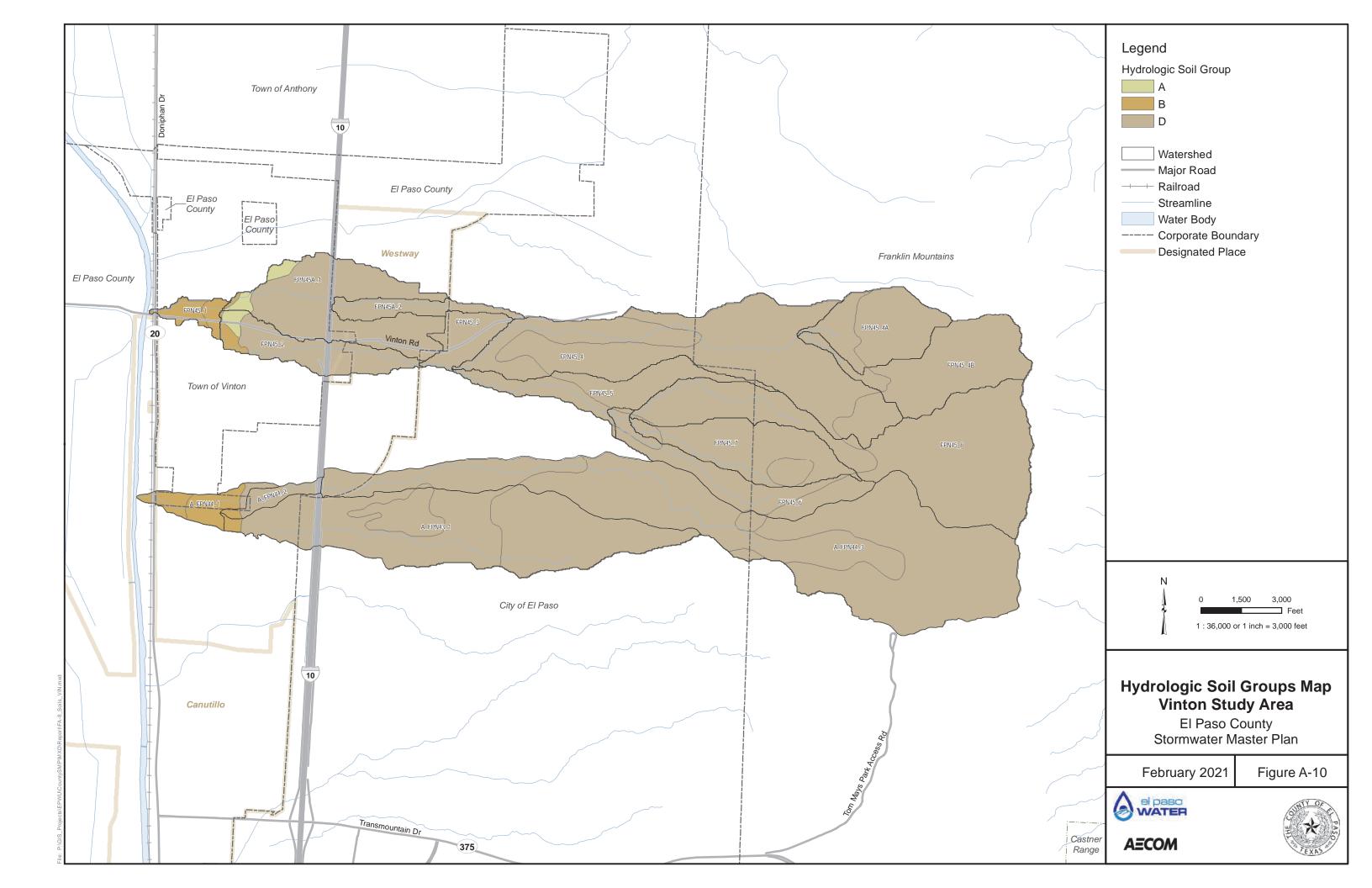


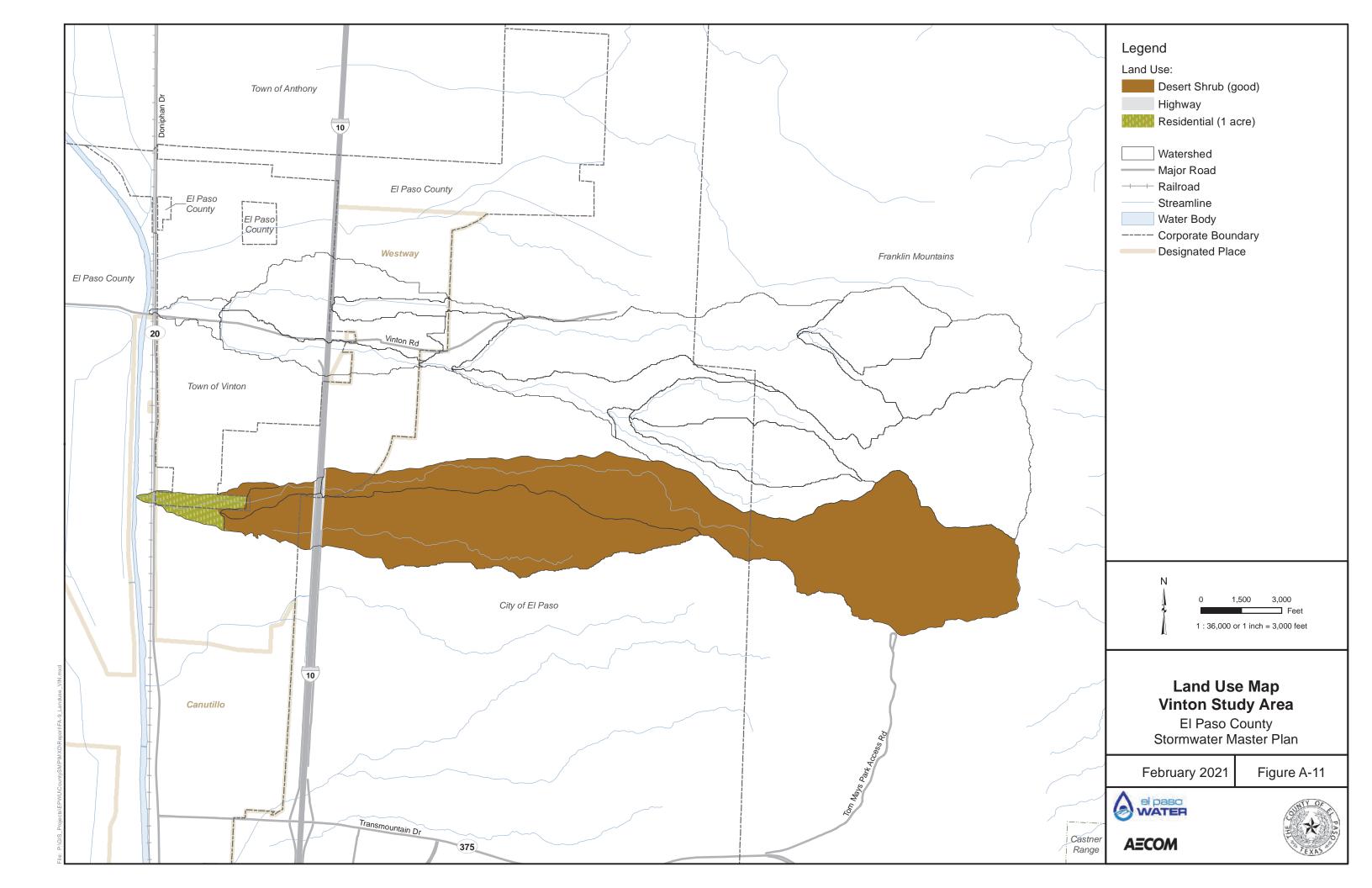


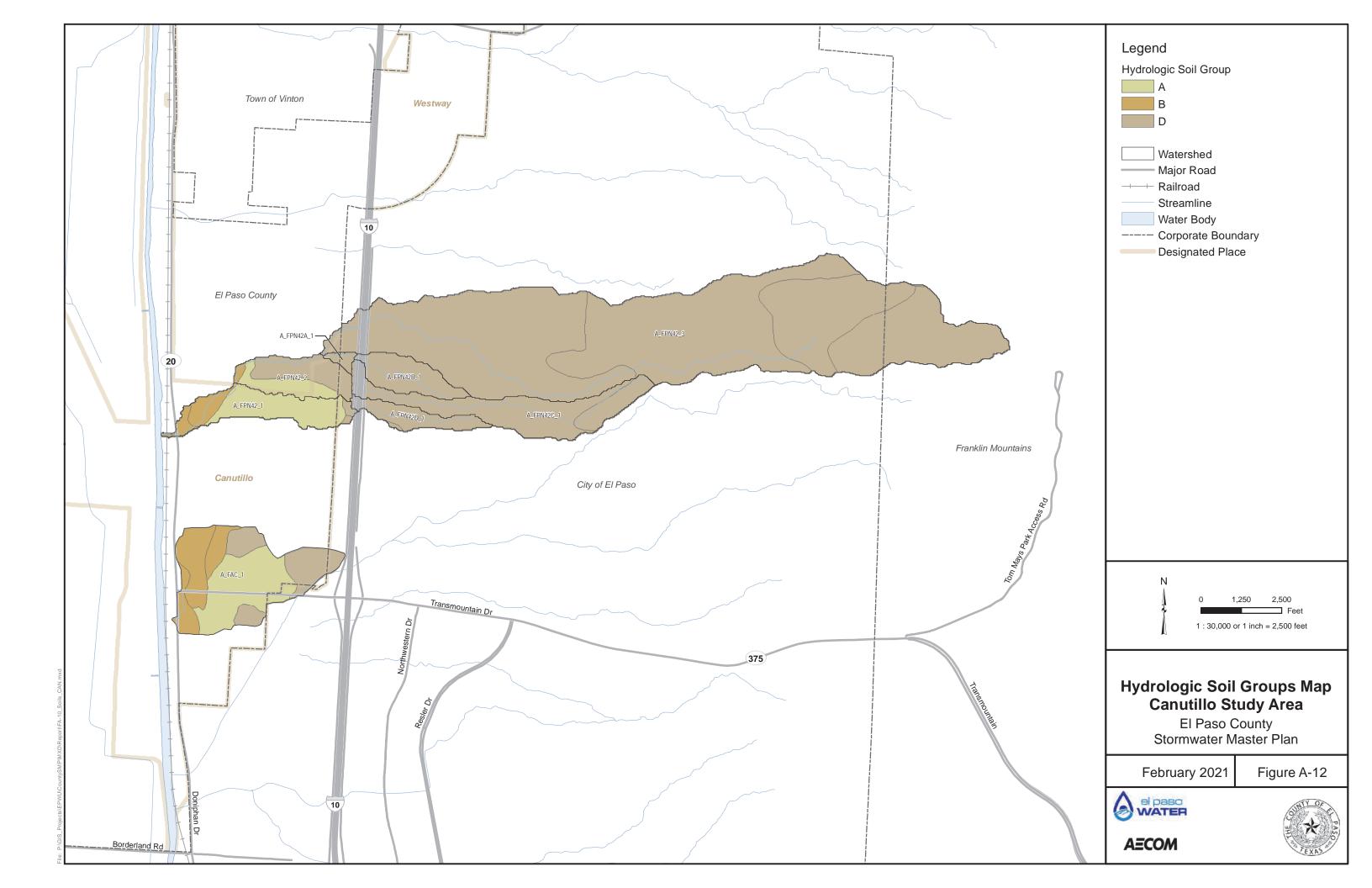


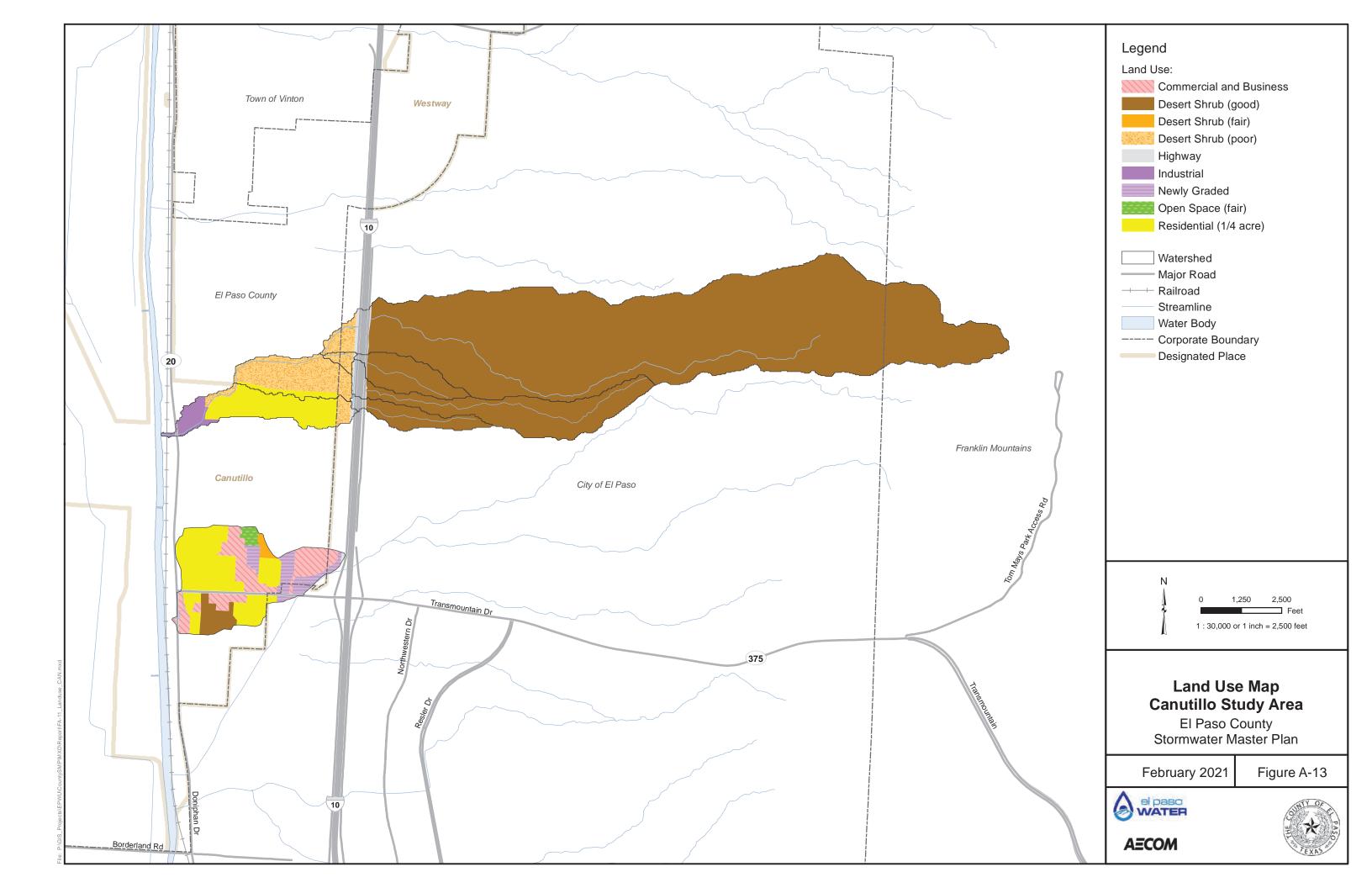


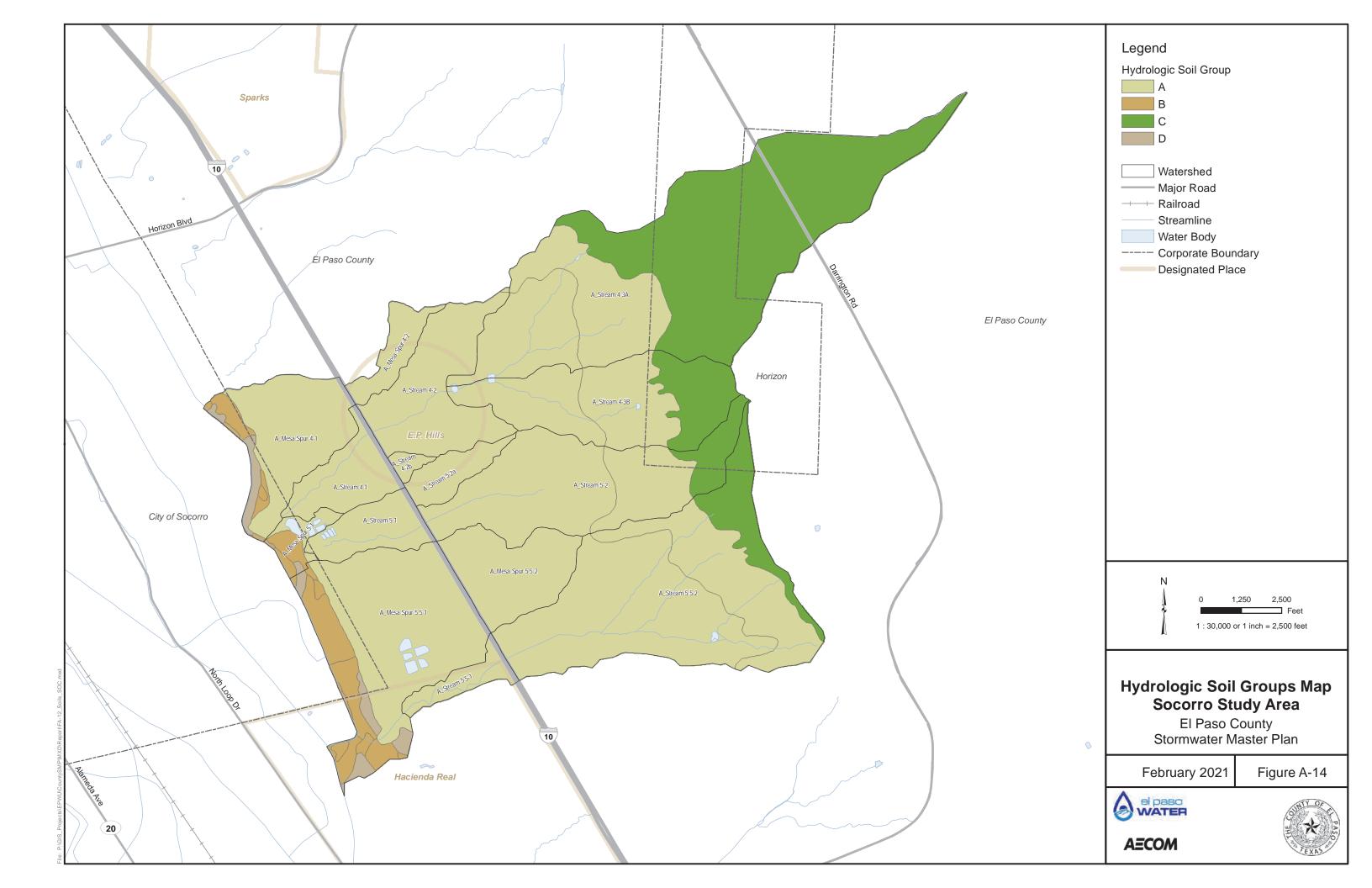


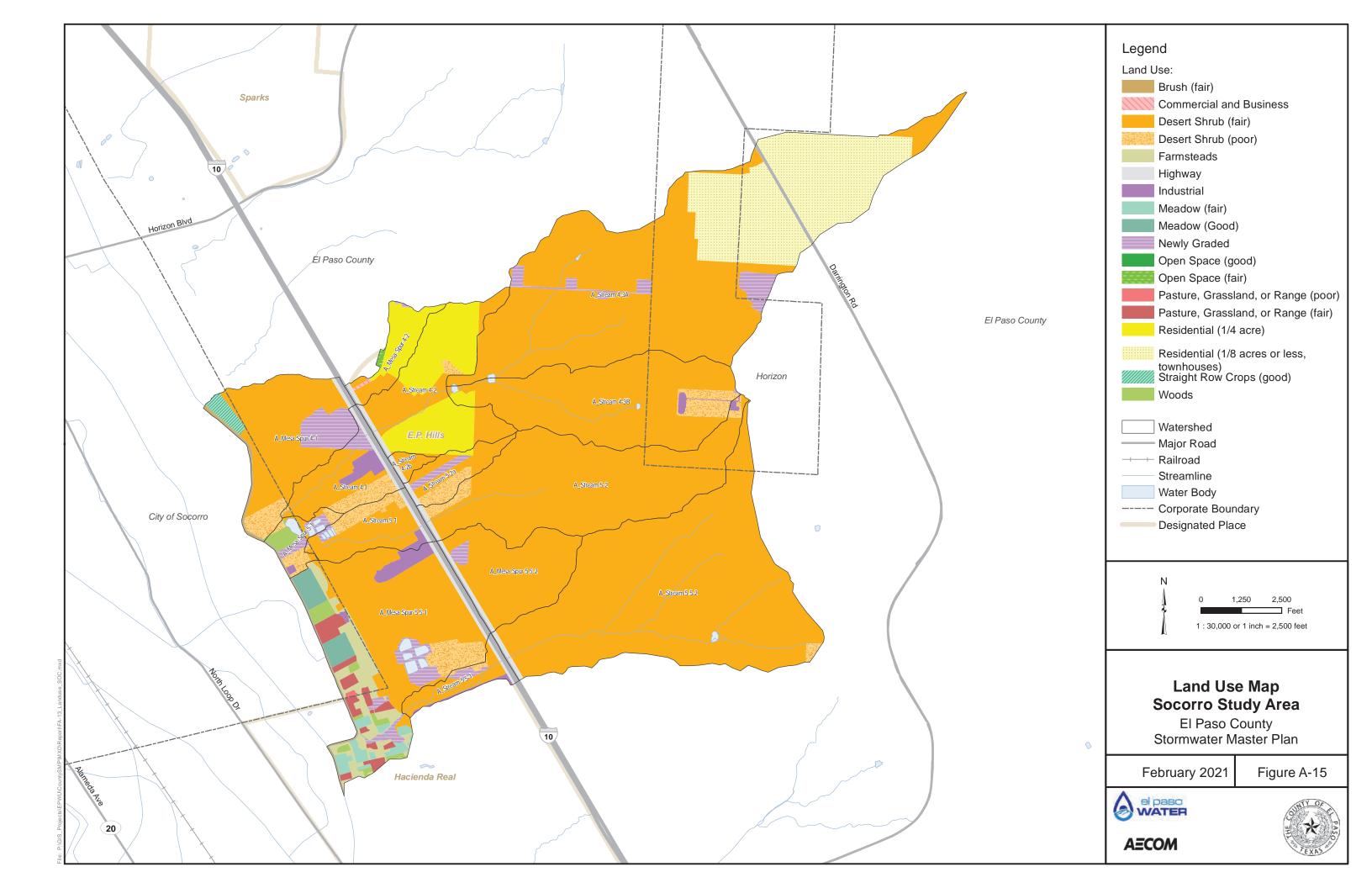


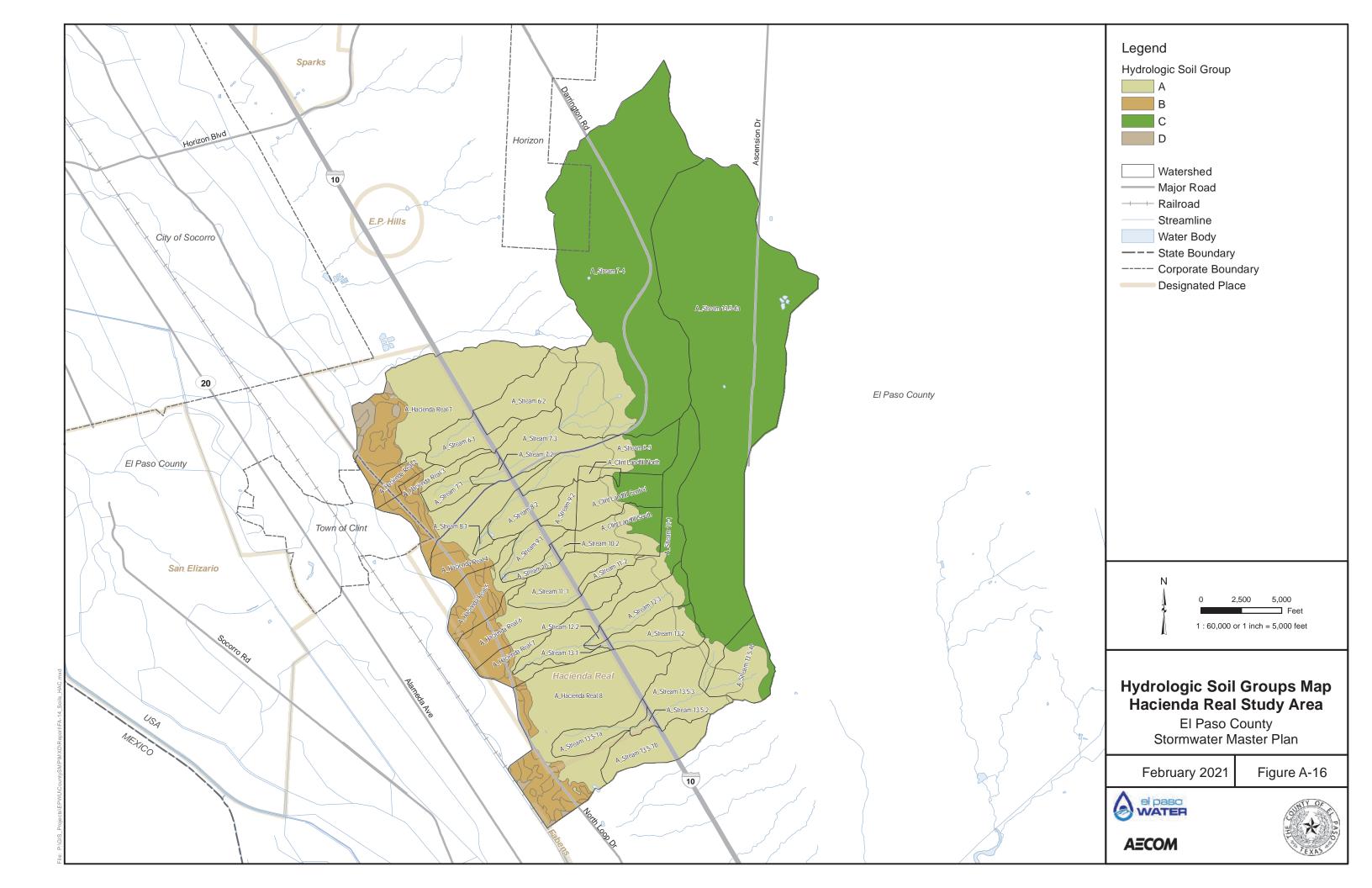


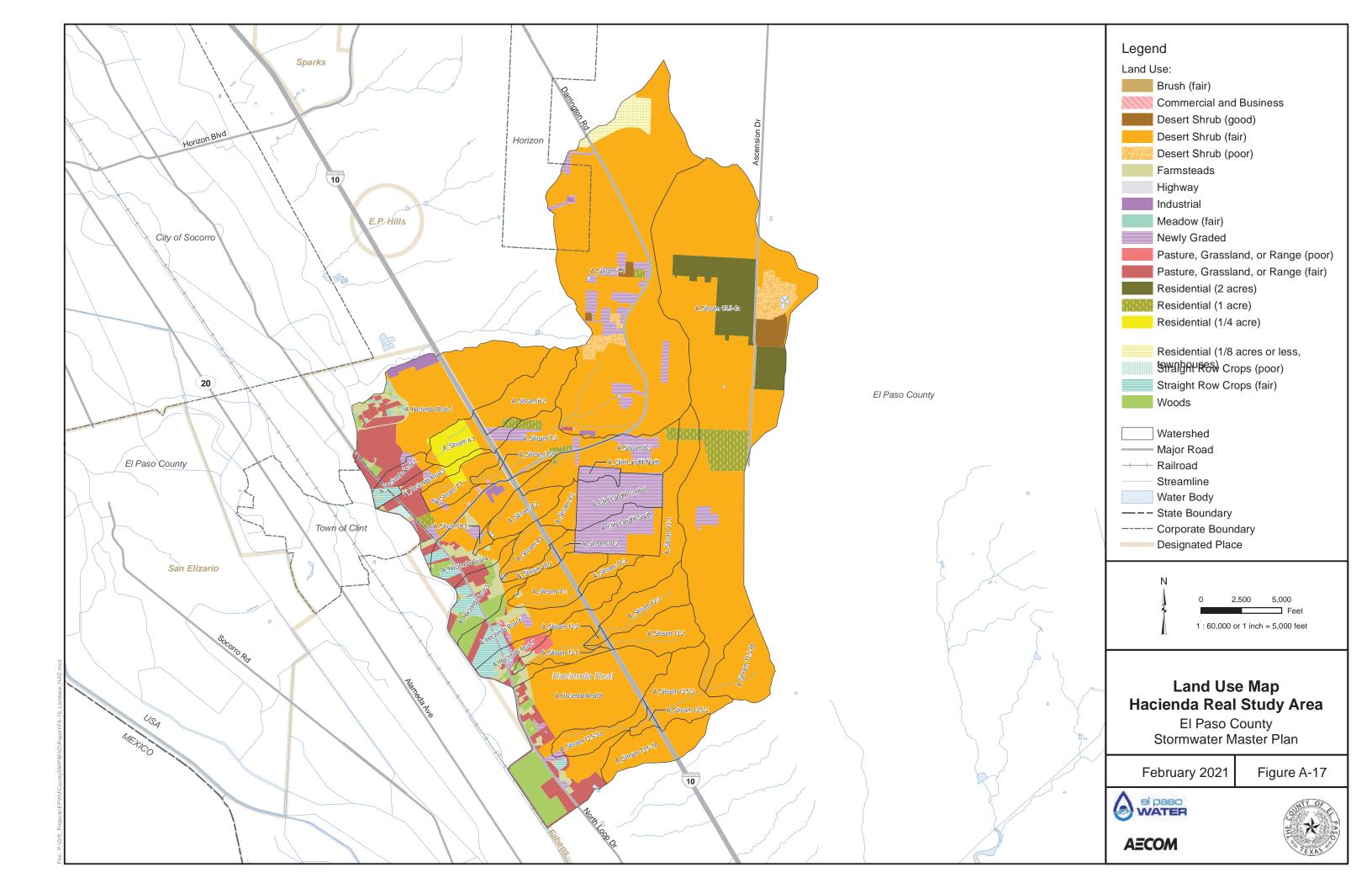


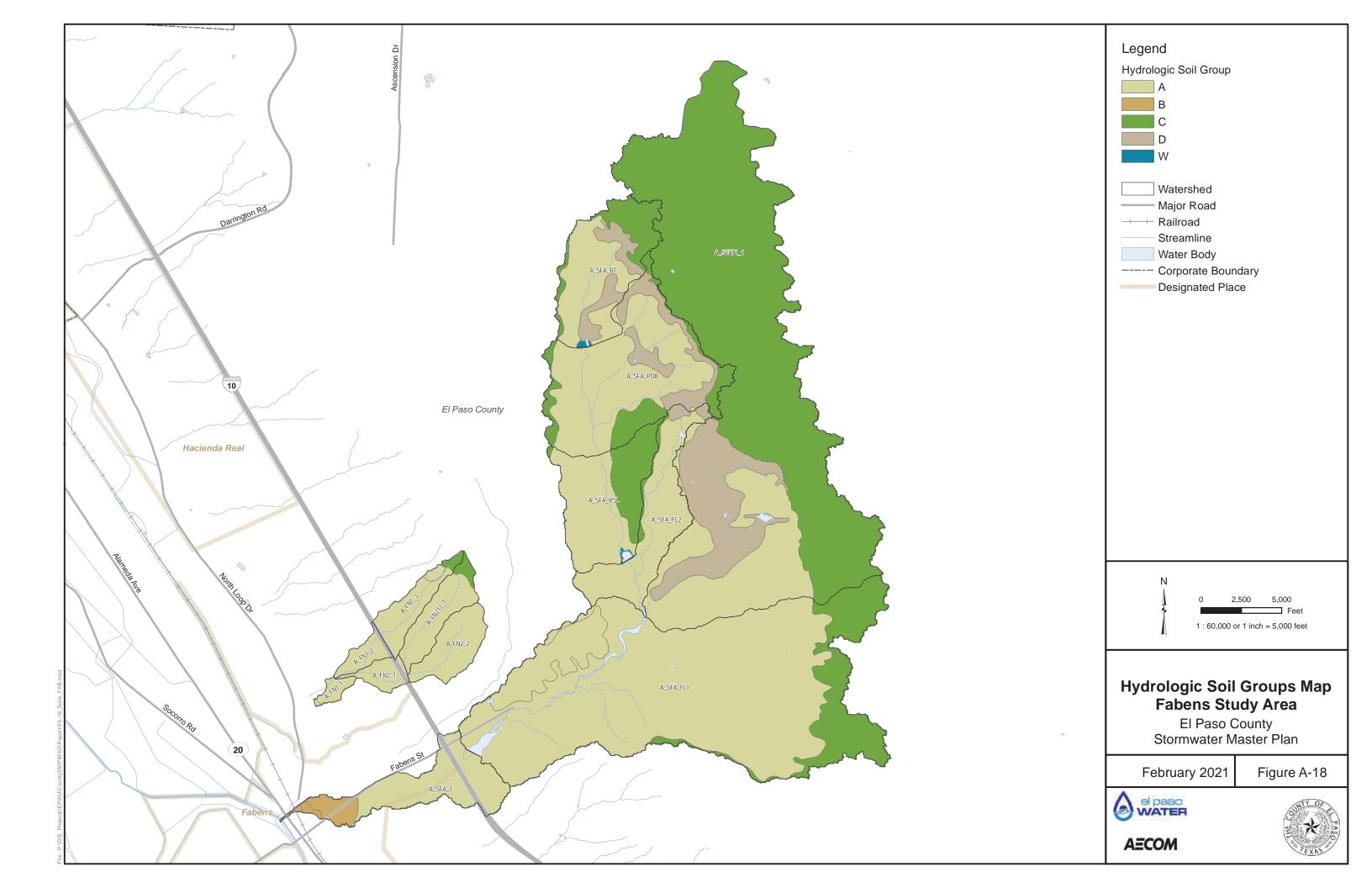


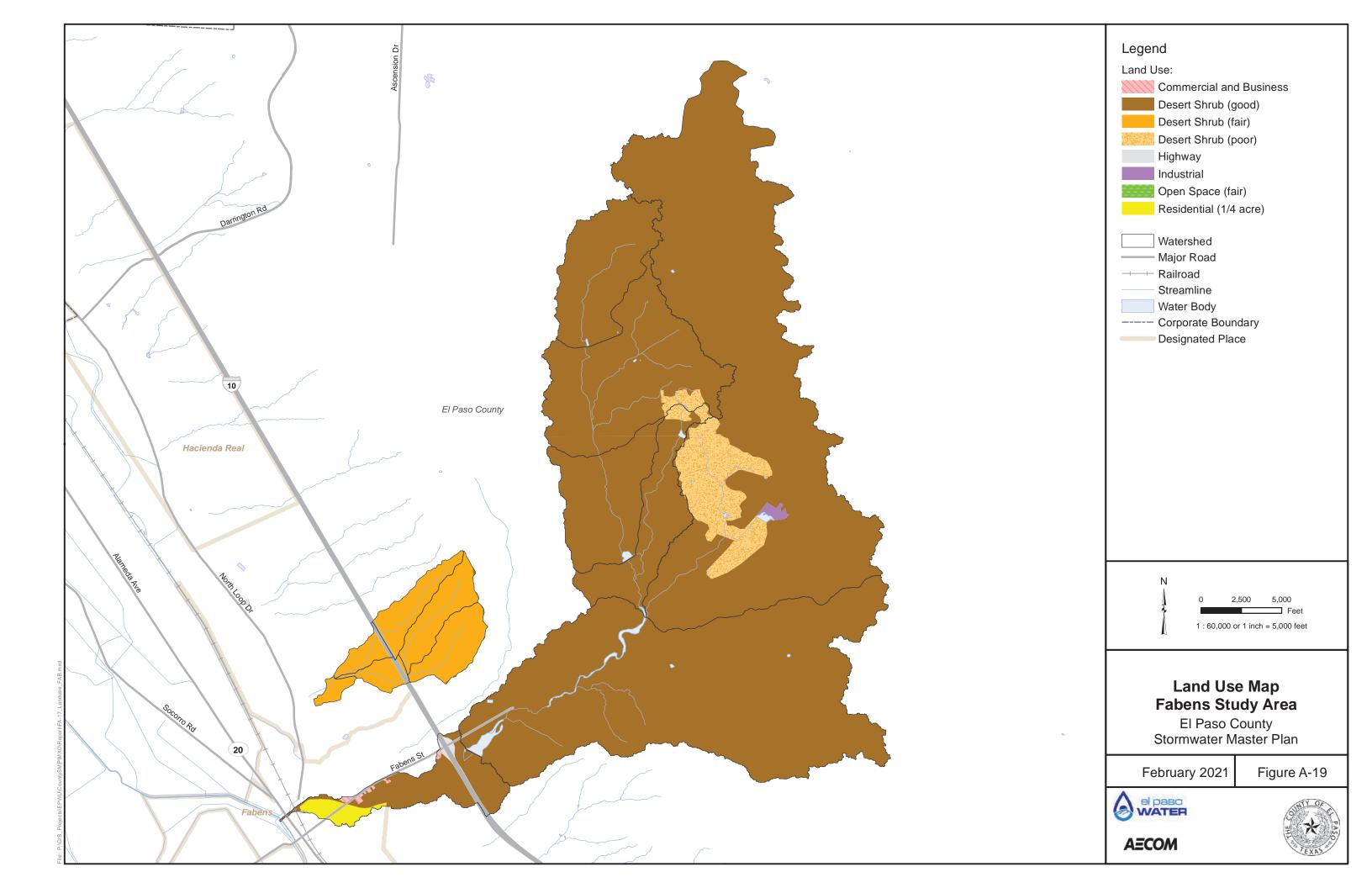


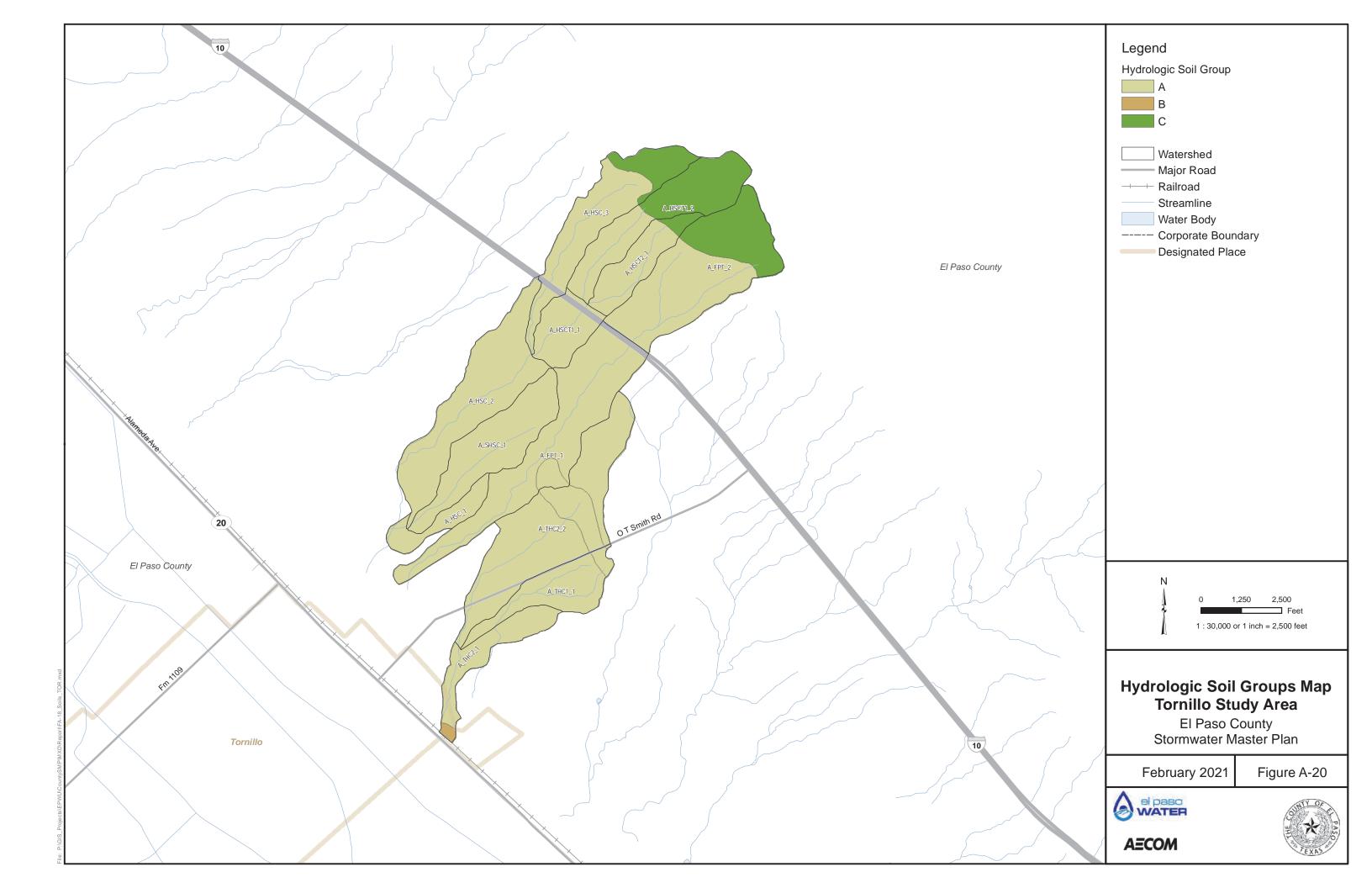


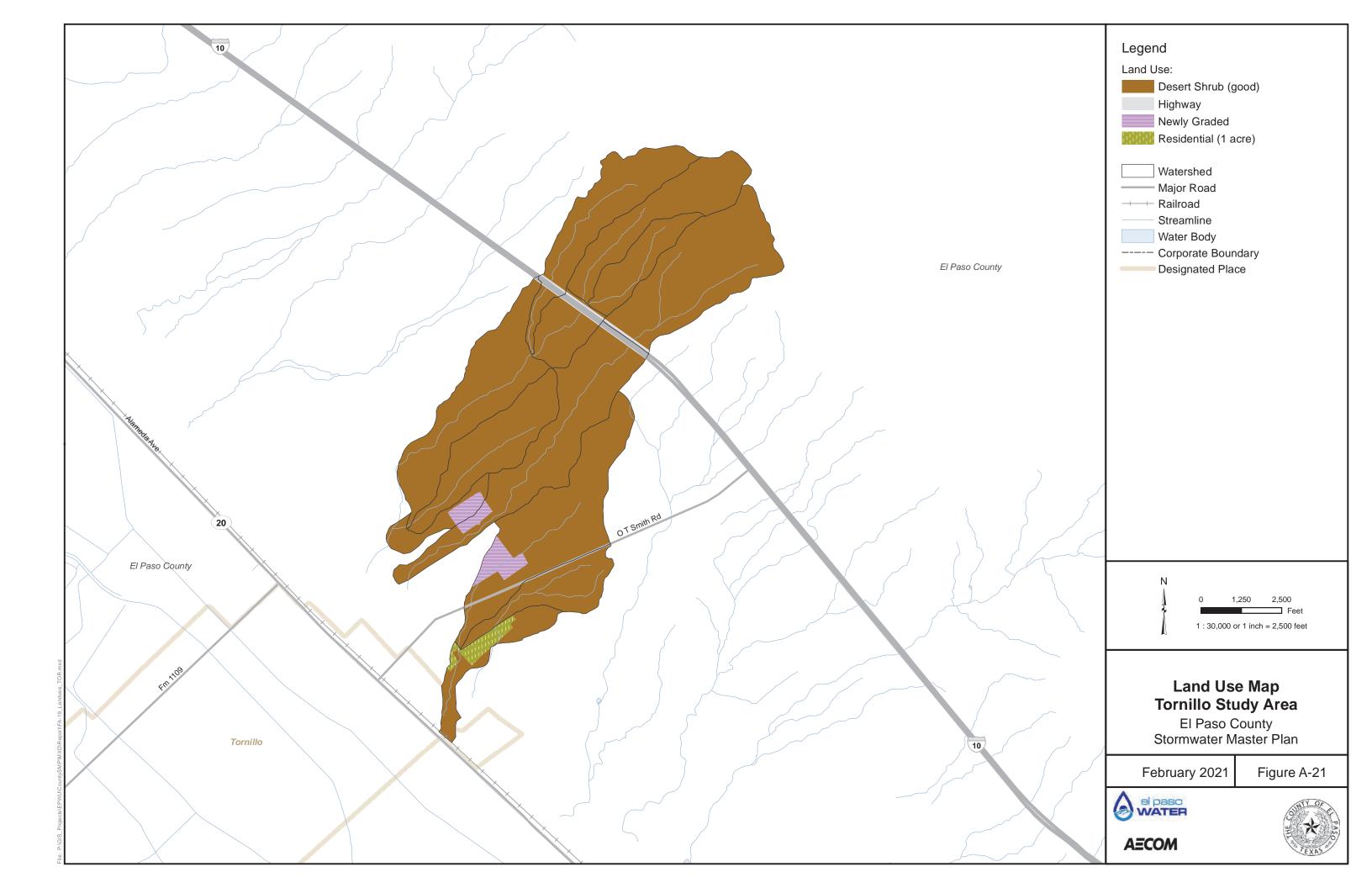


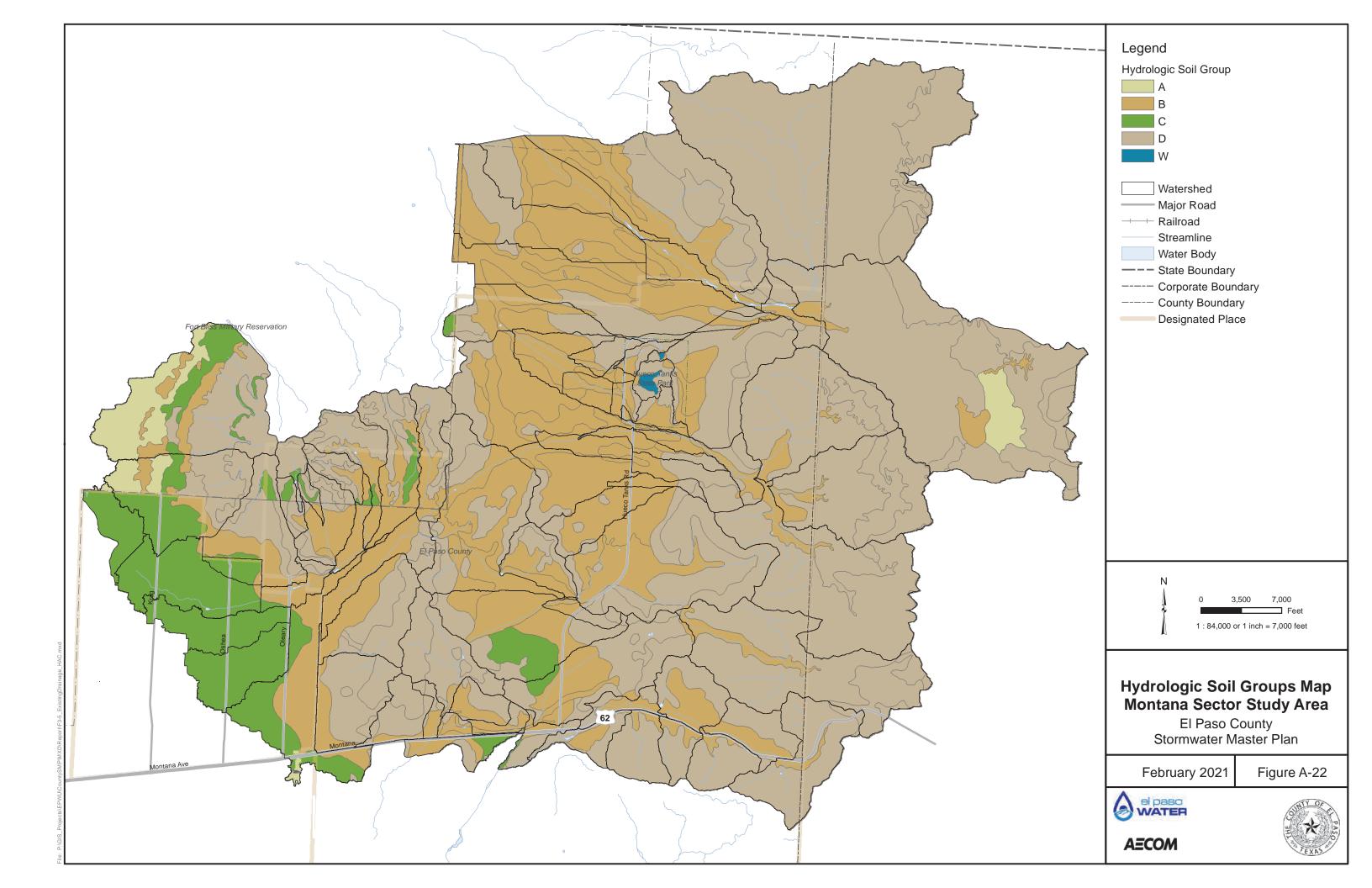


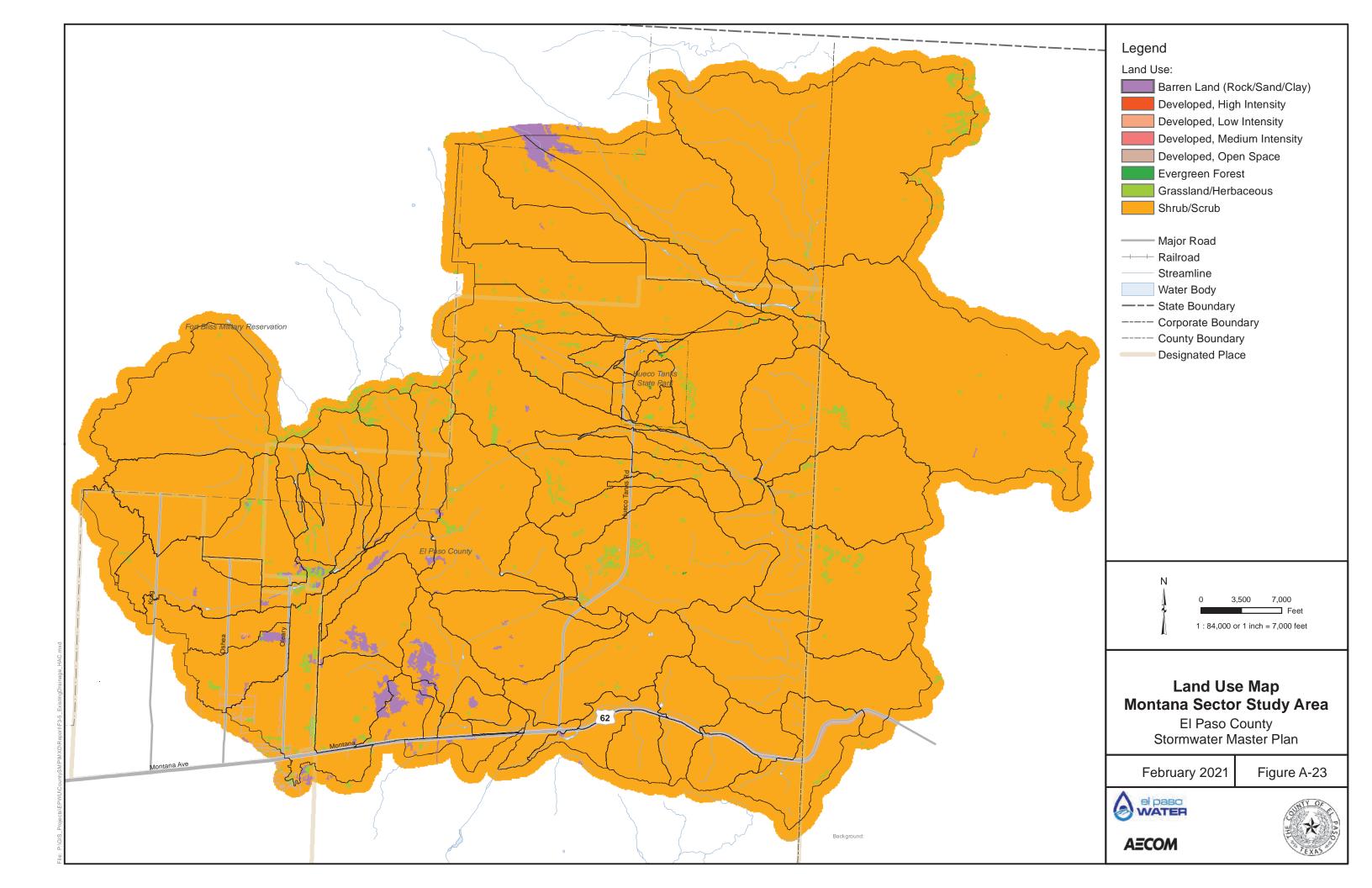


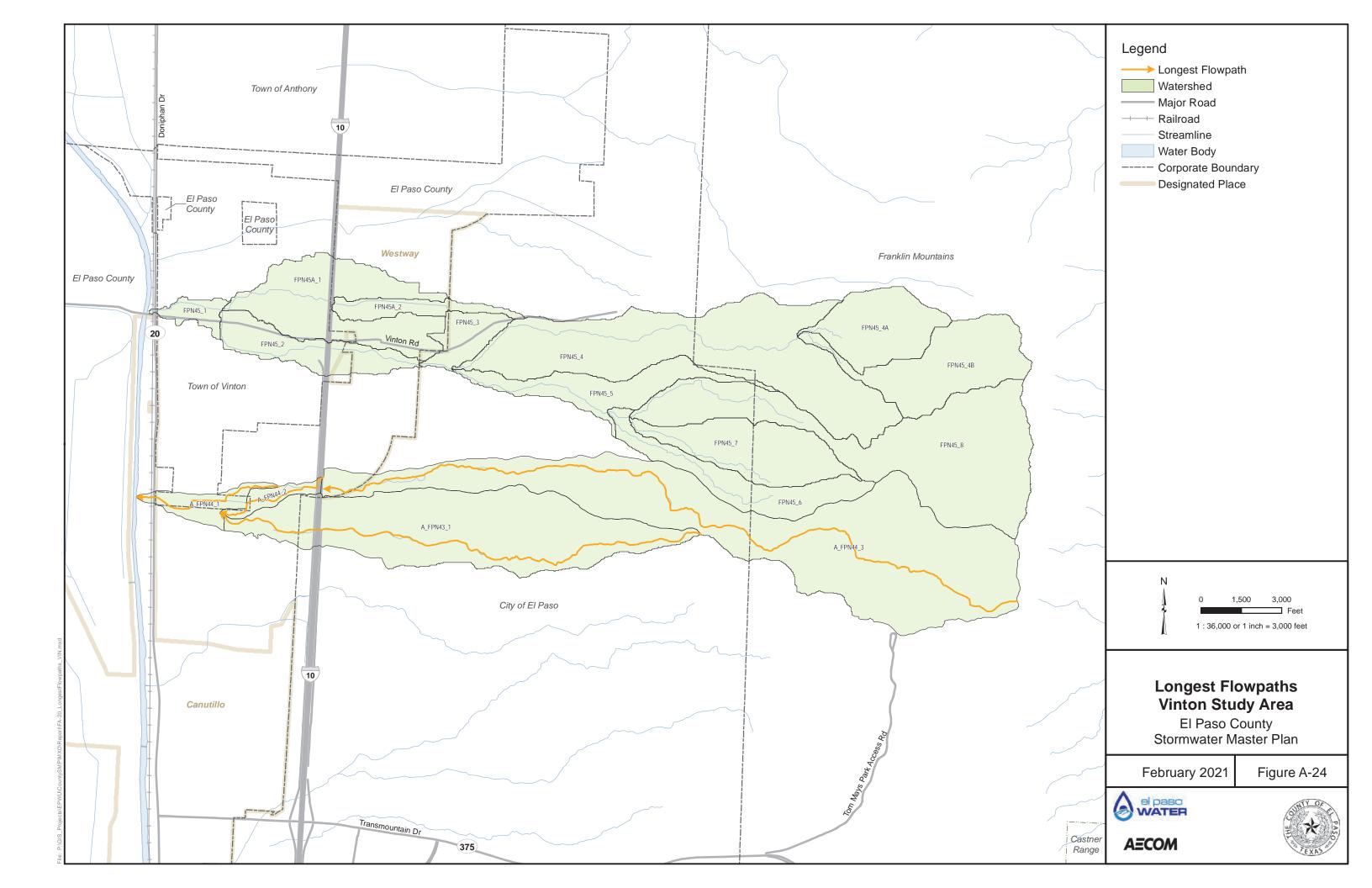


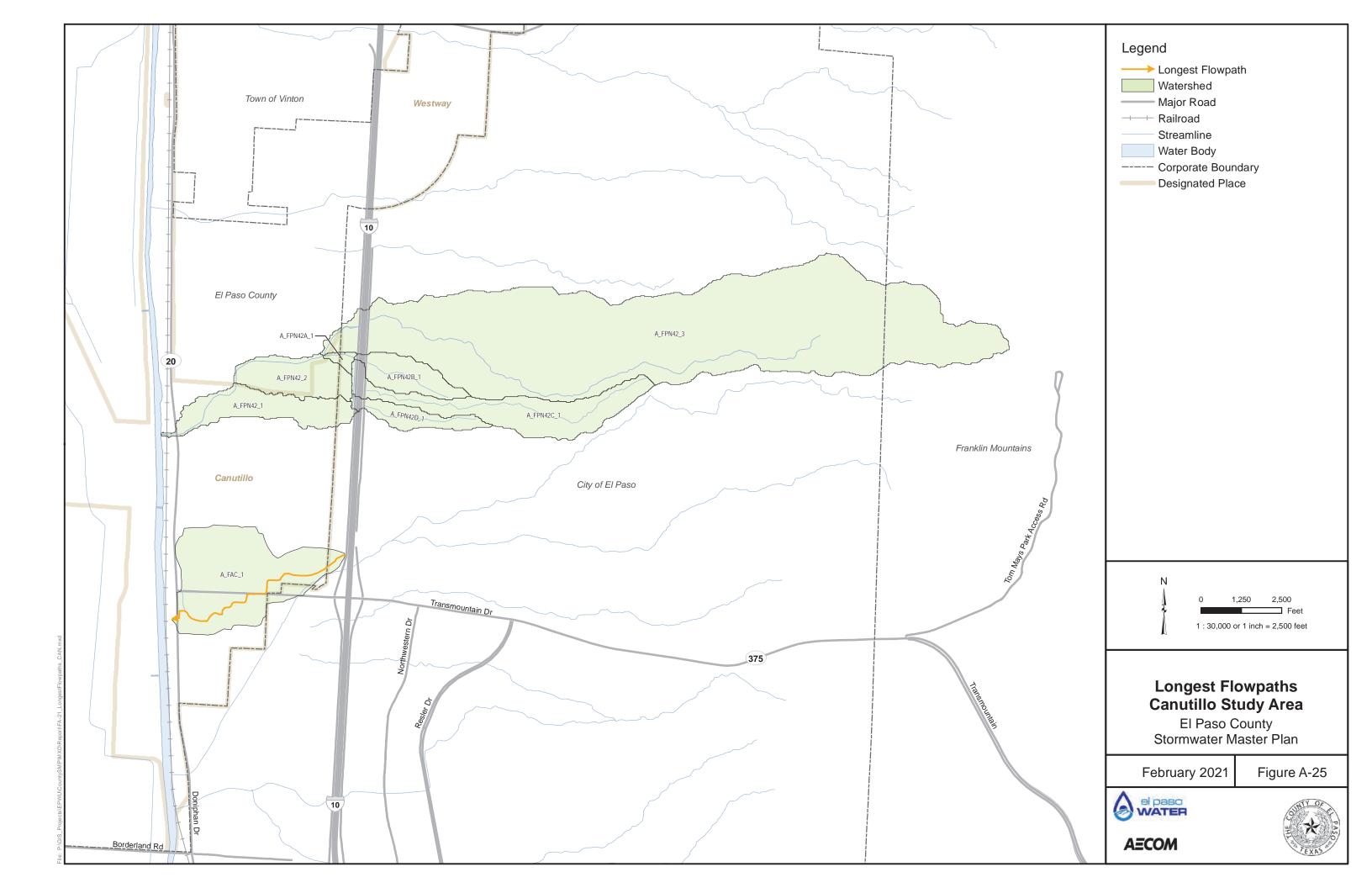


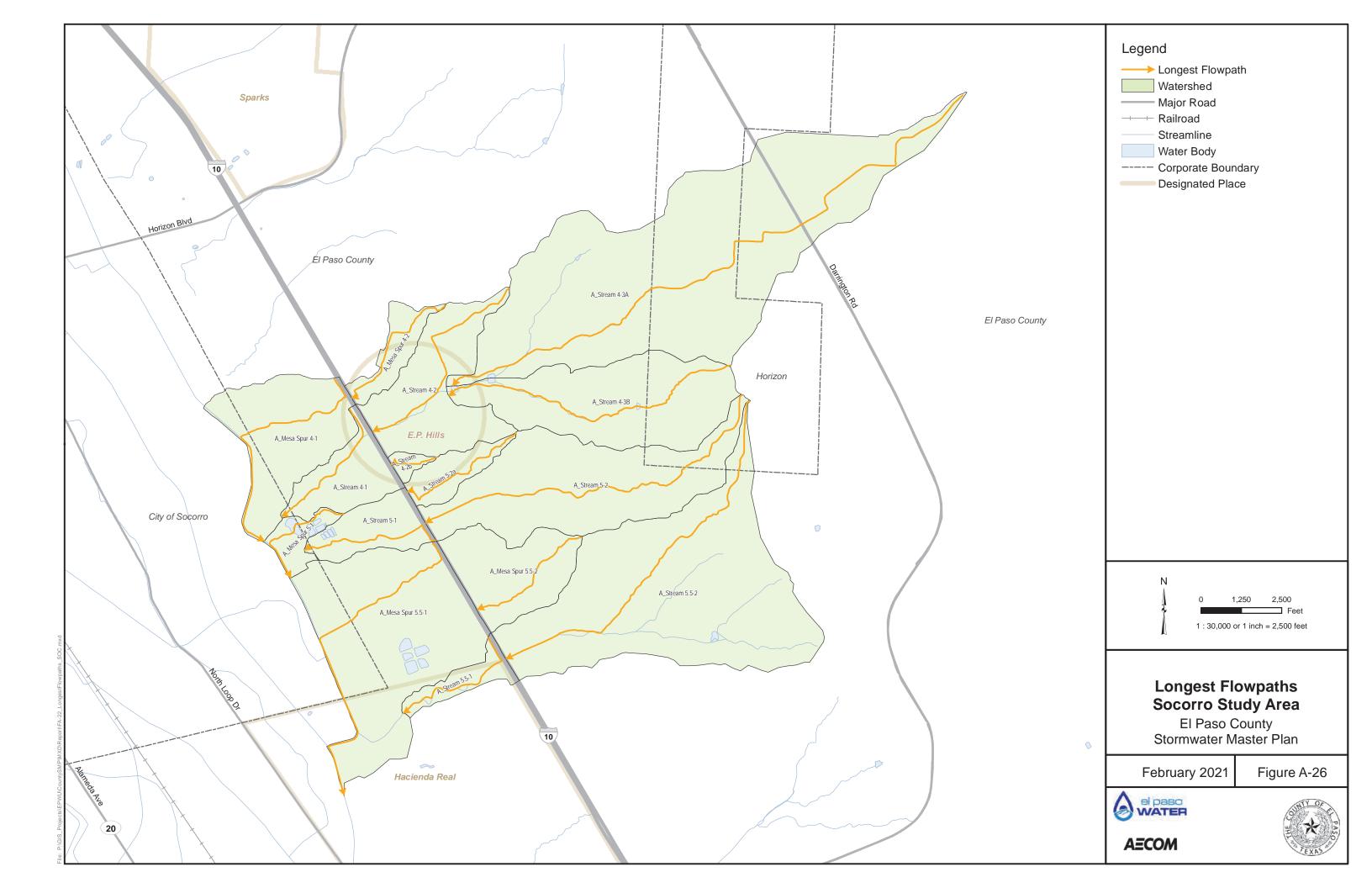


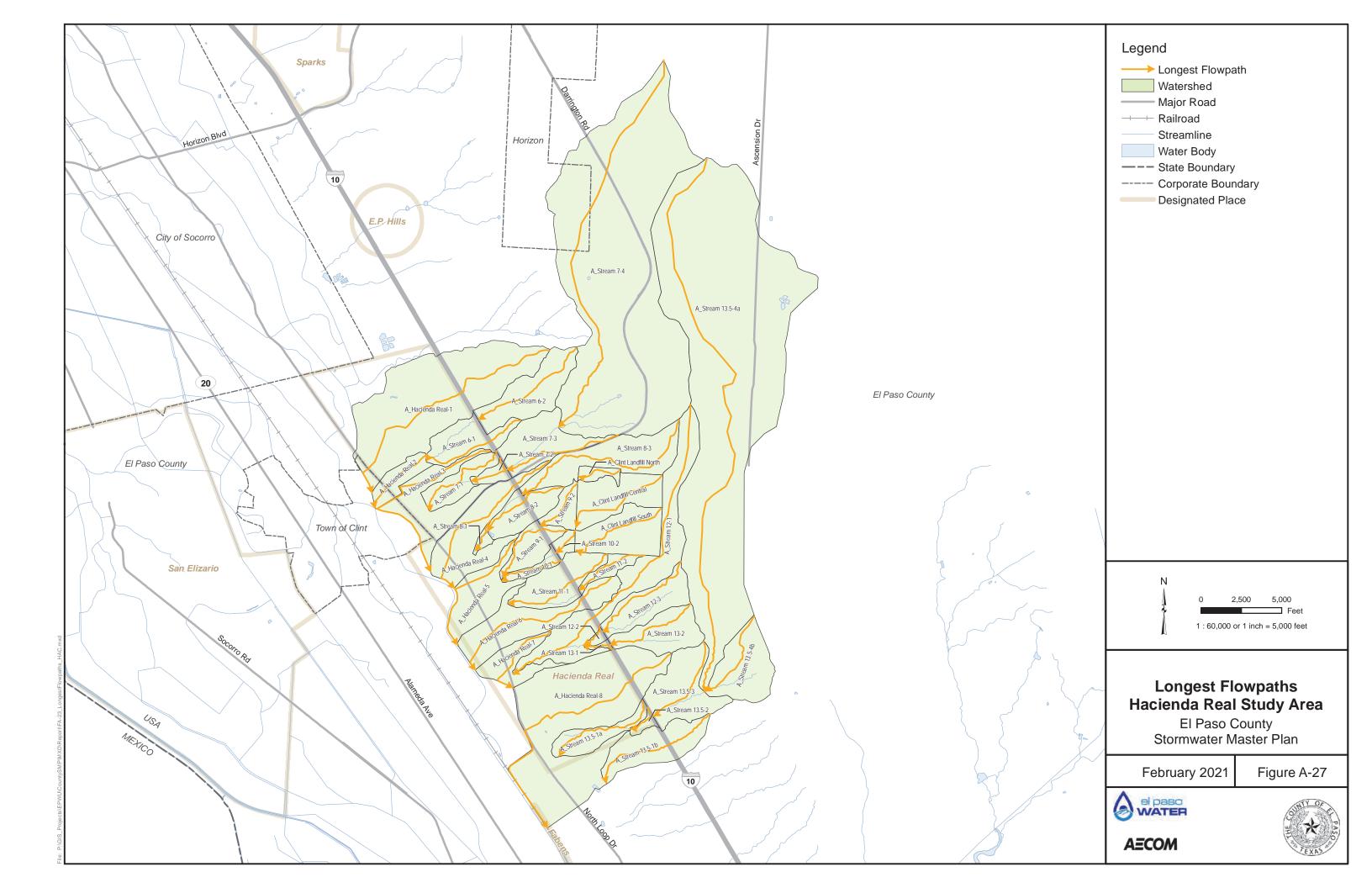


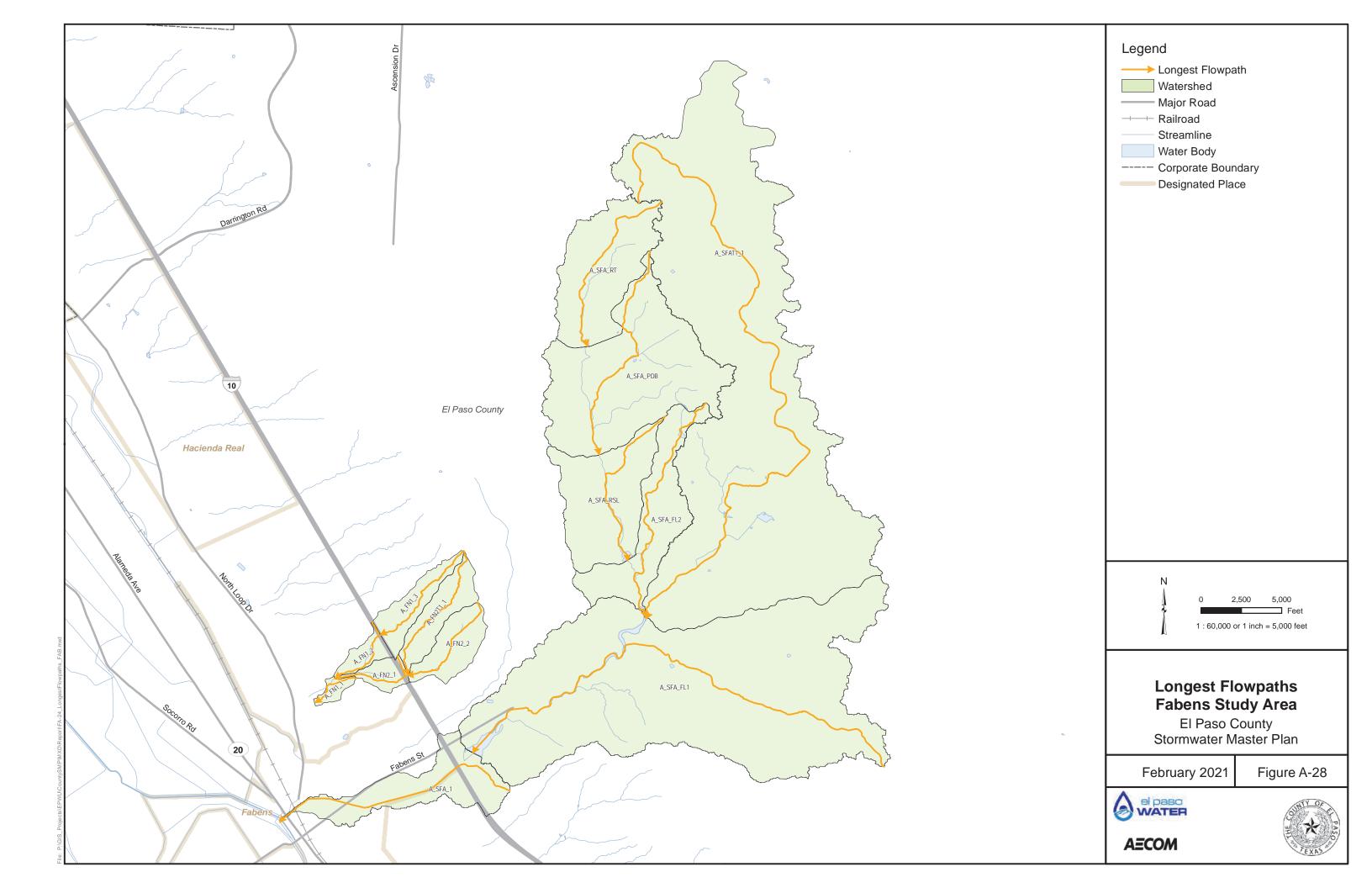


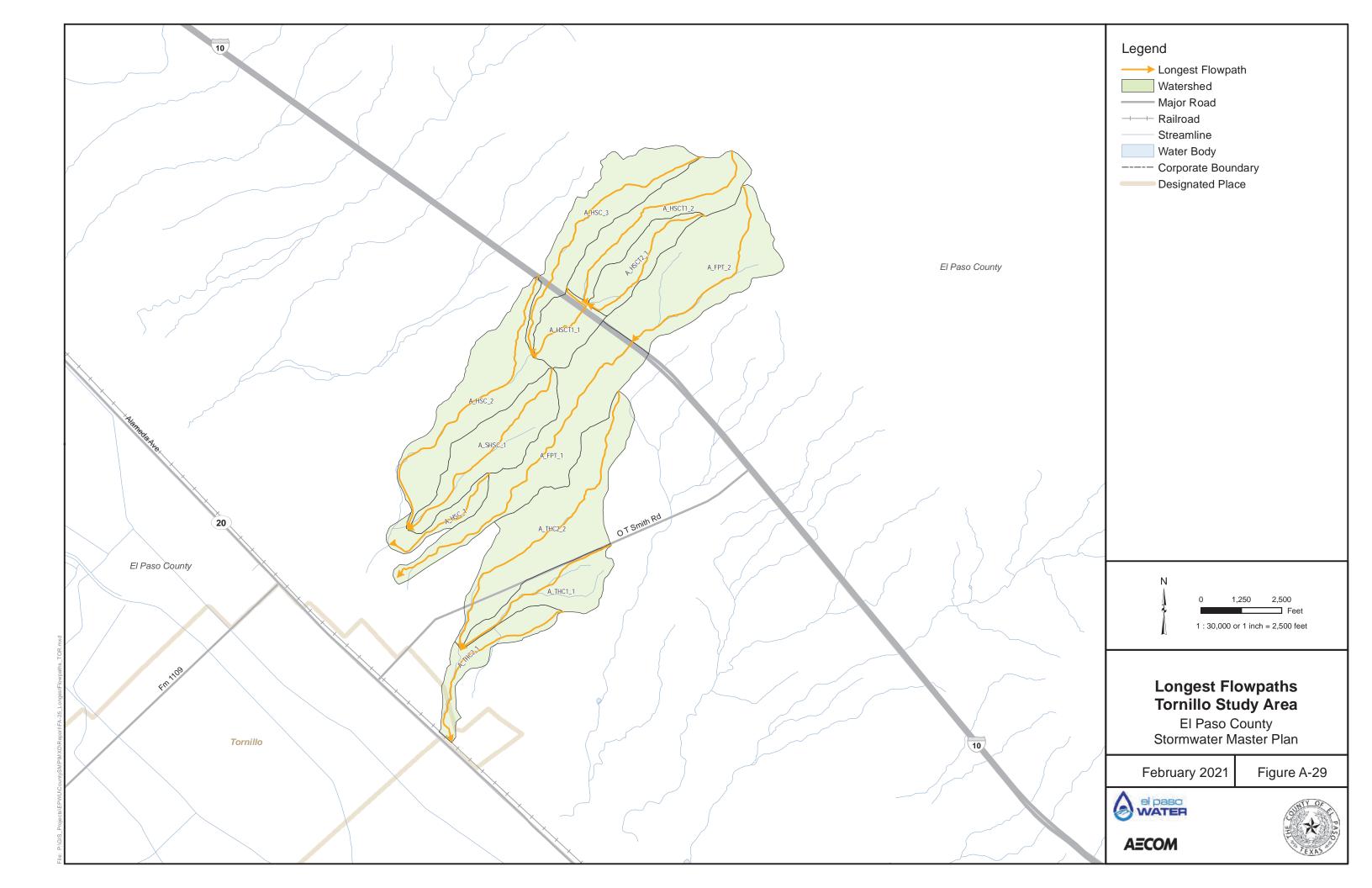


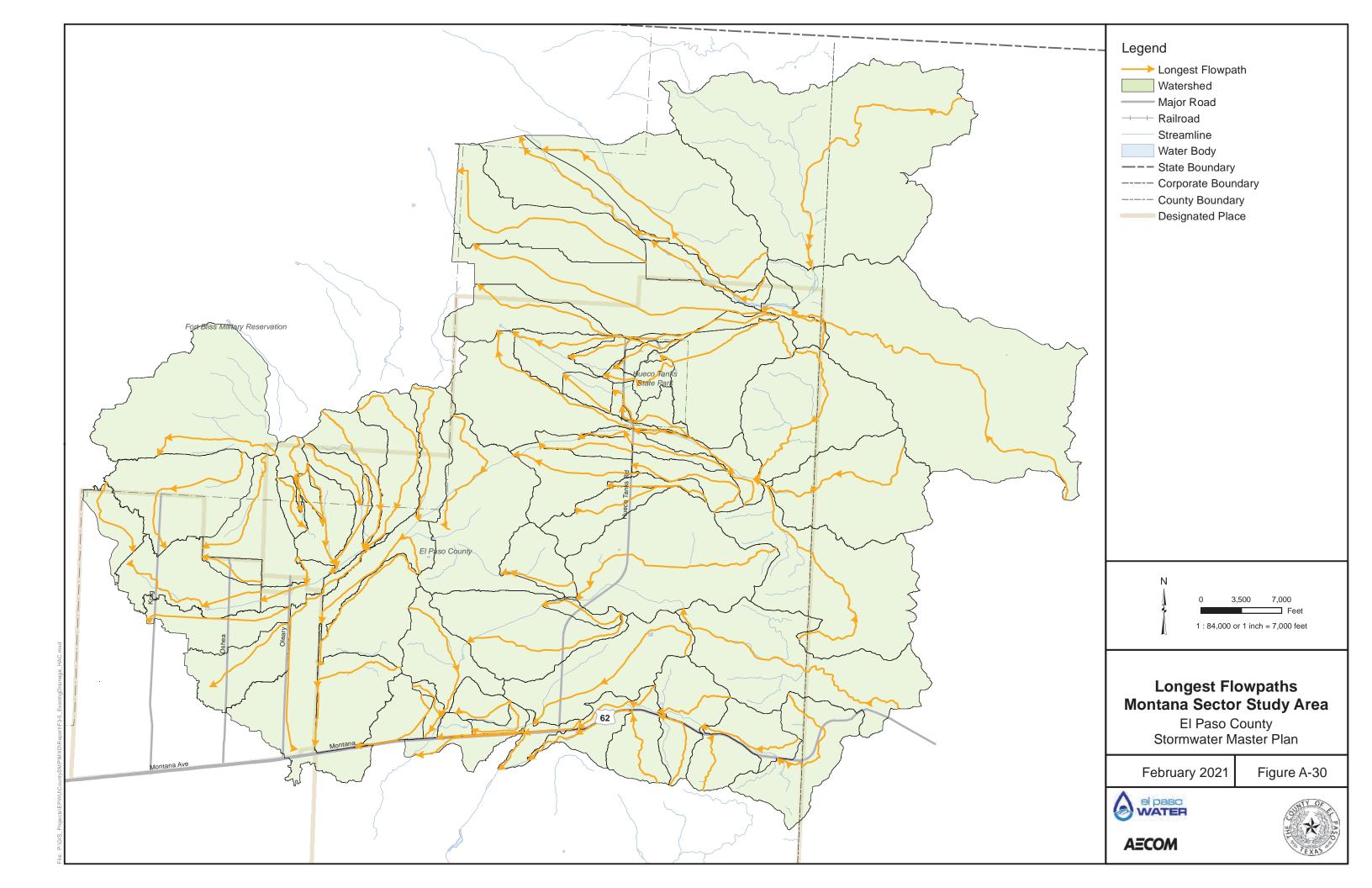


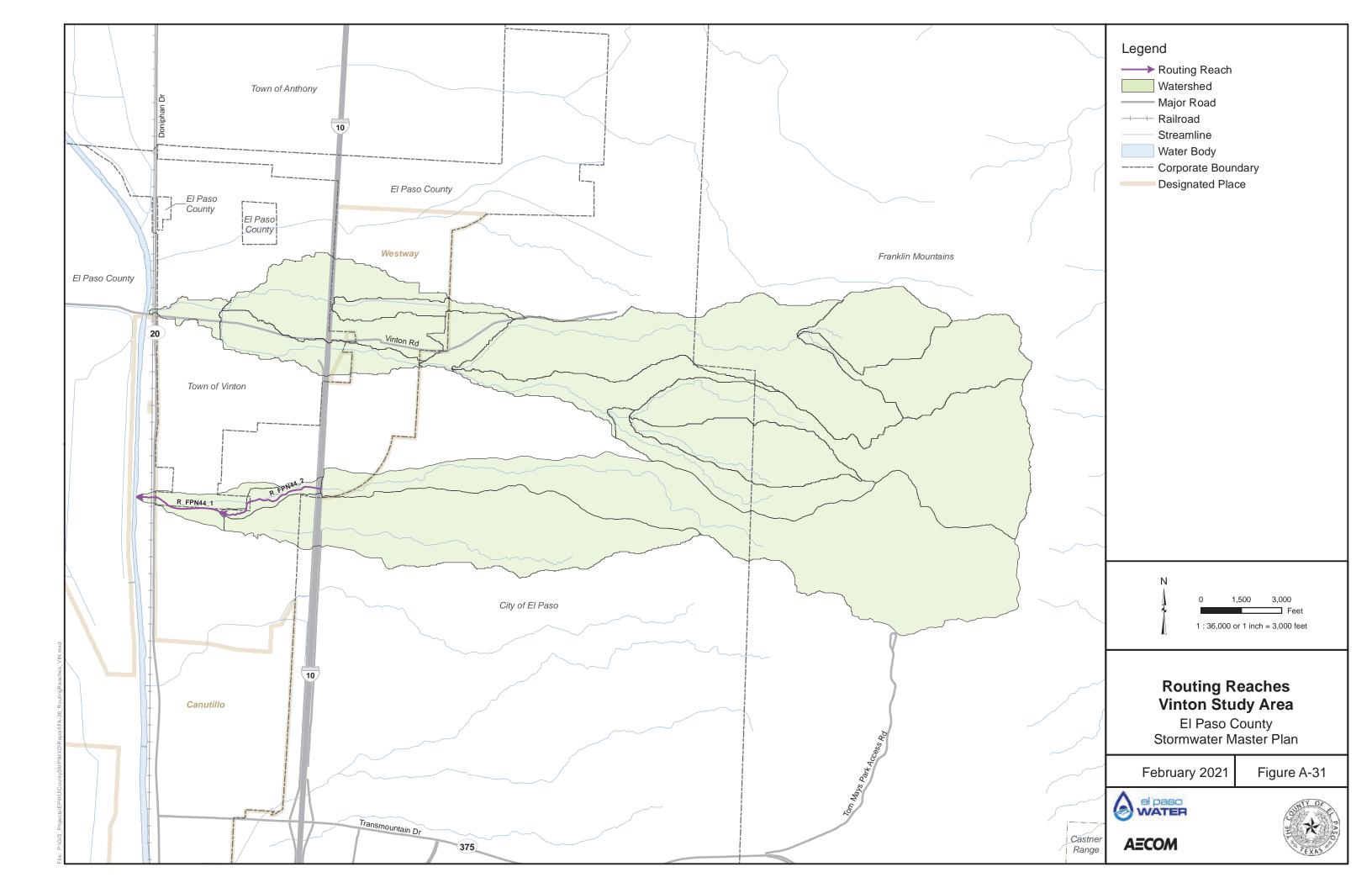


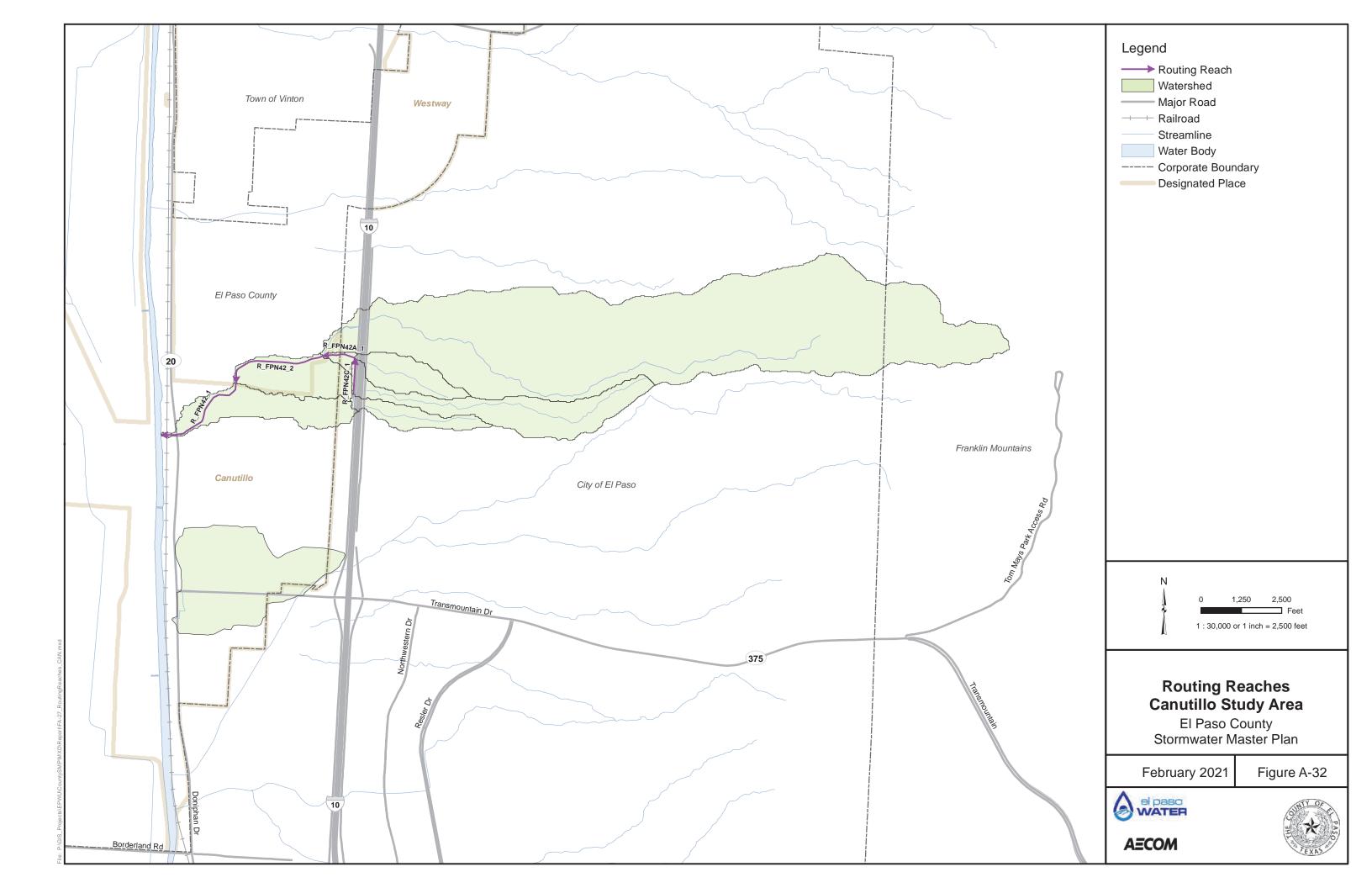


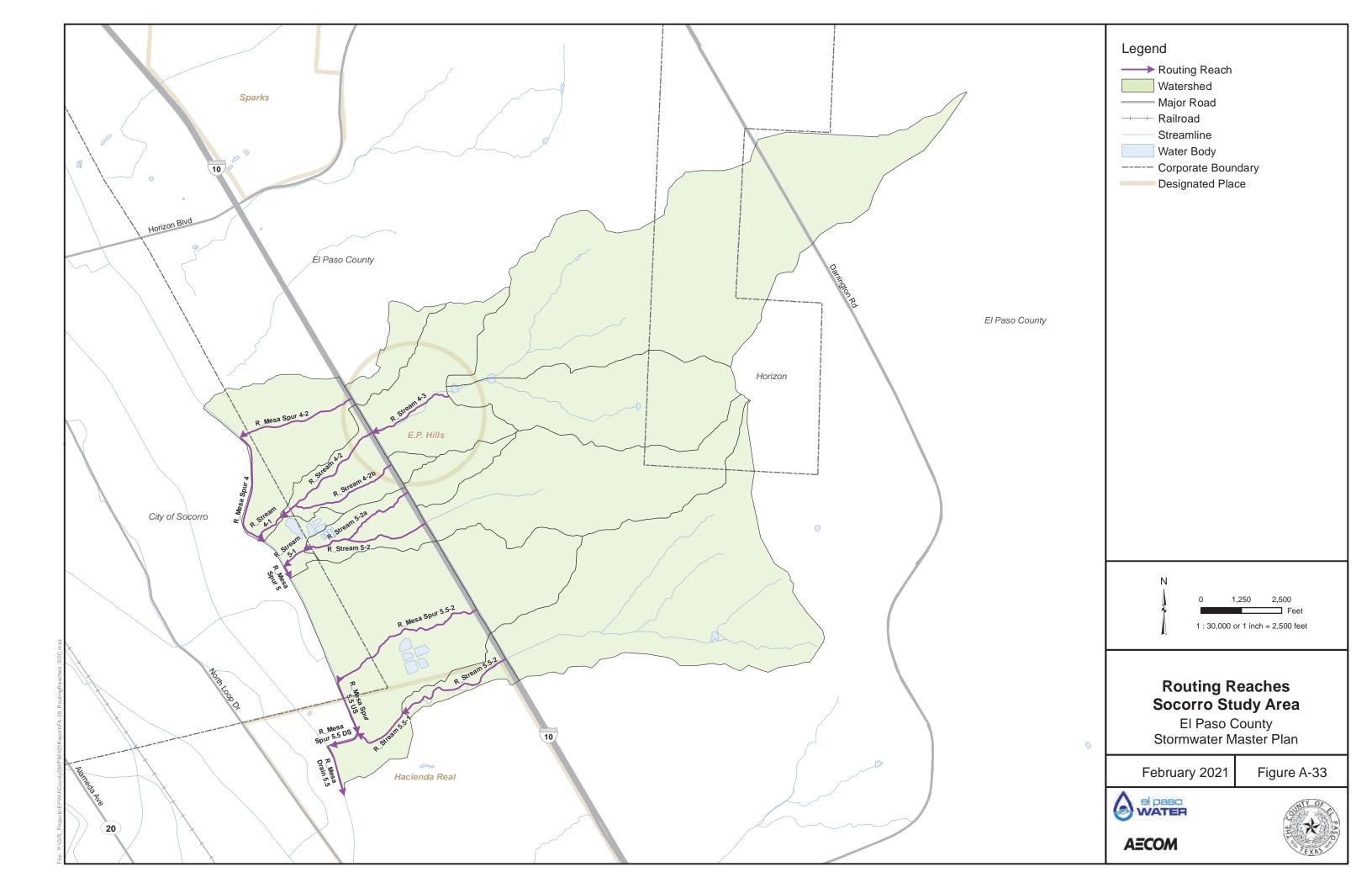


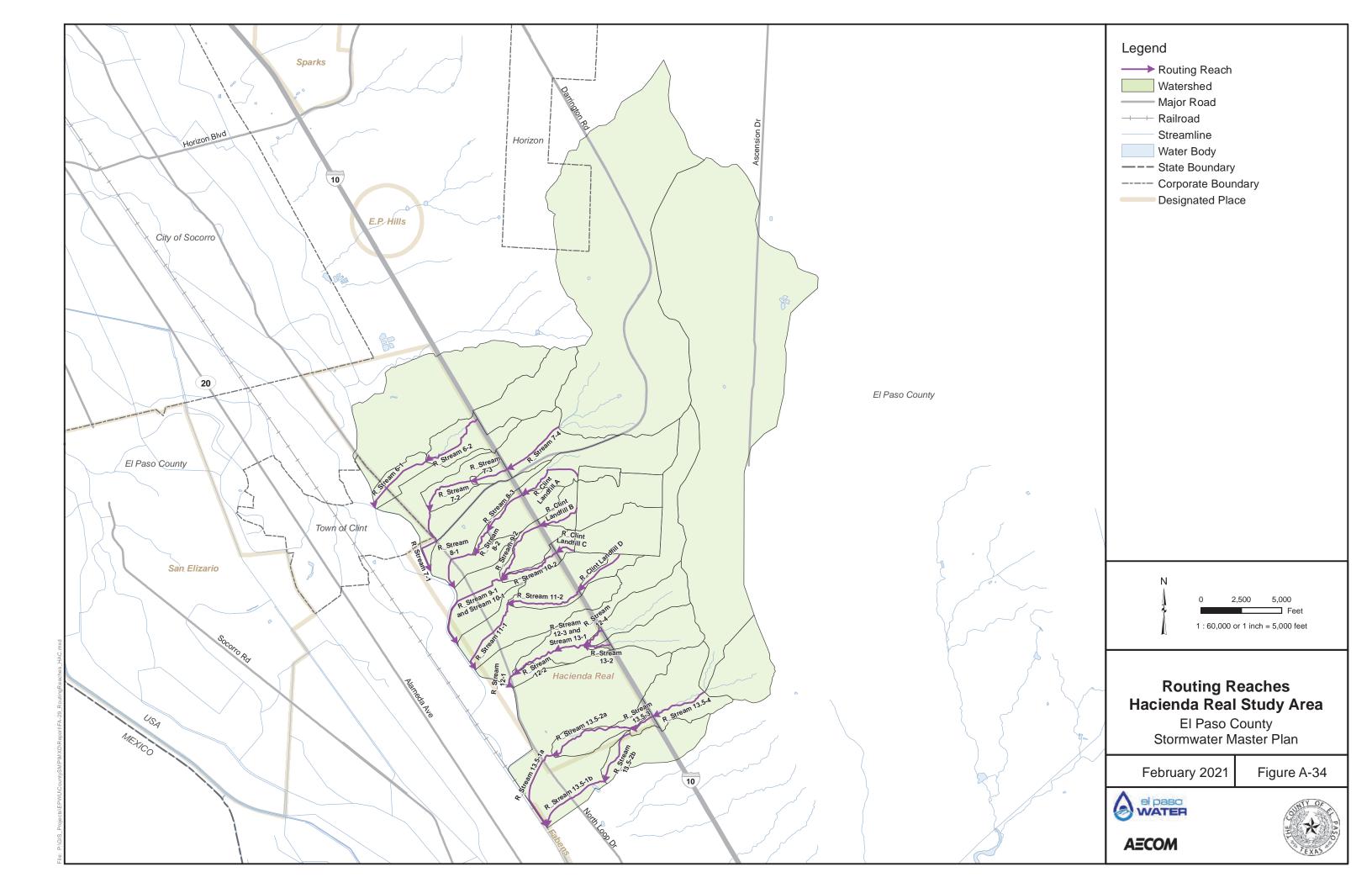


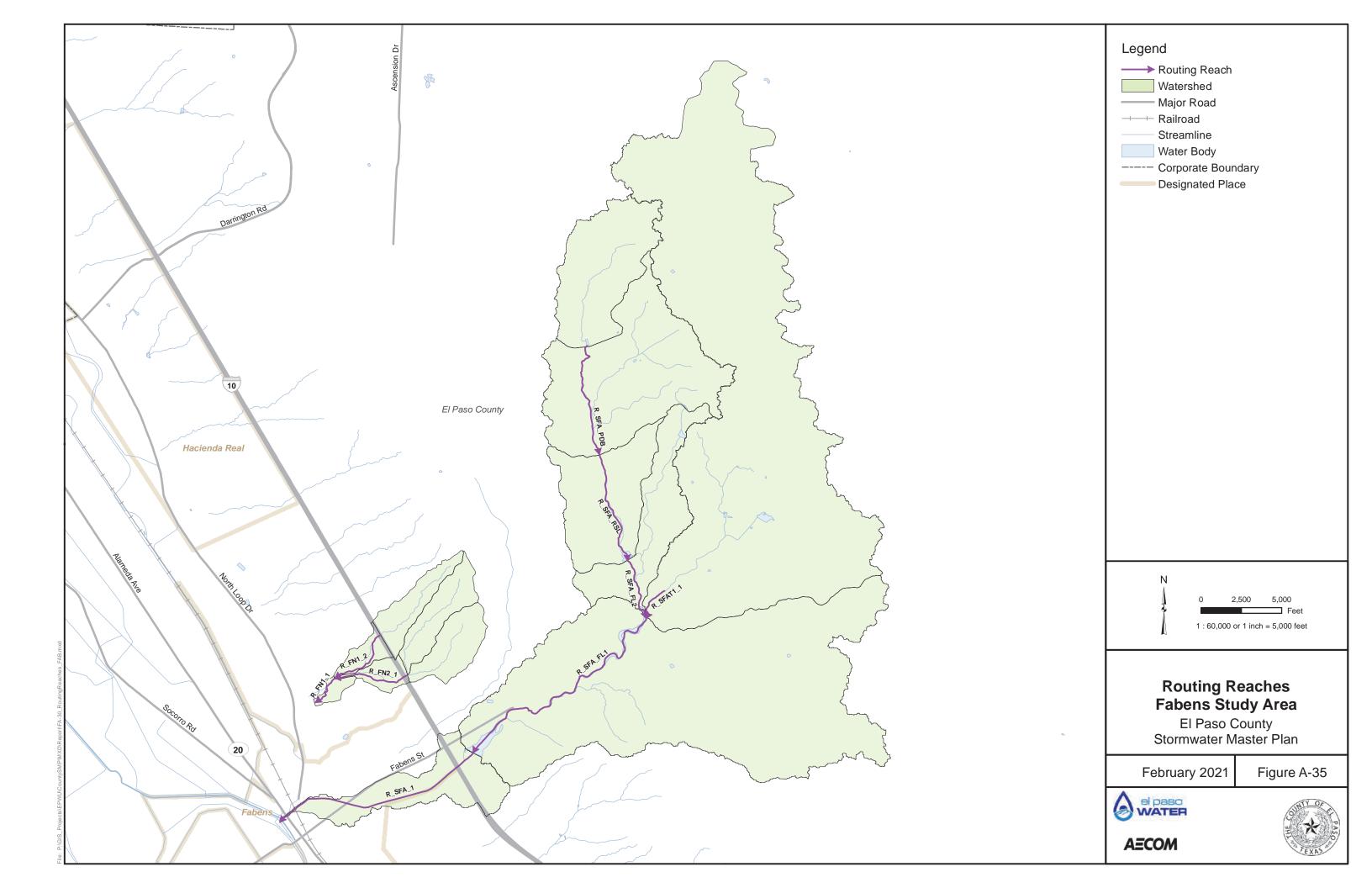


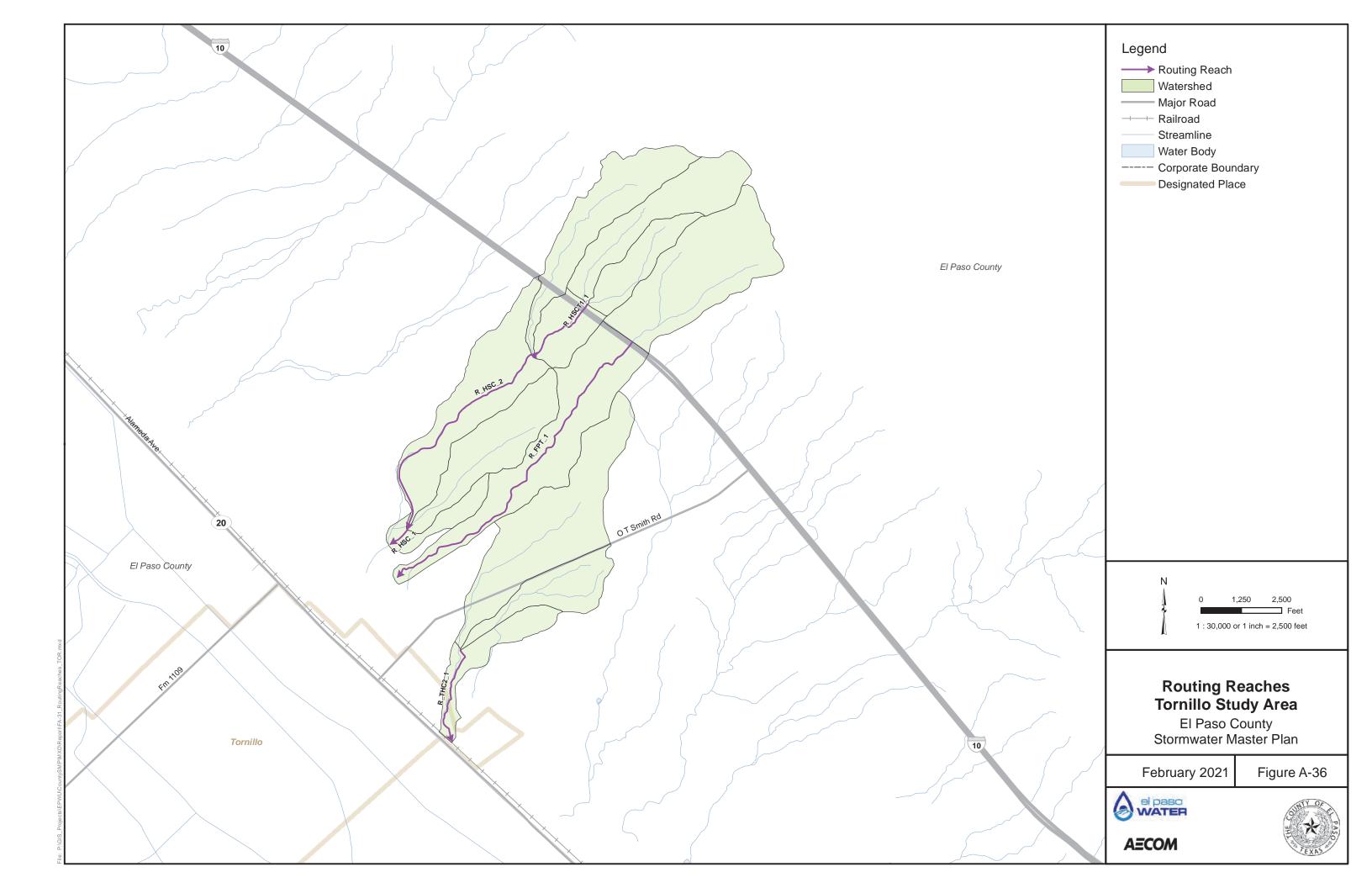


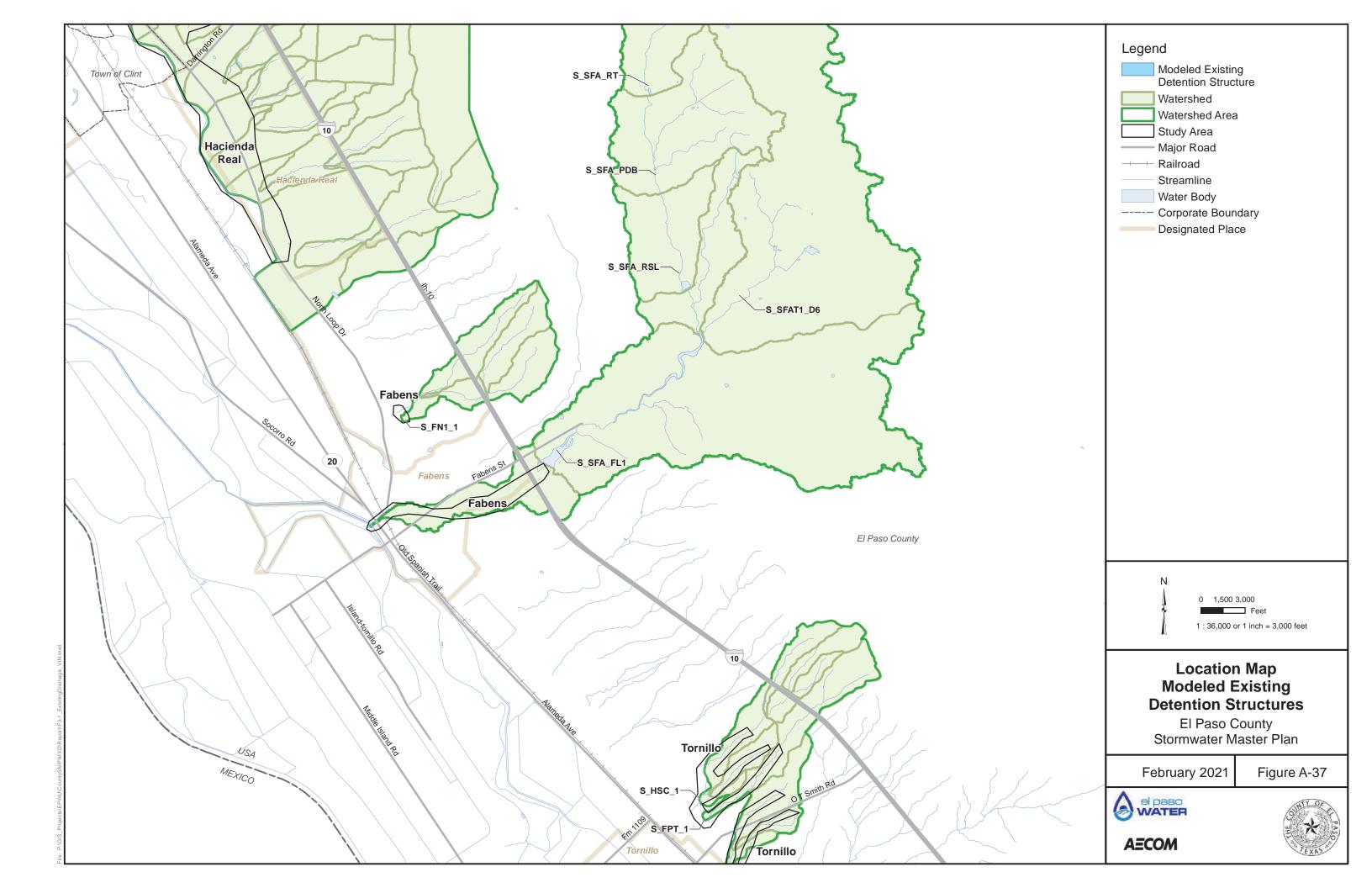


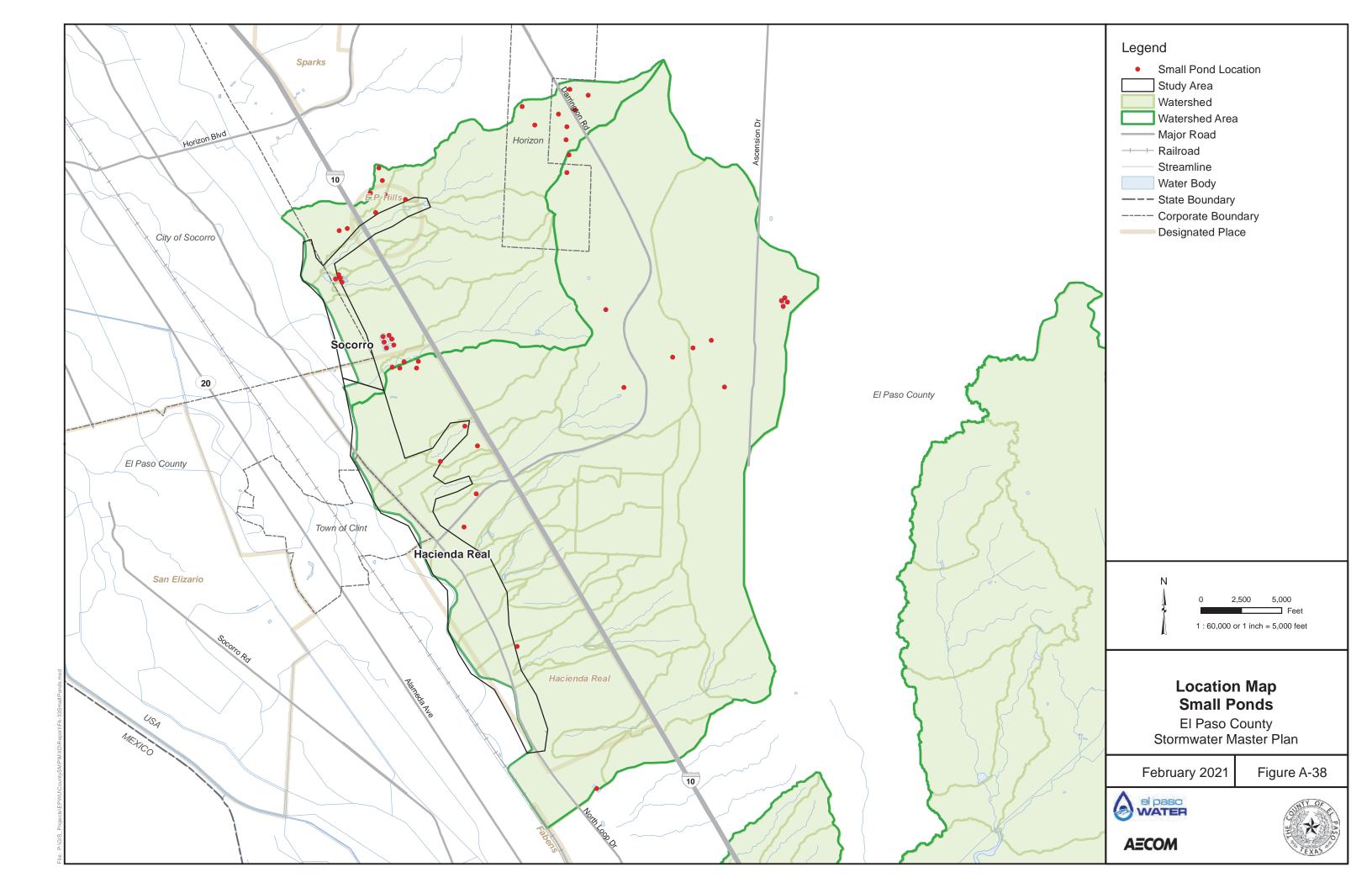












APPENDIX B HYDRAULICS REPORT

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B.1.0 BACKGROUND

A hydraulic analysis was performed in order to identify drainage structures with capacity issues. The hydraulic efficiency of the structures in the El Paso County study areas was analyzed as follows:

- Normal depth calculations were performed along all study reaches to estimate channel capacity.
- CulvertMaster calculations were performed at channel crossings to estimate crossing capacity.
- Previous Federal Emergency Management Agency (FEMA) Hydrologic Engineering Center-River Analysis System (HEC-RAS) models listed below were reviewed to identify potential capacity issues.
 - Flow Path Number 42 Canutillo study area
 - San Felipe Arroyo Fabens study area
- Other features exhibiting poor performance were identified through site evaluation and County feed back.

This appendix will present the basic methodologies associated with the calculations performed as part of the hydraulic evaluation process. An overview of the SMP Study Areas is provided on Figure B-1.

B.2.0 DATA SOURCES

Table B-1 lists the sources used in the hydraulic analysis, as well as the specific calculation(s) each source was used for.

B.3.0 CHANNEL ANALYSES

B.3.1 Method Overview

As part of the hydraulic study, channel capacities were analyzed for cross-sections located along each constructed study channel using Manning's Normal Depth assumption. Arroyo capacities were not estimated. Channel geometry was estimated from a variety of sources including site visit estimates, structure survey conducted as part of this project, El Paso County Orthophotos (El Paso County, 2008), and Texas Department of Transportation (TXDOT) 2004 three foot contour data (TXDOT, 2004). Cross-sections were analyzed near all crossing structures in order to estimate the channel capacity for the study channel. Capacity estimates were performed using Bentley FlowMaster, or an equivalent Normal Depth Method.

ArcView shapefiles were digitized to show the approximate cross-section locations corresponding to the capacities estimated for each of the regions studied.

B.3.2 Channel Analysis – Vinton

Channel flow capacities were calculated for the Vinton study area as described above. Channel top width, bottom width and depth were determined using TxDOT contour data, survey data where available and 2008 orthophotos. Channel slopes were estimated using the average channel slope within the region where the channel is consistent in geometry. Flow Path Number 45 and Flow Path Number 45A used the results that were determined during the analysis for the City of El Paso SMP. Results are provided in Table B-2 and Figure B-2 located at the end of this Appendix.

B.3.3 Channel Analysis – Canutillo

Channel flow capacities were calculated for the Canutillo study area as described above. First Ave. Channel's top width, bottom width and depth were determined by survey data received for this project and verified using orthophotos. Channel slope was estimated using the average channel slope between surveyed crossing structures. Flow Path Number 42 utilized a previous Federal Emergency Management Agency (FEMA) Hydrologic Engineering Center-River Analysis System (HEC-RAS) model, completed during the 2005 FEMA update of the Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS) for El Paso County. The model span is from Interstate Highway 10 (IH-10) and Flow Path Number 42's outlet at the Rio Grande. Results are provided in Table B-3 and Figure B-3 located at the end of this Appendix.

B.3.4 Channel Analysis - Socorro

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Channel flow capacities were calculated for the Mesa Spur Drain as described above. Channel top width, bottom width and depth were measured during initial site visits and verified using orthophotos. Channel slope was estimated using the average channel slope between surveyed crossing structures. Results are provided in Table B-4 and Figure B-4 located at the end of this Appendix.

B.3.5 Channel Analysis - Hacienda Real

Channel flow capacities were calculated for the Mesa Drain as described above. Channel top width, bottom width and depth were measured during initial site visits and verified using orthophotos. Channel slope was estimated using the average channel slope between surveyed crossing structures. Results are provided in Table B-5 and Figure B-5 located at the end of this Appendix.

B.3.6 Channel Analysis – Fabens

Channel flow capacities were calculated for the Fabens study area as described above. Fabens North 1 and Fabens North 2 used TxDOT contour data to determine the channel top width, bottom width and depth and verified the data using orthophotos. Channel slope was estimated using the average channel slope between the confluence and either the outlet structure or crossing structure. San Felipe Arroyo utilized the FEMA HEC-RAS model, completed during the 2005 FEMA update of the FIRMs and FIS for EI Paso County. The model span is from IH-10 to the channel outlet at the River Drain Canal. Results are provided in Table B-6 and Figure B-6 located at the end of this Appendix.

B.3.7 Channel Analysis – Tornillo

Channel flow capacities were calculated for the Tornillo study area as described above. Channel top width, bottom width and depth were determined using TxDOT contour data and 2008 orthophotos. Channel slopes were estimated using the average channel slope within the region where the channel is consistent in geometry. Results are provided in Table B-7 and Figure B-7 located at the end of this Appendix.

B.4.0 CROSSING STRUCTURE ANALYSES

B.4.1 Method Overview

Crossing capacities were estimated using CulvertMaster and compared to channel capcities in order to identify potentially undersized crossings. Culvert geometry was obtained from a variety of sources including survey performed as part of this study and IH-10 crossing as-builts (TXDOT,1957). In order to ascertain the effect of tailwater on the culverts included in this study, a downstream channel cross section was entered for each culvert into CulvertMaster. Clear span bridges were not typically analyzed because they do not constrict channel flow and would have approximately the same capacity as the channel itself.

CulvertMaster uses several parameters, including the upstream invert elevation, the downstream invert elevation, and slope to analyze a culvert. Survey data was used where available for upstream and downstream invert elevations as well as top of road elevations. Inverts for IH-10 crossings were taken directly from the IH-10 as-builts.

As mentioned above, a parameter that is used by CulvertMaster to calculate tailwater depth is the channel geometry downstream of the culvert. This geometry was typically estimated from the nearest downstream analyzed cross-section as described in section B.3.0. The bottom of channel elevation was set to the downstream invert used in the culvert analysis.

As with the channel analysis described previously, ArcView shapefiles were digitized to show the approximate crossing locations. For each crossing analyzed, the nearest downstream HEC-HMS flow node was identified if on a modeled channel and a comparison was performed between the 100-year frequency flow and the crossing capacity. If not on a modeled channel, the nearest analyzed channel cross-section was identified and compared to the crossing capacity to determine if the crossing was insufficiently sized to handle channel flow.

B.4.2 Crossing Structure Analysis – Vinton

Crossing capacities were calculated for Flow Path Number 44 in the Vinton study area as described above. Flow Path Number 45 and Flow Path Number 45A crossings were analyzed during the Citywide SMP and those results were carried over to this study. Results are provided in Table B-8 and Figures B-8 located at the end of this Appendix.

B.4.3 Crossing Structure Analysis – Canutillo

Crossing capacities were calculated for the Canutillo study area as described above, for First Ave. Channel. The crossing at West Avenue and First Ave. Channel was not analyzed because the conduit was considered visibly undersized during field

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reconnaissance. The crossing capacities along Flow Path Number 42 were determined in the HEC-RAS model completed for the 2005 FEMA update of the FIRMs and FIS for El Paso County. Results are provided in Table B-9 and Figures B-3 located at the end of this Appendix.

B.4.4 Crossing Structure Analysis - Socorro

Crossing capacities were calculated for the Socorro study area as described above. Results are provided in Table B-10 and Figures B-4 located at the end of this Appendix.

B.4.5 Crossing Structure Analysis – Hacienda Real

Crossing capacities were calculated for the Hacienda Real study area as described above. Results are provided in Table B-11 and Figures B-5 located at the end of this Appendix.

B.4.6 Crossing Structure Analysis – Fabens

Crossing capacities were calculated for the Fabens study area using the HEC-RAS model completed for the 2005 FEMA update of the FIRMs and FIS for El Paso County. Results are provided in Table B-12 and Figures B-6 located at the end of this Appendix.

B.4.7 Crossing Structure Analysis – Tornillo

Crossing capacities were calculated for the Tornillo study area as described above. Results are provided in Table B-13 and Figures B-7 located at the end of this Appendix.

TABLES

Table B-1. Data Sources Used in Hydraulic Analysis

Source	Used For
Bentley, CulvertMaster, 2005.	Conduit Analysis
Bentley, FlowMaster, 2005.	Channel Analysis
El Paso County, 2008. Orthophotography.	Crossing Analysis Channel Analysis
ESRI ArcView, Version 9.2 (2006) and Version 9.3.1 (2009).	Crossing Analysis Channel Analysis
Federal Emergency Management Agency (FEMA), 2005. Updated Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS).	Channel Analysis
Texas Department of Transportation (TxDOT), 1957. Plans for Proposed Highway Improvement, IH-10 From FM 659 to a Point 2 Miles NE of Fabens. As-Builts.	Crossing Analysis
TxDOT, El Paso Office, 2004. Topography.	Crossing Analysis Channel Analysis

Table B-2. Channel Capacity Summary - Vinton Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Depth (ft)	Manning's n	Cross- Section Capacity (cfs)	Cross-Section Location	HMS Node	100-Year Flow (cfs)
Flow Path Number 44	11	3:1	8.5	0.032	2,169	360' Upstream of Doniphan Drive	S_FPN44	2,169
Flow Path Number 44	6	4:1	6.5	0.03	1,175	1,080' Downstream of Confluence of Flow Path Number 43	R_FPN44_1	2,146
Flow Path Number 44	67	2:1	1	0.03	525	480' Downstream of IH-10	R_FPN44_2	1,280
Flow Path Number 45 (Vinton)	Irregu	ılar Geom	etry	0.03	511	10,800' Upstream of Tom Mays Drive	N/A	511
Flow Path Number 45 (Vinton)	Irregular Geometry		etry	0.031	2,909	4,625' Upstream of Tom Mays Drive	N/A	2,909
Flow Path Number 45 (Vinton)	Irregular Geometry		0.035	1,000	466' Downstream of Tom Mays Drive	N/A	2,909	
Flow Path Number 45 (Vinton)	Irregular Geometry		0.035	6,070	340' Downstream of IH-10	N/A	6,070	
Flow Path Number 45 (Vinton)	Irregular Geometry		0.03	2,910	250' Downstream of IH-10 Southbound On-Ramp	N/A	6,070	
Flow Path Number 45 (Vinton)	Irregu	ılar Geom	etry	0.035	1,020	250' Downstream of Kiely Road	N/A	6,201
Flow Path Number 45 (Vinton)	Irregu	ılar Geom	etry	0.031	6,201	290' Downstream of AP Ramirez Street	N/A	6,201
Flow Path Number 45 (Vinton)	Irregu	ılar Geom	etry	0.03	660	Channel Downstream End	N/A	6,201
Flow Path Number 45A	Irregu	ılar Geom	etry	0.015	120	700' Upstream of De Alva Drive	N/A	189
Flow Path Number 45A	Irregu	ılar Geom	etry	0.03	1,050	550' Downstream of IH-10	N/A	1,050
Flow Path Number 45A	Irregu	ılar Geom	etry	0.03	550	200' Downstream of Lovena Way Road	N/A	1,050
Flow Path Number 45A	Irregu	ılar Geom	etry	0.032	630	535' Downstream of Lovena Way Road	N/A	1,050
Flow Path Number 45A	Irregu	ılar Geom	etry	0.032	1,050	200' Upstream of Kiely Road	N/A	1,050
Flow Path Number 45A	Irregu	ılar Geom	etry	0.032	1,050	290' Upstream of Confluence with Flow Path Number 45	N/A	1,050

Table B-3. Channel Capacity Summary - Canutillo Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Cross- Section Depth Manning's Capacity (ft) n (cfs) Cross-Section Location		HMS Node	100-Year Flow (cfs)		
First Avenue Channel	4	1:1 3		0.013	137	Upstream of West Avenue	A_FAC_1	533
Flow Path Number 42	Irregular Geometry		0.05	1,527	Upstream of Los Mochis Road	J_FPN42A,3	1,527	
Flow Path Number 42	Irregular Geometry			0.05	1,537	530' Upstream of Doniphan Drive	J_FPN42_2	1,578
Flow Path Number 42	Irregi	ular Geom	etry	0.05	571	Upstream of Doniphan Drive	J_FPN42_2	1,578

Table B-4. Channel Capacity Summary - Sparks Arroyo and Sub Basin A Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Depth (ft)	Manning's	Cross- Section Capacity (cfs)	Cross-Section Location	HMS Node ID	100-Year Flow (cfs)
Sparks Arroyo	25	3	5	0.03	2,650	Sparks	N/A	N/A

Table B-5. Channel Capacity Summary - Socorro Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Depth (ft)	Manning's	Cross- Section Capacity (cfs)	Cross-Section Location	HMS Node	100-Year Flow (cfs)
Mesa Spur Drain	10	1	10	0.05	335	Upstream of Carr Rd	N/A	N/A
Mesa Spur Drain	10	1	10	0.05	330	Upstream of Coker Rd	N/A	N/A
Mesa Spur Drain	10	1.5	8.5	0.05	275	Upstream of Anderson Rd	N/A	N/A
Mesa Spur Drain	12	1.25	10	0.05	480	Upstream of Mesa Drain	N/A	N/A

Table B-6. Channel Capacity Summary - Hacienda Real Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Depth (ft)	Manning's n	Cross- Section Capacity (cfs)	Cross-Section Location	HMS Node	100-Year Flow (cfs)
Mesa Drain	12	1.5	10	0.05	500	Upstream of Young John	N/A	N/A
Mesa Drain	16	1	9	0.05	470	Upstream of Pickard	N/A	N/A
Mesa Drain	12	1.5	9	0.05	320	Upstream of Northloop	N/A	N/A
Mesa Drain	17	1	9	0.05	870	Upstream of FM 1110 (Clint Cut-Off)	N/A	N/A
Mesa Drain	15	1.5	12	0.05	970	Upstream of Salatral Lateral	N/A	N/A
Mesa Drain	11	1	11	0.05	230	Upstream of Fenter	N/A	N/A
Mesa Drain	11	1.5	10	0.05	670	1000' Upstream of Celum (Dirt Road Crossing)	N/A	N/A
Mesa Drain	12	1.5	10	0.05	590	Upstream of Celum	N/A	N/A

Table B-7. Channel Capacity Summary - Fabens Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Depth (ft)	Manning's n	Cross- Section Capacity (cfs)	Cross-Section Location	HMS Node ID	100-Year Flow (cfs)
Fabens North 1	25	4:1	3	0.03	201	1830' Upstream of Downstream End	J_FN1_2,3	201
Fabens North 1	59	15:1	1	0.031	74	1355' Downstream of I-10 Crossing	J_FN1_2	74
Fabens North 2	72	3:0.5	0.5	0.03	127	1050' Downstream of I-10 Crossing	J_FN2_1	127
San Felipe Arroyo	Irregular Geometry		etry	0.03	629	Upstream of Citizen Transfer Road	R_SFA_1	629

Table B-8. Channel Capacity Summary - Tornillo Study Area

Channel	Bottom Width (ft)	Side Slopes (H:V)	Depth (ft)	Manning's	Cross- Section Capacity (cfs)	Cross-Section Location	HMS Node ID	100-Year Flow (cfs)
High School Channel	13	21:1	1	0.033	283	440' Upstream of Downstream End	S_HSC_1	283
High School Channel	22	3:1	3	0.033	254	1533' Upstream of Confluence of South High School Channel	J_HSC_2	254
High School Channel	82	5:1	1	0.03	223	3165' Downstream of Confluence of High School Channel Trib 1	R_HSC_2	223
South High School Channel	21	4:1	2	0.03	25	3000' Upstream of Confluence with High School Channel	A_SHSC_1	25
Flow Path T	46	1:1	1	0.03	232	5100' Upstream of Downstream end	S_FPT_1	232
Flow Path T	58	10:1	2	0.03	143	2670' Downstream of IH-10	R_FPT_1	143
Tornillo Handle Channel 1	32	4:1	4	0.03	17	810' Upstream of Confluence with Tornillo Handle Channel 2	A_THC1_1	17
Tornillo Handle Channel 1	23	14:1	1	0.03	17	2940' Upstream of Confluence with Tornillo Handle Channel 2	A_THC1_1	17
Tornillo Handle Channel 2	28	1:1	1	0.03	84	1160" Downstream of Big Master Street	S_THC2_1	84
Tornillo Handle Channel 2	13	4:1	2	0.03	53	Downstream of OT Smith Road	A_THC2_2	53
Tornillo Handle Channel 2	56	1:1	1	0.03	27	3300' Upstream of OT Smith Road	A_THC2_2	27

Table B-9. Culvert Capacity Summary - Vinton Study Area

Channel	Dimensions	Length (ft)	Velocity (ft/s)	Crossing Capacity (cfs)	Crossing Location	HMS Node	100-Year Flow (cfs)	Channel Capacity
Flow Path Number 44	1 - 16' x 5' CBC	70	27.11	800	Doniphan Drive	S_FPN44	2,169	2,169
Flow Path Number 45 (Vinton)	13 - 9' x 5' CBC	39	17	5,065	FP45 CV IH-10 Off-Ramp	NA	6,070	6,070
Flow Path Number 45 (Vinton)	Bridge	142	8	6,070	FP45 IH-10	NA	6,070	6,070
Flow Path Number 45 (Vinton)	13 - 9' x 5.3' CBC	42	7	4,610	FP45 CV IH-10 On-Ramp	NA	6,070	2,910
Flow Path Number 45 (Vinton)	2 - 8' x 3' CBC	43	11	303	FP45 CV Kiely Rd	NA	6,070	1,020
Flow Path Number 45 (Vinton)	4 - 36" Circular	67	16	348	FP45 CV A P Ramirez	NA	6,201	6,201
Flow Path Number 45 (Vinton)	2 - 6' x 6' CBC	70	16	915	FP45 CV Doniphan Dr	NA	6,201	6,201
Flow Path Number 45 (Vinton)	Bridge	19	16	3,555	FP45 Railroad	NA	6,201	6,201
Flow Path Number 45A	3 - 54" Circular	341	16	189	FP45A IH-10	NA	189	189
Flow Path Number 45A	5 - 48" Circular	73	17	788	FP45A - Lovena Way	NA	788	1,050
Flow Path Number 45A	3 - 30" Circular	38	9	116	FP45A Iron Dr	NA	1,050	630
Flow Path Number 45A	2 - 30" Circular	47	8	71	FP45A Kiely Rd	NA	1,050	1,050

Table B-10. Culvert Capacity Summary - Canutillo Study Area

Channel	Dimensions	Length (ft)	Velocity (ft/s)	Crossing Capacity (cfs)	Crossing Location	HMS Node ID	100-Year Flow (cfs)	Channel Capacity
First Avenue Channel	2 - 6' x 3' CBC	89	3.6	130	Doniphan Drive	A_FAC_1	533	137
Flow Path Number 42	2 - 8' x 8' CBC	74	17.4	1,255	Los Vecinos	J_FPN42A,3	1,527	1,527
Flow Path Number 42	2 - 8' x 8' CBC	74	15.3	977	Los Poblanos	J_FPN42A,3	1,527	1,527
Flow Path Number 42	2 - 8' x 8' CBC	93	19.4	1,527	Loas Mochis	J_FPN42A,3	1,527	1,527
Flow Path Number 42	3 - 8' x 8' CBC	92	18.1	1,578	El Chanate	J_FPN42_2	1,578	1,537
Flow Path Number 42	8 - 5' x 5' CBC	67	8.0	1,578	Doniphan Drive	J_FPN42_2	1,578	571

Table B-11. Culvert Capacity Summary - Socorro Study Area

Channel	Dimensions	Length (ft)	Velocity (ft/s)	Crossing Capacity (cfs)	Crossing Location	HMS Node ID	100-Year Flow (cfs)	Channel Capacity
Mesa Spur Drain	1 - 48" CMP	40	9.4	118	Anderson	N/A	N/A	275
Mesa Spur Drain	1 - 48" CMP	50	10.0	126	Carr Rd	N/A	N/A	335
Mesa Spur Drain	1 - 48" CMP	40	10.7	135	Coker	N/A	N/A	330
Mesa Spur Drain	1 - 60" CMP	65	9.4	185	Mesa Drain	N/A	N/A	480
Arroyo 5	2 - 8' x 8' CBC	69	20.2	1,420	IH-10	A_Stream 5-2	185	N/A
Arroyo 5.5	2 - 10' x 10' CBC	81	21.1	2,045	IH-10	A_Stream 5.5-2	308	N/A

Appendix B - Tables

Table B-12. Culvert Capacity Summary - Hacienda Real Study Area

Channel	Dimensions	Length (ft)	Velocity (ft/s)	Crossing Capacity (cfs)	Crossing Location	HMS Node ID	100-Year Flow (cfs)	Channel Capacity
Mesa Drain	1 - 60" RCP	65	14.4	245	Northloop	N/A	N/A	320
Mesa Drain	1 - 42" CMP	132	10.4	99	FM 1110/Clint Cut Off	N/A	N/A	870
Mesa Drain	1 - 36" RCP	128	77.6	549	Salatral Lateral	N/A	N/A	970
Mesa Drain	1 - 72" CMP	139	13.1	322	Fenter	N/A	N/A	230
Mesa Drain	1 - 54" CMP	60	10.2	162	1000 US of Celum	N/A	N/A	670
Mesa Drain	1 - 36" CMP	63	11.7	82	Celum	N/A	N/A	590
Stream 6	4 - 7' x 4' CBC	76	18.0	1,238	IH-10	A_Stream 6-2	111	N/A
Stream 7	3 - 10' x 10' CBC	74	20.3	1,630	IH-10	J_AS7-3	2,084	N/A
Stream 7	5 - 48" CMP	130	13.5	733	Bridgeway	J_AS7-2	2,090	N/A
Stream 8	2 - 10' x 6' CBC	70	18.5	832	IH-10	J_AS8-3	309	N/A
Stream 9	2 - 10' x 6' CBC	67	19.5	1,458	IH-10	J_AS9-2	39	N/A
Stream 10	3 - 54" RCP	86	16.8	428	IH-10	J_AS10-2	26	N/A
Stream 11	4 - 54" RCP	85	16.3	673	IH-10	J_AS11-2	576	N/A
Stream 12	4 - 60" RCP	93.8	18.4	962	IH-10	A_Stream 12-4	106	N/A
Stream 13	5 - 60" RCP	99.7	17.0	1,368	IH-10	A_Stream 13-2	99	N/A
Stream 13.5	5 - 9' x 5' CBC	76	22.6	2,476	IH-10	J_AS13.5-3	1,609	N/A

Table B-13. Culvert Capacity Summary - Fabens Study Area

Channel	Dimensions	Length (ft)	Velocity (ft/s)	Crossing Capacity (cfs)	Crossing Location	HMS Node ID	100-Year Flow (cfs)	Channel Capacity
San Felipe Arroyo	Bridge	130	6.7	629	IH-10	R_SFA_1	629	629
San Felipe Arroyo	4 - 60" RCP	58	14.4	313	Citizen Transfer Road	R_SFA_1	629	629
San Felipe Arroyo	12' x 6' CBC	88	12.6	390	Fabens Road	R_SFA_1	629	629
San Felipe Arroyo	5 - 8.5' x 4' CBC	39	5.1	629	Camp Street	R_SFA_1	629	629
San Felipe Arroyo	5 - 8' x 4' CBC	24	4.8	629	Railroad	R_SFA_1	629	629
San Felipe Arroyo	10 - 4' x 4' CBC	44	5.3	629	Alameda Avenue/Old Spanish Trail	R_SFA_1	629	629

Table B-14. Culvert Capacity Summary - Tornillo Study Area

Channel	Dimensions	Length (ft)	Velocity (ft/s)	Crossing Capacity (cfs)	Crossing Location	HMS Node ID	100-Year Flow (cfs)	Channel Capacity
Tornillo Handle Channel 2	2 - 36" x 19" Arch	70	8.95	27	OT Smith Road	A_THC2_2	53	53

Appendix B - Tables